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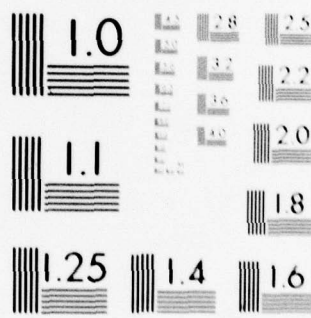
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MARINE SEISMIC REFRACTION DATA BETWEEN
WAINWRIGHT INLET AND PRUDHOE BAY, ALASKA.

BY

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MICHEL BEE
STEPHEN H. JOHNSON
EDWARD F. CHIBURIS
RICHARD E. McALISTER

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OR, 97331
- 2 WESTON OBSERVATORY, DEPARTMENT OF GEOLOGY AND GEOPHYSICS,
BOSTON COLLEGE, WESTON, MA 02193



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CONF of the methods and techniques used in the data collection and analysis.
Interpretation of the data is the subject of articles to be submitted to
professional journals.

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Michel Bée ¹
Stephen H. Johnson ¹
Edward F. Chiburis ²
Richard E. McAlister ¹

Office of Naval Research
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Geophysics Technical Report
No. 790626
June 1979

1 School of Oceanography, Oregon State University, Corvallis, OR, 97331

2 Weston Observatory, Department of Geology and Geophysics, Boston College,
Weston, MA, 02193. Formerly at Marine Sciences Institute, University
of Connecticut, Groton, CT.

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INTRODUCTION

The tectonic history of the Arctic Ocean Basin, and in particular the Canada Basin and the adjoining Beaufort Sea shelf, today remains unclear even after decades of geological and geophysical investigations. Reconstruction of the tectonic history of the margin requires information about the deep crustal structure of northern Alaska at the Beaufort Sea. In 1975 and 1976 a substantial amount of refraction data was successfully collected on the Alaskan shelf from an icebreaker. This technical report contains a detailed description of the methods and techniques used in the data collection and analysis. Interpretation of the data is the subject of articles to be submitted to professional journals.

DATA ACQUISITION

Location

Personnel from Oregon State University and the University of Connecticut conducted marine refraction studies in the eastern Chuckchi Sea and the western Beaufort Sea to obtain structural and velocity information on the continental margin. In contrast to most previous refraction studies in the region which were made from stations located on the ice, these data were obtained using standard marine seismic techniques during the Arctic Summer. Nineteen profiles were obtained between Wainwright Inlet and Prudhoe Bay in August 1975 from the USCG icebreaker Glacier and in August 1976 from the USCG icebreaker Burton Island with helicopter support. The profiles, ranging in length from 13 to 75 km, were roughly parallel to the coastline in about 20 m of water. Heavy ice cover forced many minor course changes and is the reason for the non-linear direction of individual profiles shown in Figure 1.

Techniques

A zone of ice-free or semi ice-free water exists along the northern continental shelf area out to a depth of approximately 2000 meters during one month of the year, and existence of this zone permitted operation of standard marine refraction techniques with sonobuoys and explosive charges.

The lines were shot in the standard marine fashion by dropping charges in the water from the fantail of the icebreaker, using powder fuses and tilt table, while the ship was underway. Rotor-mounted yagi antennas received the sonobuoy signals which were recorded on a 4-channel tape recorder. Two of the four channels were sonobuoy signals, one was

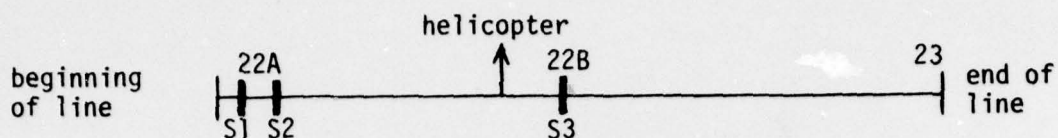
A map of Alaska showing the locations of profiles in the Beaufort and Chukchi Seas. The map includes a grid of latitude and longitude lines. The Beaufort Sea is labeled in the upper left, and the Chukchi Sea is labeled in the lower left. The profile locations are marked with numbers 1 through 37, and letters A and B. The locations are distributed along the northern coast of Alaska, from Point Barrow in the west to Oulitok Point in the east. A shaded rectangular area is shown in the upper right corner of the map, indicating a specific region of interest. The map also shows the outlines of Alaska and the surrounding waters.

a clock signal and one was a shot-break signal from a streamer 3 m long which was towed close behind the ship. When radio contact with the sonobuoys was lost, at a distance of about 30 km because of earth curvature, a portable recording unit consisting of a radio receiver, an amplifier, and strip-chart and tape recorders installed in a helicopter, monitored the sonobuoy. The helicopter remained within radio reception range of the sonobuoy during the shooting.

Expendable naval sonobuoys of the type AN/SSQ 41A were modified for extended time operation by addition of dry-cell batteries which worked well in spite of the cold water. Explosive charges of less than 10 pounds were made up of nitro-carbonitrate (Nitromon) in one pound metal cans. Explosive charges between 30 and 660 pounds were made up of Tovex in 30 pound plastic bags. Extra boosters (Dupont HDP-1) were required for large charges or for long burn times in order to insure complete detonation in the cold water.

Shots were detonated every three minutes at a ship speed of 10 kt which was slightly variable because of ice conditions. This resulted in a shot spacing of about 0.7 km. During the helicopter operations, shots were detonated at intervals of from 5 to 15 minutes resulting in a shot spacing of 1.4 to 4.3 km.

Sonobuoy deployments consisted of two sonobuoys (S1, S2) dropped at the beginning of each line and an intermediate sonobuoy (S3) deployed in the middle of long lines. This resulted in a special line numbering with letter A for the first sonobuoys and letter B for the intermediate one (for example, Lines 22A-23 and 22B-23)



The satellite navigation equipment was inoperative during the second half of the experiment, therefore most of the navigation was by radar fixes to land points at 15 minute intervals. The ice coverage ranged from 0 to 8 octas during the course of the experiment and required frequent course changes and caution on the part of the shooter not to drop the charge onto pieces of floating ice.

Sea-surface currents were not negligible and affected sonobuoy drift. The direction and magnitude of the drift was estimated by combining water wave travel time and navigation. The in-line component of drift ranged from 0 to 1.65 m/s and was quite variable from line to line.

DATA REDUCTION

A combination of manual and computer-aided manipulations shown in the flow chart of Figure 2 transform the raw data to record sections and velocity-depth profiles.

Arrival times for ground and water waves picked on each seismogram and other information such as bathymetry, ship velocity and streamer length, constitute an input data file for computer program TIMCORM. This program computes corrected ground and water wave arrival times to a datum, making corrections for the shot instant due to separation of shot and streamer and surface and bottom corrections at receiver and shot.

These results form an input file for the computer program REFPLT which produces a travel time plot with the corrected arrival times of the ground waves at the distances calculated from corrected water wave arrival times. A first attempt is then made to interpret seismic velocities and the data examined for possible errors.

From the corrected output file obtained from program TIMCORM, the computer program REDPLOT2 produces a reduced time plot where arrival times reduced with a velocity of 5.00 km/s are plotted versus distance

A profile which includes some helicopter refraction data requires an additional routine. A data file is prepared from the ship navigation as an input to computer program UTMSTEVE and its two subroutine programs UTMGRIDB and UTM. These programs plot the navigation data on a Universal Transverse Mercator projection. Shot positions are added manually by interpolating time and arcs are drawn using a compass at a radius corresponding to the water wave travel time. Sonobuoy drift due to wind and currents appears as a non-coincidence of the arcs. A drift rate

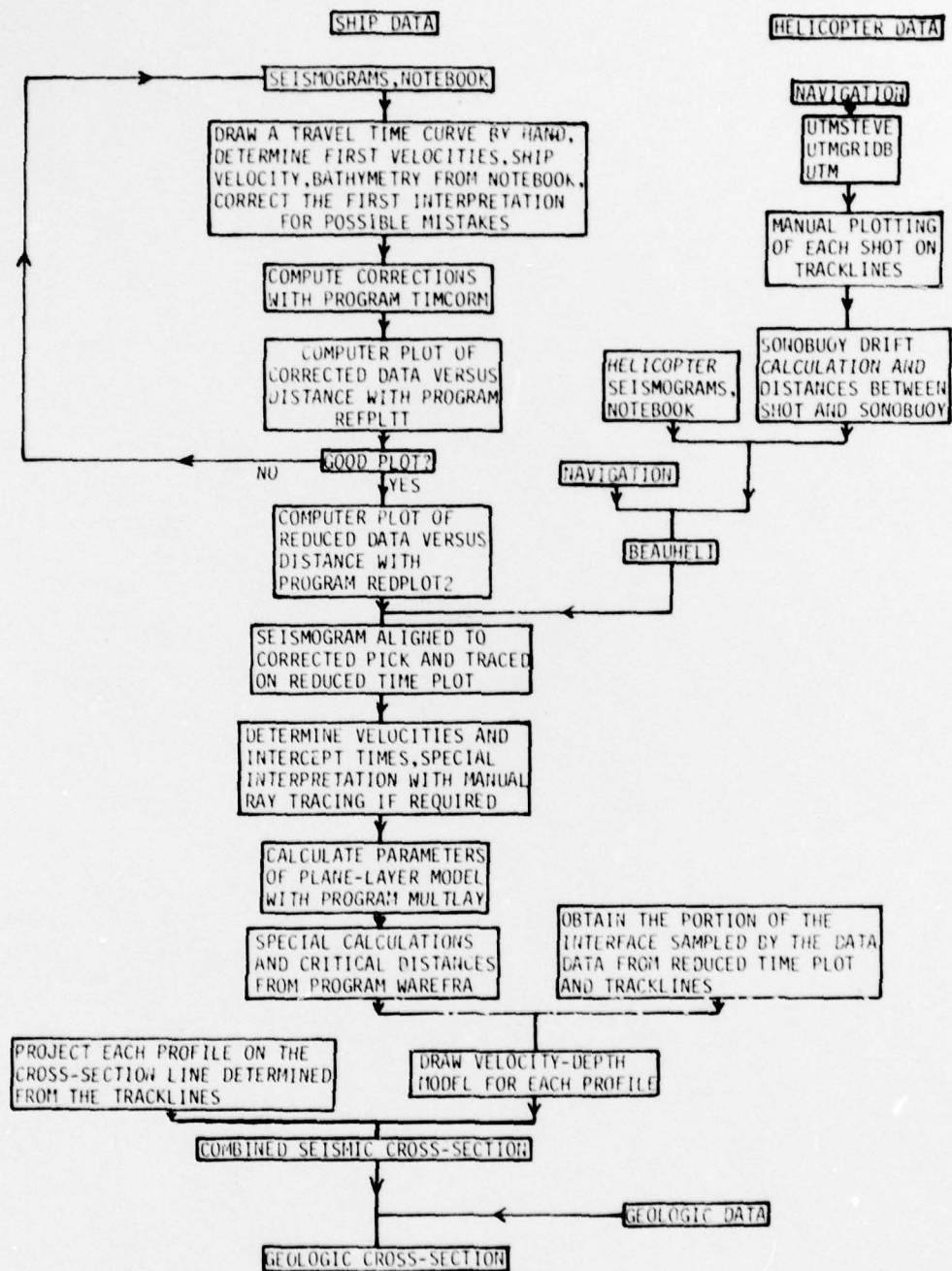


Figure 2. Flow chart of data analysis.

parallel to the trackline is assumed to apply to more distant shots where water wave arrival times may not be detected by the sonobuoy. The shot distance is then the distance between the shot location and the drift position of the sonobuoy at the time of the shot.

The drift distances between the shot and the sonobuoy and the ground wave arrival times from the helicopter refraction data constitute an input file for program BEAUHELI. Computer program BEAUHELI computes time corrections between the ship and the helicopter clocks, the corrected distance between the shot and the sonobuoy, and the corrected travel time for the ground arrival. The strip chart records played back from the helicopter recorder are then aligned to the corrected ground arrival times as plotted on the reduced time plot and traced to produce the record section.

Apparent velocities and intercept times are obtained from this record section and put into the computer program MULTLAY. The computer program MULTLAY computes a model composed of N dipping plane layers from reversed seismic refraction profile data using the formulation of Adachi (1954). The program requires two sets of apparent velocities and intercept times from single-ended refraction data. Complications such as non-reciprocal data or early intercept times require a manual ray tracing method based on the formulation of Adachi (1954).

On each seismic model obtained from MULTLAY the portion of an interface drafted with heavier lines on Figure 8 through Figure 26 represents only that portion of the layer which gives rise to observable seismograms. The offset distances of the rays are obtained from the program WAREFRA. The computer program WAREFRA is based also on the formulation of Adachi (1954) and requires the seismic model obtained from MULTLAY as an input data file.

For the combined velocity-depth section (Figure 27), each profile was projected onto a straight line drawn through the tracklines.

DATA INTERPRETATION

Because of the navigation difficulties, only five lines were reversed. These lines are Lines 1-2 and 6-7, Lines 3-4 and 4-5, Lines 10-11 and 12-13, Lines 22A-23 and 24B-25, and Lines 24A-25 and 22B-23 where the numbers indicate the end points of the lines (see for example Figures 10 and 11). The nine remaining lines (Lines GL-1, GL-2, 8A-9A, 8B-9B, 16-17, 18-19, 20-21, 26A-27A, 26B-27B) were interpreted as single-ended lines (see for example Figure 19). For complicated lines showing non-reciprocal data or early intercept times, a manual ray tracing method was used (see Figures 16 and 17).

Figures 8 to 26 show the nineteen profile plotted as reduced record sections where the reducing velocity is 5.0 km/s. The distance is plotted as water wave travel time seconds where the water velocity was estimated to be 1.44 km/s. All the velocities are in km/s. The seismic models determined from interpreted reduced sections are composed of plane horizontal or plane dipping layers. These are shown above the record sections with a vertical exaggeration of 3:1. Heavy lines on the refractors indicate the interfaces responsible for observed arrivals and contain the horizontal offsets for upgoing rays. Only the reversed profiles resulted in true velocities, and on all the single-ended profiles apparent velocities are assumed to be true velocities. A few estimated velocities are shown in parentheses.

The composite section shown in Figure 27 summarizes the subsurface velocity and depth information calculated from the refraction data. The heavy lines on the interfaces, corresponding to the observed arrivals as shown in Figures 16 through 26, were projected onto a composite section

which passes through the profiles. The small arrows along each interface correspond to the appropriate refraction lines shown at the top of the figure. The refraction layers from adjacent lines have been correlated on the basis of velocity as indicated in Figure 27 by light lines.

PRESENTATION OF DATA

I

MAP-GENERATING COMPUTER PROGRAMS (UTMSTEVE, UTMGRIDB, UTM)
NAVIGATION LISTING AND
TRACKLINE MAPS


```

UTASTEVE
1.  COMPILER DOUBLE PRECISION
2.C  PROGRAM UTMAPP
3.C  THIS PROGRAM CALLS UTMGRID TO MAKE AN UNIVERSAL TRANSVERSE
4.C  MERCATOR GRID. IT THEN READS AN AEROMAS DATA FILE AND PLOTS
5.C  EITHER TRACKLINES OR ANNOTATED DATA POINTS ON THE GRID
6.  COMMON /UTM2/ MLAT, SLAT, ELONG, WLONG
7.  REAL LAT, LONG, NLAT, LX, LY, NX, NY, LATN, LONGN
8.  DIMENSION NAME (6), IVARI (2), FNAME (6)
9.C  CONSTANTS FOR THE CALCULATIONS
10.  PI = 3.1415926536
11.  PIB2 = PI / 2.0
12.  PIB4 = PI / 4.0
13.  TWOPI = PI * 2.0
14.  RTOD = 180. / PI
15.  DTOR = PI / 180.
16.  ISIDE = 1
17.C  GO GET THE GRID PARAMETERS AND DRAW THE GRID
18.  CALL UTMGRID
19.  TYPE "ANNOTATE THE DATA PTS"
20.  READ (11, 101) IANS
21.  101 FORMAT (A2)
22.C  SET UP THE INPUT FILE
23.  5 TYPE "FILENAME"
24.  READ (11, 102) FNAME (1)
25.  102 FORMAT (S10)
26.  CALL FOPEN (1, FNAME)
27.C  GET A DATA POINT
28.  10 READ (1, 100, END=20) IVARI, LAT, LATN, LONG, LONGN
29.  100 FORMAT (7X, 2A2, 1X, F3, 0, 1X, F5, 0, 1X, F4, 0, 1X, F5, 0)
30.C  CHECK LAT AND LONG FOR WITHIN THE GRID
31.  LAT = LAT + SIGN (LATN/60., LAT)
32.  LONG = LONG + SIGN (LONGN/60., LONG)
33.  IF (LAT .EQ. 0.0) GO TO 10
34.  IF (LONG .LT. 0.0) LONG = 360. + LONG
35.  IF (LAT .LT. SLAT OR LAT .GT. MLAT) GO TO 10
36.  IF (LONG .LT. WLONG OR LONG .GT. ELONG) GO TO 10
37.C  CONVERT LAT AND LONG TO UTM X AND Y
38.  CALL UTM (LAT, LONG, X, Y)
39.C  IF NO ANNOTATION DON'T NEED THE ANGLES ETC
40.  IF (IANS .EQ. 2HNO) GO TO 16
41.C  FIGURE OUT WHERE AND WHAT ANGLE TO ANNOTATE THE DATA POINT
42.  ISIDE = ISIDE * (-1)
43.  YMLY = Y - LY
44.  THETA = ATAN (YMLY / (X-LX))
45.  LX = X
46.  LY = Y
47.  IF (ABS (THETA) .LT. PIB4) GO TO 12
48.  ANGLE = 0
49.  NX = X
50.  IF (ISIDE .LT. 0) NX = NX - 0.3
51.  NY = Y
52.  GO TO 13
53.  12 ANGLE = 270.
54.  NX = X
55.  NY = Y
56.  IF (ISIDE .LT. 0) NY = NY + 0.3
57.C  LABEL THE DATA POINT
58.  15 CALL SYMBOL (NX, NY, 0.07, IVARI, ANGLE, 4)
59.  CALL PLOT (X, Y, 3)
60.C  PLOT THE DATA POINT
61.  16 CALL PLOT (X, Y, 2)
62.  CALL MARKER (1)
63.  GO TO 10
64.C  HERE ON EGF
65.  20 CONTINUE
66.  CALL FCLOS (1)
67.C  ANOTHER FILE ON THIS GRID
68.  TYPE "ANOTHER FILE"
69.  READ (11, 101) IFILE
70.  IF (IFILE .EQ. 2HYES) GO TO 5
71.  END

```

```

07      UTMGRID IS
08      COMPILER DOUBLE PRECISION
09      SUBROUTINE UTMGRID
10      THIS SUBROUTINE DRAWS A UTM MERCATOR GRID ON THE PLOTTER. IT
11      QUERIES THE USER FOR THE MAP PARAMETERS AND LEAVES THEM IN
12      COMMON FOR THE CALLING PROGRAM.
13      SOUTHERN LATITUDES AND WESTERN LONGITUDES ARE NEGATIVE
14      UTMRAP WILL WORK ACROSS BOTH THE DATELINE AND GREENWICH
15      MERIDIAN.
16      REAL    RINLAT, MAXLAT, MINLONG, MAXLONG
17      COMMON /UTM1/ SCALE, X0, Y0, BTOR, MTOI, A, B, C, LA, LALA
18      I       LESQ, ORLESQ, CRERI, K0
19      REAL    LA, LB, LESQ, LALA, MTOI, K0
20      REAL    RINLATN, MAXLATN, MINLONGN, MAXLONGN
21      REAL    LAT, LONG, MLAT, RLIN
22      COMMON /UTM2/ MLAT, SLAT, ELONG, WLONG
23      DIMENSION ABCD(40)
24      CODES FOR THE PLOTTER SUBROUTINES
25      INTEGER PENUP, PENDOWN, PLOTEB, PEN, ABCD
26      PENDOWN = 2
27      PENUP   = 3
28      PLOTEB  = -PENUP
29      CONSTANT FOR CALCULATIONS
30      BTOR = 3.1415926536 / 180
31      MTOI = 39.37
32      PARAMETERS FOR A UTMGRID
33      K0 = 0.9996
34      A = 1.0051092
35      B = 0.0051202
36      C = 0.0000100
37      LA = 6370206.4
38      LB = 6356583.0
39      LALA = LA * LA
40      LESQ = (LALA - LB * LB) / LALA
41      ORLESQ = 1.0 - LESQ
42      X0 = 0.0
43      Y0 = 0.0
44      IO WRITE (10,100)
45      LONGS WEST ARE NEGATIVE AND LATs SOUTH ARE NEGATIVE
46      100 FORMAT ('GIVE THE FOLLOWING: ',/,
47     1          '        MLAT    SLAT    WLONG    ELONG    SCALE    GRID',/,
48     2          '        B N   B N   B N   B N   B N   ')
49      READ (11,101) MAXLAT, MAXLATN, MINLAT, MINLATN,
50     1             MINLONG, MINLONGN, MAXLONG, MAXLONGN,
51     2             SCALE, RLIN
52      101 FORMAT ('F3.0,F2.0,F3.0,F2.0,F4.0,F2.0,F4.0,F4.0',/,
53     1            'IX,F3.0,4X,F6.0,1X,F4.0')
54      MAKE DECIMAL DEGREES OUT OF THE DEGREES AND MINUTES
55      SLAT = MINLAT + SIGN(MINLATN, MINLAT) / 60
56      MLAT = MAXLAT + SIGN(MAXLATN, MAXLAT) / 60
57      WLONG = MINLONG + SIGN(MINLONGN, MINLONG) / 60
58      ELONG = MAXLONG + SIGN(MAXLONGN, MAXLONG) / 60
59      RLIN = RLIN / 60
60      IF (MLAT .LE. SLAT) GO TO 16
61      MAKE LONGS 0 TO 360 TO THE EAST
62      IF (WLONG LT. 0.) WLONG = 360. + WLONG
63      IF (ELONG LT. 0.) ELONG = 360. + ELONG
64      TAKE CARE OF CROSSING GREENWICH - MAKE LONGS GO TO 720 DEGS
65      IF (WLONG LT. ELONG) GO TO 12
```

```

59.      ELONG = ELONG + 360
60.      12 WRITE (10,117)
61.      117 FORMAT (' PLOTTER READY')
62.      READ (11,114) IANS
63.      114 FORMAT (A2)
64.      IF (IANS .EQ. 2HYES) GO TO 15
65.      GO TO 10
66.      16 TYPE 'NLAT, SLAT ERROR'
67.      GO TO 10
68.      17 TYPE 'LONGS NOT WITHIN + OR - 3 DEGREES OF CENTRAL MERIDIAN'
69.      GO TO 10
70.      15 CALL FOPEN (6, 'SPLT')
71. C INITIALIZE THE PLOTTER
72.      CALL INITIAL (6, 100, -0.5, 22)
73.      CALL PLOT (1, 1, PLOTENB)
74. C INITIALIZE PEN POSITIONS
75.      SCALE = 1.0 / SCALE
76. C LETS LABEL IT AGAIN WITH INFORMATION CONCERNING THE MAP.
77. C AREA, DATA, ETC
78.      WRITE (10,102)
79.      102 FORMAT ('GIVE THE PLOT LABEL -- UP TO 80 CHARS ')
80.      READ (11,103) ABCD
81.      103 FORMAT (40A2)
82.      CALL SYMBOL (0, -1, 21, ABCD, 0, 80)
83.      TEMP = WLONG
84.      IF (WLONG .GE. 180) TEMP = WLONG - 360
85.      IZONE = (TEMP + 186) / 6
86.      CNERID = MOD ((IZONE-1) * 6 + 183, 360)
87. C NOTE CNERID 0 TO 360 DEGREES TO THE EAST
88.      IF (DABS (CNERID - WLONG) .GT. 3) GO TO 17
89.      IF (DABS (CNERID - ELONG) .GT. 3) GO TO 17
90. C NOW WITHIN + OR - 3 DEGREES OF CNERID
91.      IF (WLONG .GE. CNERID) CALL UTM (SLAT, WLONG, X, Y)
92.      IF (ELONG .LE. CNERID) CALL UTM (SLAT, ELONG, X, Y)
93.      IF (WLONG .LT. CNERID AND ELONG .GT. CNERID)
94.      1 CALL UTM (SLAT, CNERID, X, Y)
95.      Y0 = Y
96. C NOW HAVE MIN Y VALUE (Y0) FOR THE MAP
97.      IF (WLONG .GT. CNERID) CALL UTM (NLAT, WLONG, X, Y)
98.      IF (WLONG .LE. CNERID) CALL UTM (SLAT, WLONG, X, Y)
99.      X0 = X
100. C NOW HAVE MIN X VALUE (X0) FOR THE MAP
101. C (X0, Y0) ARE THE SOUTH WEST CORNER OF THE MAP SUCH THAT THE GRID
102. C DOES NOT GO EITHER SOUTH OR WEST OF THIS POINT
103. C GUESS THAT WE CAN START MAKING THE GRID
104. C START THE GRID DRAWING THE LATS EAST AND WEST
105.      LONG = WLONG
106.      LAT = SLAT
107.      BLONG = (ELONG - WLONG) / 10.001
108.      CALL UTM (LAT, WLONG, X, Y)
109.      CALL NUMBER (X-75, Y, 14, MINLAT, 0, -1)
110.      CALL NUMBER (X-30, Y, 14, MINLAT, 0, -1)
111.      CALL PLOT (X, Y, PENUP)
112.      PEN = PENDOWN
113.      GO TO 25
114. C DRAWING A LAT FROM WEST TO EAST
115.      20 PEN = PENUP
116.      LAT = LAT + MIN

```

```

117.      DLONG = -DLONG
118.      LONG = WLONG
119.      IF (LAT GT NLAT) GO TO 40
120. 25 IF (LONG GT ELONG) GO TO 30
121.      CALL UTM (LAT, LONG, X, Y)
122.      CALL PLOT (X, Y, PEN)
123.      PEN = PENDOWN
124.      LONG = LONG + DLONG
125.      GO TO 25
126. C DRAWING A LAT FROM THE EAST TO WEST
127. 30 PEN = PENUP
128.      LAT = LAT + MIN
129.      IF (LAT GT NLAT) GO TO 40
130.      LONG = ELONG
131.      DLONG = -DLONG
132.      CALL UTM (LAT, LONG, X, Y)
133.      CALL PLOT (X, Y, PEN)
134.      PEN = PENDOWN
135. 35 LONG = LONG + DLONG
136.      IF (LONG LT WLONG) GO TO 20
137.      CALL UTM (LAT, LONG, X, Y)
138.      CALL PLOT (X, Y, PEN)
139.      GO TO 35
140. 40 CONTINUE
141. C DONE WITH EAST AND WEST PORTION OF THE GRID
142. C NOW LETS DO THE NORTH AND SOUTH LINES
143.      LONG = WLONG
144.      LAT = SLAT
145.      DLAT = (NLAT - SLAT) / 10 001
146.      CALL UTM (LAT, LONG, X, Y)
147.      CALL NUMBER (X- 40, Y- 25, 14, MINLONG, 0, -1)
148.      CALL NUMBER (X+ 10, Y- 25, 14, MINLONG, 0, -1)
149.      CALL PLOT (X, Y, PENUP)
150.      PEN = PENDOWN
151.      GO TO 50
152. C DRAWING A LONG FROM SOUTH TO NORTH
153. 45 PEN = PENUP
154.      LONG = LONG + MIN
155.      DLAT = -DLAT
156.      LAT = SLAT
157.      IF (LONG GT ELONG) GO TO 70
158. 50 IF (LAT GT NLAT) GO TO 55
159.      CALL UTM (LAT, LONG, X, Y)
160.      CALL PLOT (X, Y, PEN)
161.      PEN = PENDOWN
162.      LAT = LAT + DLAT
163.      GO TO 50
164. C DRAWING A LONG FROM NORTH TO SOUTH
165. 55 PEN = PENUP
166.      LONG = LONG + MIN
167.      IF (LONG GT ELONG) GO TO 70
168.      LAT = NLAT
169.      DLAT = -DLAT
170.      CALL UTM (LAT, LONG, X, Y)
171.      CALL PLOT (X, Y, PEN)
172.      PEN = PENDOWN
173. 60 LAT = LAT + DLAT
174.      IF (LAT LT SLAT) GO TO 45
175.      CALL UTM (LAT, LONG, X, Y)
176.      CALL PLOT (X, Y, PEN)
177.      GO TO 60
178. C DONE WITH THE GRID
179. 70 CONTINUE
180.      RETURN
181.      END

```



```

      UTM
1.  COMPILER DOUBLE PRECISION
2.  SUBROUTINE UTM (LAT, LONG, X, Y)
3.C  THIS SUBROUTINE CONVERTS LAT (PHI), LONG (DLAMBDA) TO X, Y
4.C  IN UTM COORDINATES IN INCHES FROM THE LOWER LEFT CORNER OF
5.C  THE PLOT AT SCALE
6.  REAL LA, LB, LESQ, LA, NU, LALA, MTOI, LAT, LONG, K0
7.C  UTM HAS PROJECTION PARAMETERS THAT ARE PASSED FROM UTMGRID
8.  COMMON /UTM/ SCALE, X0, Y0, DTOR, MTOI, A, B, C, LA, LALA,
9.  LESQ, OMLESQ, CNERID, K0
10.  PHI = LAT * DTOR
11.  SINPHI = SIN (PHI)
12.  SPSP = SINPHI * SINPHI
13.  RHO = LA * OMLESQ / (1.0 - LESQ * SPSP) ** 1.5
14.  MU = LA / SQRT (1.0 - LESQ * SPSP)
15.  LN = LA * OMLESQ * (A * PHI - B * SIN (2 * PHI) / 2 +
16.  C * SIN (4 * PHI) / 4.)
17.  DLAMBDA = (LONG - CNERID) * DTOR
18.  DLDL = DLAMBDA * DLAMBDA
19.  DLDL2L = DLDL * DLAMBDA
20.  SINPHI = SIN (PHI)
21.  COSPHI = COS (PHI)
22.  TANPHI = TAN (PHI)
23.  Y = K0 * (LN + DLDL * MU / 2.0 * SINPHI * COSPHI)
24.  X = K0 * (DLAMBDA * MU * COSPHI + DLDL2L * MU / 6.0 * COSPHI ** 3 +
25.  (MU / RHO - TANPHI * TANPHI))
26.C  SCALE X AND Y TO INCHES ON THE PAPER
27.  X = X * SCALE * MTOI - X0
28.  Y = Y * SCALE * MTOI - Y0
29.  RETURN
30.  END

```

KBNAY

| | | | | | | | |
|-----------|------|----------|------------|------------|------|----------|------------|
| 1.750020 | 0440 | 71 15 63 | -157 01 00 | 73.760012 | 1200 | 70 50 20 | -151 29 00 |
| 2.750020 | 0500 | 71 10 17 | -157 24 20 | 74.760012 | 1220 | 70 48 50 | -151 19 00 |
| 3.750020 | 0512 | 71 02 78 | -157 30 60 | 75.760012 | 1240 | 70 47 50 | -151 10 00 |
| 4.750020 | 0540 | 71 04 50 | -157 47 50 | 76.760012 | 1300 | 70 47 90 | -151 05 00 |
| 5.750020 | 0600 | 71 02 54 | -157 55 60 | 77.760012 | 1320 | 70 46 50 | -150 55 00 |
| 6.750020 | 2000 | 71 10 73 | -157 07 50 | 78.760012 | 1340 | 70 44 70 | -150 48 00 |
| 7.750020 | 2015 | 71 12 00 | -157 02 00 | 79.760012 | 1400 | 70 44 00 | -150 40 00 |
| 8.750020 | 2025 | 71 14 02 | -156 59 60 | 80.760012 | 1420 | 70 41 42 | -150 32 90 |
| 9.750020 | 2035 | 71 15 07 | -156 56 00 | 81.760012 | 1440 | 70 41 32 | -150 21 30 |
| 10.750020 | 2040 | 71 15 70 | -156 55 30 | 82.760012 | 1500 | 70 40 00 | -150 10 40 |
| 1.760005 | 2240 | 70 50 70 | -159 50 30 | 83.760012 | 1520 | 70 40 10 | -150 02 00 |
| 2.760005 | 2300 | 70 40 50 | -159 56 45 | 84.760012 | 1540 | 70 38 90 | -149 52 90 |
| 3.760005 | 2315 | 70 47 20 | -160 01 20 | 85.760012 | 1600 | 70 37 60 | -149 43 00 |
| 4.760005 | 2330 | 70 45 00 | -160 05 10 | 86.760015 | 0540 | 70 32 12 | -148 39 50 |
| 5.760005 | 2340 | 70 45 23 | -160 06 70 | 87.760015 | 0600 | 70 32 95 | -148 46 00 |
| 6.760006 | 0001 | 70 45 54 | -160 05 30 | 88.760015 | 0620 | 70 34 66 | -148 56 20 |
| 7.760006 | 0104 | 70 45 56 | -160 01 39 | 89.760015 | 0640 | 70 35 70 | -149 05 40 |
| 8.760006 | 0115 | 70 44 00 | -160 06 10 | 90.760015 | 0702 | 70 35 95 | -149 15 30 |
| 9.760006 | 0130 | 70 44 50 | -160 08 30 | 91.760015 | 0722 | 70 35 20 | -149 25 00 |
| 10.760006 | 0145 | 70 43 95 | -160 08 30 | 92.760015 | 0802 | 70 35 00 | -149 30 00 |
| 11.760006 | 0200 | 70 43 70 | -160 00 30 | 93.760015 | 0820 | 70 36 00 | -149 37 50 |
| 1.760006 | 0215 | 70 44 00 | -160 10 90 | 94.760015 | 0840 | 70 37 10 | -149 30 75 |
| 2.760006 | 0230 | 70 46 70 | -160 15 70 | 95.760015 | 0900 | 70 37 47 | -149 56 00 |
| 3.760006 | 0245 | 70 47 90 | -160 19 00 | 96.760015 | 0920 | 70 37 25 | -150 07 20 |
| 4.760006 | 0300 | 70 50 00 | -160 24 00 | 97.760015 | 0950 | 70 36 00 | -150 23 50 |
| 5.760006 | 0316 | 70 52 20 | -160 30 00 | 98.760015 | 1000 | 70 36 75 | -150 30 00 |
| 6.760006 | 0340 | 70 45 00 | -160 30 00 | 99.760015 | 1025 | 70 37 45 | -150 39 00 |
| 7.760006 | 0600 | 70 44 00 | -160 25 00 | 100.760015 | 1140 | 70 37 53 | -150 30 60 |
| 8.760006 | 0630 | 70 42 50 | -160 17 20 | 101.760015 | 1200 | 70 37 45 | -150 27 00 |
| 1.760007 | 2100 | 70 44 60 | -160 12 40 | 102.760015 | 1220 | 70 37 09 | -150 16 91 |
| 2.760007 | 2156 | 70 46 50 | -160 02 20 | 103.760015 | 1242 | 70 37 18 | -150 03 65 |
| 3.760007 | 2210 | 70 48 60 | -159 56 70 | 104.760015 | 1300 | 70 37 41 | -149 50 10 |
| 4.760007 | 2225 | 70 50 70 | -159 50 70 | 105.760015 | 1320 | 70 37 50 | -149 57 20 |
| 5.760007 | 2235 | 70 52 25 | -159 46 70 | 106.760015 | 1340 | 70 37 50 | -149 57 20 |
| 6.760007 | 2250 | 70 54 60 | -159 42 90 | 107.760015 | 1400 | 70 37 50 | -149 57 20 |
| 7.760007 | 2300 | 70 55 20 | -159 39 30 | 108.760015 | 1420 | 70 37 30 | -149 54 00 |
| 8.760007 | 2310 | 70 56 50 | -159 35 30 | 109.760015 | 1435 | 70 36 67 | -149 46 05 |
| 9.760007 | 2320 | 70 57 60 | -159 30 70 | 110.760015 | 1500 | 70 36 25 | -149 36 25 |
| 10.760007 | 2330 | 70 58 40 | -159 25 40 | 111.760015 | 1520 | 70 36 50 | -149 30 75 |
| 30.760011 | 1045 | 71 06 45 | -154 30 00 | 112.760015 | 1540 | 70 35 50 | -149 20 00 |
| 31.760011 | 1900 | 71 05 63 | -154 24 30 | 113.760015 | 1600 | 70 35 50 | -149 09 00 |
| 32.760011 | 1915 | 71 04 44 | -154 19 10 | 114.760017 | 0500 | 71 00 10 | -152 00 20 |
| 33.760011 | 1930 | 71 03 15 | -154 13 40 | 115.760017 | 0520 | 70 59 10 | -151 54 40 |
| 34.760011 | 1945 | 71 02 45 | -154 00 53 | 116.760017 | 0540 | 70 57 90 | -151 47 10 |
| 35.760011 | 2000 | 71 01 40 | -154 03 60 | 117.760017 | 0600 | 70 56 60 | -151 38 20 |
| 36.760011 | 2015 | 71 00 45 | -153 58 60 | 118.760017 | 0620 | 70 56 10 | -151 27 70 |
| 37.760011 | 2030 | 71 00 00 | -153 51 00 | 119.760017 | 0640 | 70 55 30 | -151 17 70 |
| 38.760011 | 2045 | 71 00 55 | -153 42 45 | 120.760017 | 0700 | 70 53 90 | -151 08 30 |
| 39.760011 | 2100 | 70 59 50 | -153 39 40 | 121.760017 | 0720 | 70 53 90 | -151 08 30 |
| 40.760011 | 2115 | 71 00 30 | -153 35 20 | 122.760017 | 0740 | 70 52 90 | -151 00 40 |
| 41.760011 | 2315 | 71 01 00 | -153 27 00 | 123.760017 | 0800 | 70 51 00 | -150 50 70 |
| 42.760011 | 2330 | 71 01 10 | -153 22 30 | 124.760017 | 0820 | 70 47 20 | -150 50 06 |
| 43.760011 | 2345 | 71 01 10 | -153 18 30 | 125.760017 | 0850 | 70 45 00 | -150 42 00 |
| 44.760012 | 0000 | 71 01 56 | -153 13 00 | 126.760017 | 0900 | 70 44 00 | -150 39 00 |
| 45.760012 | 0015 | 71 01 70 | -153 02 40 | 127.760017 | 0920 | 70 42 50 | -150 24 50 |
| 46.760012 | 0030 | 71 00 60 | -152 58 90 | 128.760017 | 0938 | 70 59 59 | -150 12 73 |
| 47.760012 | 0045 | 71 00 00 | -152 55 20 | 129.760018 | 0300 | 70 40 35 | -150 00 20 |
| 48.760012 | 0100 | 70 59 50 | -152 47 30 | 130.760018 | 0320 | 70 41 60 | -150 10 70 |
| 49.760012 | 0115 | 70 59 20 | -152 40 60 | 131.760018 | 0340 | 70 42 60 | -150 20 20 |
| 50.760012 | 0130 | 70 58 30 | -152 35 40 | 132.760018 | 0400 | 70 44 20 | -150 29 00 |
| 51.760012 | 0145 | 70 58 70 | -152 39 00 | 133.760018 | 0420 | 70 45 00 | -150 39 20 |
| 52.760012 | 0200 | 70 59 30 | -152 45 40 | 134.760018 | 0440 | 70 47 50 | -150 40 00 |
| 53.760012 | 0215 | 70 59 00 | -152 50 40 | 135.760018 | 0500 | 70 47 40 | -150 50 00 |
| 54.760012 | 0230 | 71 00 50 | -152 54 50 | 136.760018 | 0520 | 70 49 00 | -150 52 00 |
| 55.760012 | 0245 | 71 01 30 | -153 00 90 | 137.760018 | 0540 | 70 49 20 | -151 05 00 |
| 56.760012 | 0300 | 71 01 50 | -153 02 20 | 138.760018 | 0600 | 70 50 60 | -151 15 00 |
| 57.760012 | 0315 | 71 02 10 | -153 06 90 | 139.760018 | 0620 | 70 52 60 | -151 24 50 |
| 58.760012 | 0330 | 71 02 10 | -153 12 70 | 140.760018 | 0640 | 70 54 00 | -151 33 00 |
| 59.760012 | 0345 | 71 02 70 | -153 18 00 | 141.760018 | 0700 | 70 54 00 | -151 44 00 |
| 60.760012 | 0400 | 71 02 90 | -153 24 00 | 142.760018 | 0720 | 70 55 60 | -151 55 00 |
| 61.760012 | 0740 | 71 00 90 | -153 02 40 | 143.760018 | 0740 | 70 56 70 | -152 08 00 |
| 62.760012 | 0800 | 71 00 40 | -152 53 50 | 144.760018 | 1000 | 71 02 00 | -152 59 40 |
| 63.760012 | 0820 | 70 59 35 | -152 44 60 | 145.760018 | 1020 | 71 04 12 | -153 05 10 |
| 64.760012 | 0900 | 70 58 65 | -152 39 55 | 146.760018 | 1040 | 71 05 60 | -153 13 20 |
| 65.760012 | 0922 | 70 58 00 | -152 32 30 | 147.760018 | 1100 | 71 06 25 | -153 26 10 |
| 66.760012 | 0940 | 70 56 95 | -152 25 00 | 148.760018 | 1120 | 71 07 00 | -153 35 20 |
| 67.760012 | 1000 | 70 55 65 | -152 17 20 | 149.760018 | 1140 | 71 07 45 | -153 36 50 |
| 68.760012 | 1020 | 70 55 00 | -152 09 30 | 150.760018 | 1200 | 71 07 60 | -153 42 20 |
| 69.760012 | 1040 | 70 54 20 | -152 00 70 | 151.760018 | 1220 | 71 08 40 | -153 52 00 |
| 70.760012 | 1100 | 70 53 45 | -151 53 00 | 152.760018 | 1245 | 71 09 17 | -154 05 00 |
| 71.760012 | 1120 | 70 53 20 | -151 43 50 | 153.760018 | 1300 | 71 10 00 | -154 14 40 |
| 72.760012 | 1140 | 70 51 10 | -151 35 00 | 154.760018 | 1320 | 71 11 40 | -154 26 55 |
| | | | | 155.760018 | 1342 | 71 12 20 | -154 30 40 |

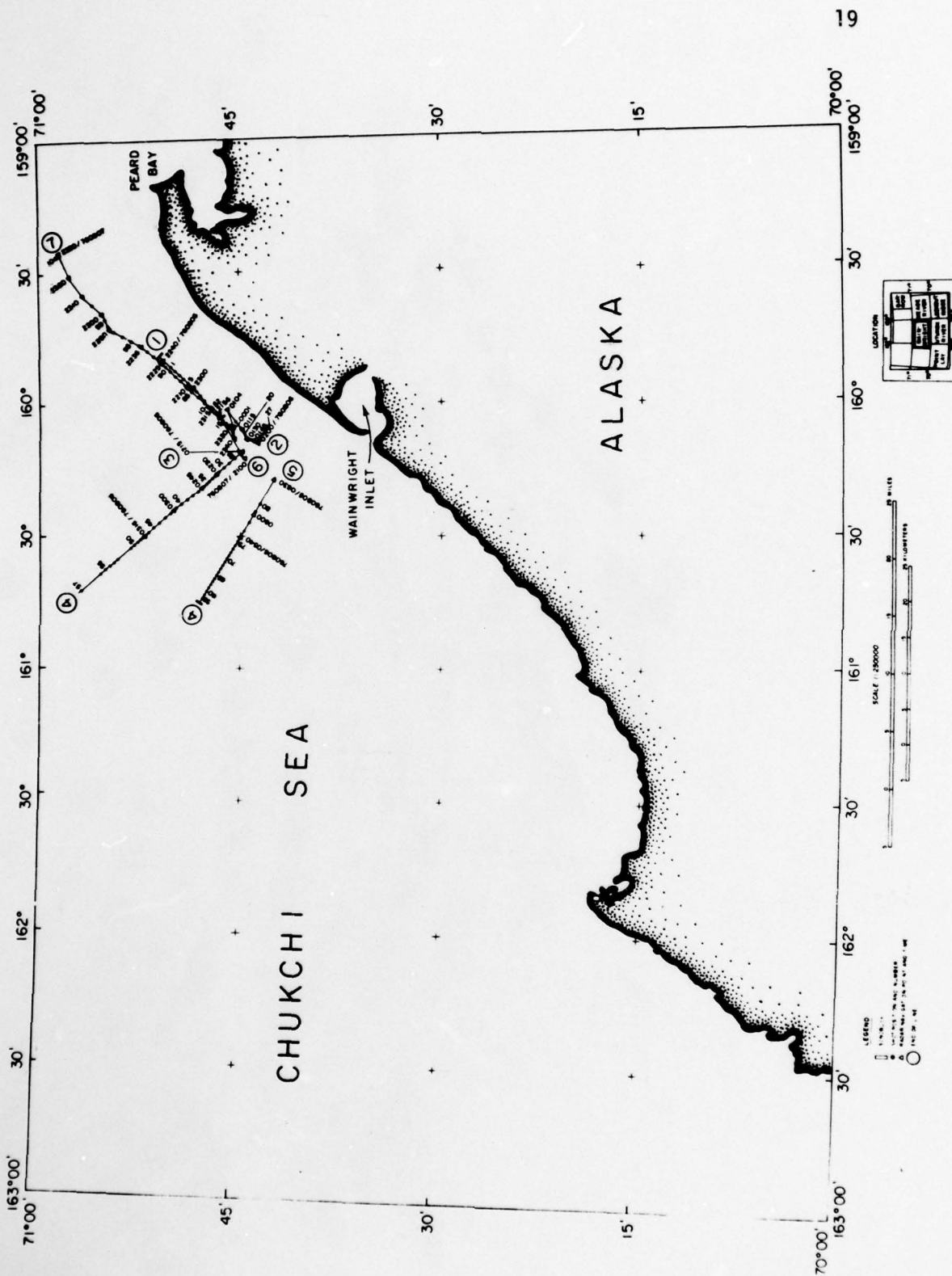


Figure 3. Tracklines and shot locations of Lines 1-2, 3-4, 4-5 and 6-7.

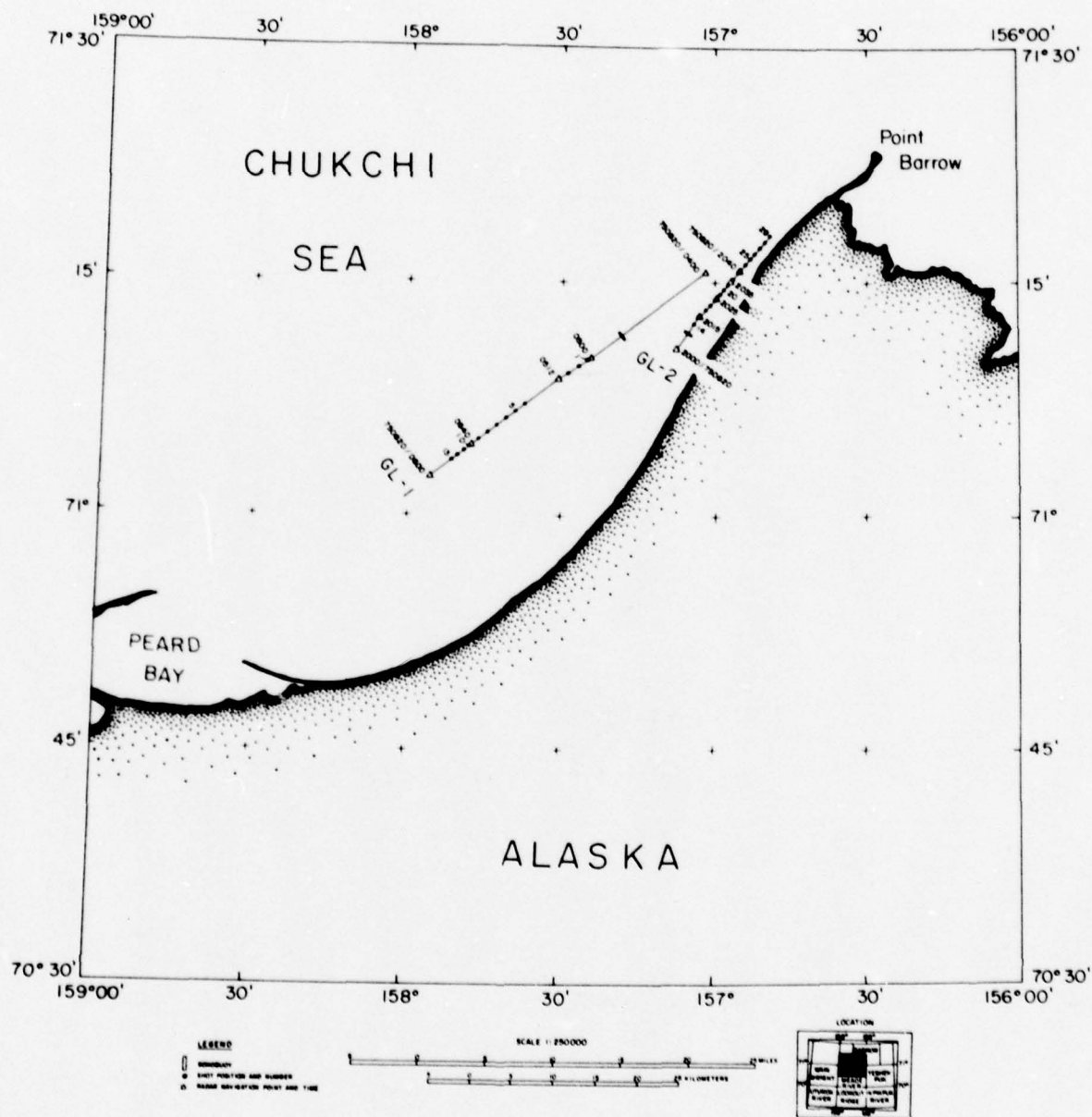


Figure 4. Tracklines and shot locations of Lines GL-1 and GL-2.

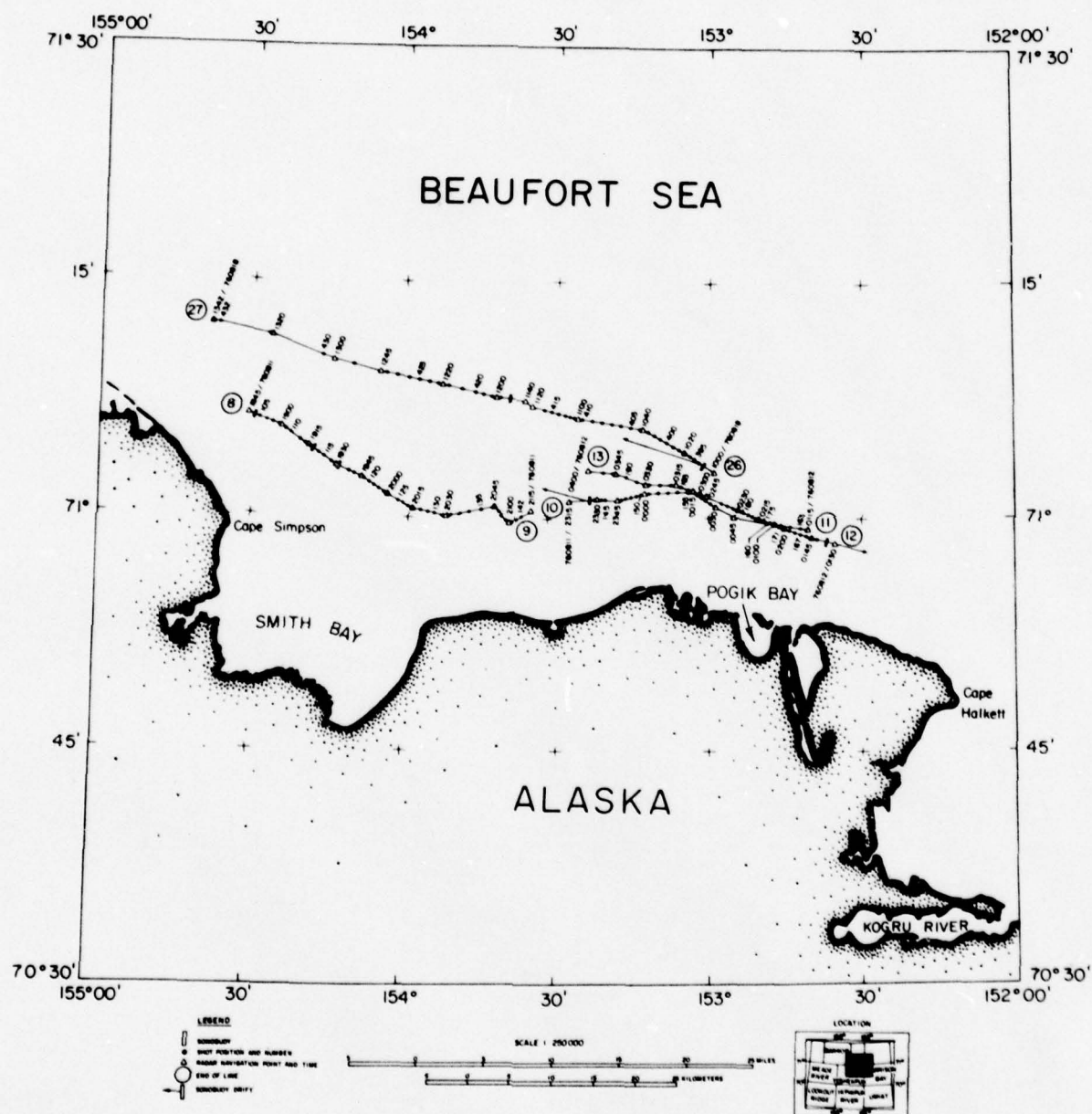


Figure 5. Tracklines and shot locations of Lines 8-9, 10-11, 12-13 and 26-27.

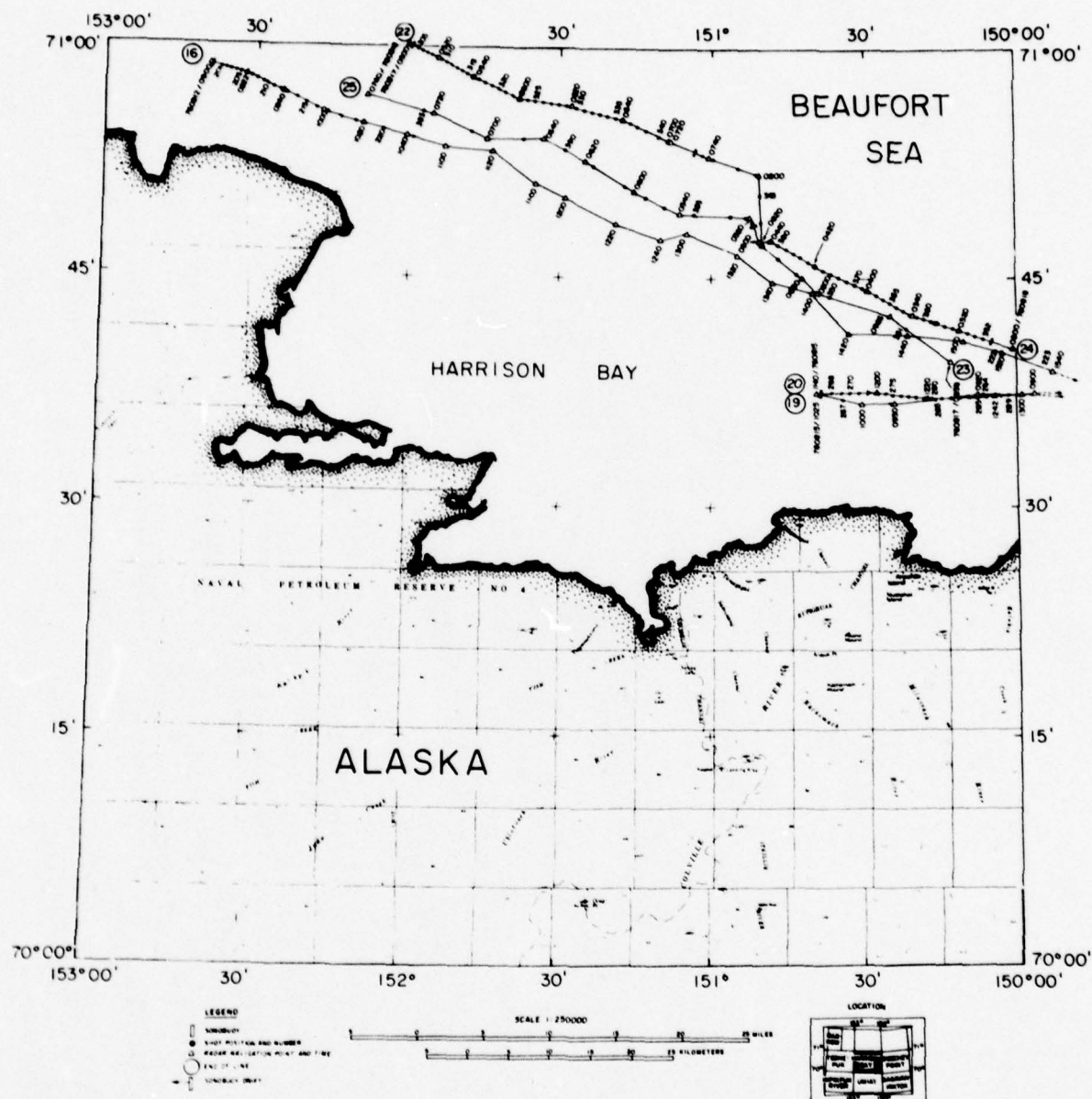


Figure 6. Tracklines and shot locations of Lines 16-17, 18-19 20-21, 22-23 and 24-25.

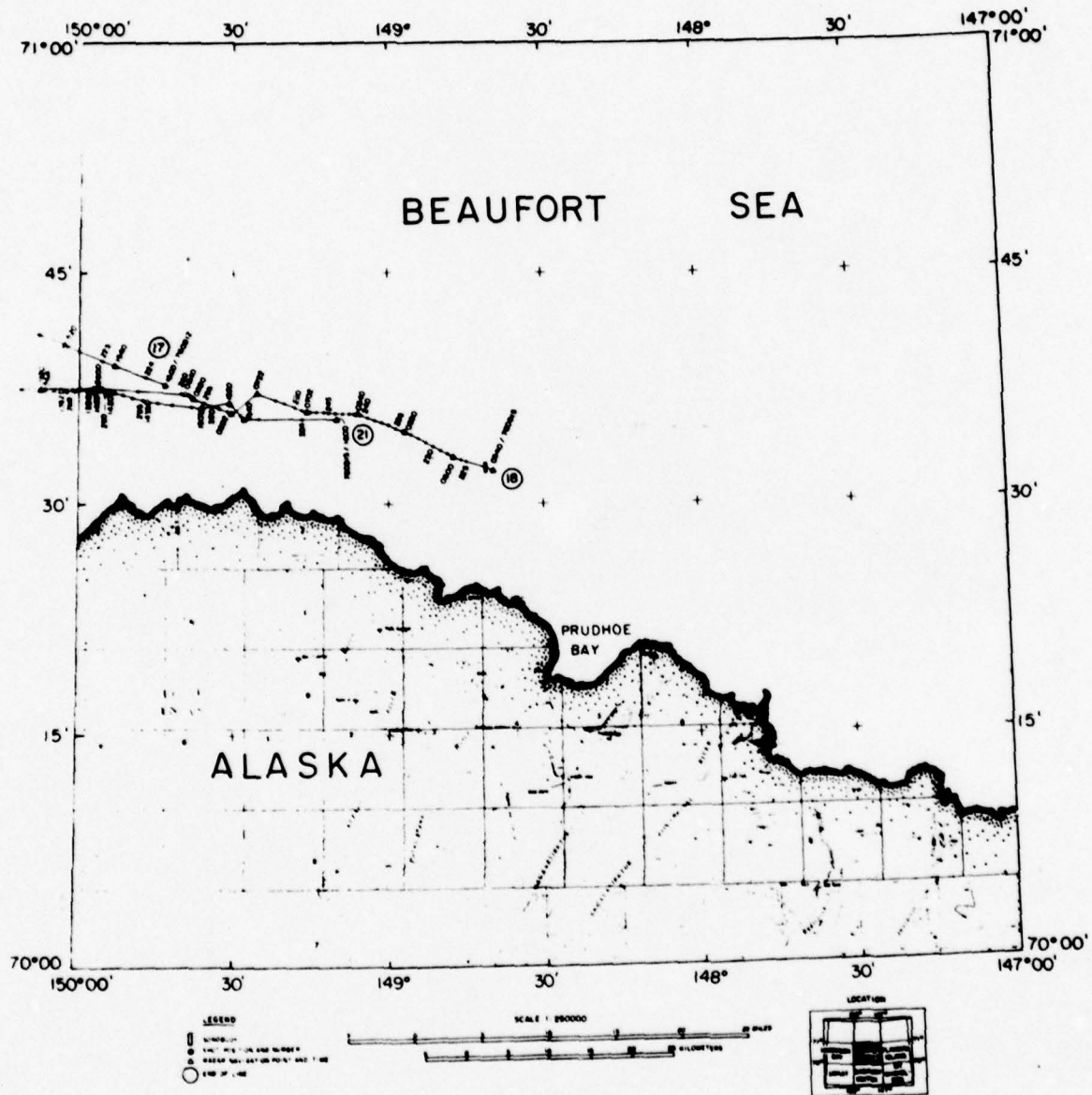


Figure 7. Tracklines and shot locations of Lines 16-17, 18-19 and 20-21.

II

COMPUTER PROGRAM TO FORM
ARRIVAL TIME CORRECTIONS (TIMCORM)
AND INPUT AND OUTPUT FILES
FOR ALL LINES


```

PROGRAM TIMCORN
DIMENSION G(22),GC(22),A(11),R(4)
READ(5,5)AID1,AID2
5 FORMAT(2A8)
6 READ(5,10)DBRM,DBBM,DBEM,TOTS,DRM,V1,SVMS,CLM,SLM,SDM
10 FORMAT(3F5.0,7F5.2)
WRITE(7,14)AID1,AID2
14 FORMAT(2A8)
WRITE(7,16)TOTS,V1
16 FORMAT(15X,F5.2,5X,F5.3)
15 FORMAT(1X,2A9,/)
WRITE(61,15)AID1,AID2
WRITE(61,17)
17 FORMAT(1X DBRM DBBM DBEM TOTS DRM V1 SVMS #,
1XCLM SLM SDM)
WRITE(61,20)DBRM,DBBM,DBEM,TOTS,DRM,V1,SVMS,CLM,SLM,
SDM
20 FORMAT(1X,3F6.0,2F6.2,F6.3,4F6.2)
WRITE(61,25)
25 FORMAT(1X SHOT TIME DISTTS TS TC TCCR G1 G2#,
1X G3 G4 G5 G6)
N=0
ILL=0
30 READ(5,35)ACE,(A11),I=1,11)
35 FORMAT(A5,11F5.0)
IF(EOF(5)) ILL=1
IF(N.EQ.11.AND.ILL.EQ.1) GO TO 40
IF(ILL.EQ.1) CALL EXIT
IF(ACE.EQ.5H99999) GO TO 6
IF(ACE.EQ.5H ) GO TO 135
ITYPE=0
40 IF(ITYPE.EQ.0.AND.N.EQ.0) GO TO 95
D=0+TC
DISTS=0+TS
DO 43 I=1,N
43 R(I)=R(I)+TC
WRITE(7,45)SHOT,ITIM,DBSM,TS,0,(R(I),I=1,N)
45 FORMAT(A5,15,F5.0,15X,6F5.2)
DO 46 I=1,N
G(I)=G(I)+TCCR+TC
46 GC(I)=G(I)+TS
IF(N.GT.11)GO TO 55
WRITE(7,50)(G(I),I=1,N)
50 FORMAT(5X,11F5.2)
GO TO 60
55 WRITE(7,50)(G(I),I=1,11)
WRITE(7,50)(G(I),I=12,N)
50 KN=N
IF(N.GT.6)KN=5
WRITE(61,65)SHOT,ITIM, DISTS,TS,TC,TCCR,(GC(I),I=1,KN)
IF (KN.EQ.N) GO TO 90
65 FORMAT(1X, A5,15,10F6.2)
KN=7
70 IF(N.GT.KN+6) GO TO 75
KN=N
GO TO 80
75 KN=KN+5
80 WRITE(61,85)(GC(I),I=KN,KN)
85 FORMAT(1X,34X,6F6.2)
IF(KN.EQ.N)GO TO 90
KN=KN+5
GO TO 70

```

```

90 IF(ILL.EQ.1) CALL EXIT
IF(N.EQ.11) GO TO 94
N=0
GO TO 30
94 N=0
95 SHOT=ACE $ ITIM=A(1) $ DBSM=A(2) $ V2=A(3) $ VJ=A(4)
RT=A(5) $ TS=A(6) $ TD=A(7)
NR=0
DO 100 I=1,4
RTI=A(I+7)
IF(RTI.EQ.0.) GO TO 105
100 NR=I
105 S1=SQR(1.-V1*V1/VJ/VJ)/V1
S2=SQR(1.-V1*V1/V2/V2)/V1
SX=RT*SVMS
SY=-40.54+1.513*RT
IF(SY.GT.DBSM) SY=DBSM
IF(SX.GT.CL) GO TO 110
TC=SQR((SX-CL)**2+(SY-SM)**2)*.001/V1
GO TO 120
110 TLM=CL+SLM
IF(SX.GT.TLM) GO TO 115
WY=SM-SY
TC=ABS(WY)*.001/V1
GO TO 120
115 TC=SQR((SX-TLM)**2+(SY-SM)**2)*.001/V1
120 CONTINUE
ANG=ASINF(V1/VJ)
OFFSET=DBSM*TANF(ANG)*.001/V1
OMS=OBHM*(DBEM-OBHM)*(D+TS+TC-OFFSET)/TOTS
OFFSET=OBHM*TANF(ANG)*.001/V1
OMS=OBHM*(DBEM-OBHM)*OFFSET/TOTS
C=(DMR-OBHM+OMS-DBSM)*.001
IF(V2.NE.VJ) GO TO 125
DT1=(SY+OMS)*S2*.001
DT2=C*S2
GO TO 130
125 S3=SQR(1.-V2*V2/VJ/VJ)/V2
DT1=(SY+OMS)*.001*S1
DT2=C*(S1-S3)
130 CONTINUE
TCOR=DT1+DT2
ITYPE=1
GO TO 30
135 NS=1
IF(N.EQ.11) NS=12
I=1
140 G(NS)=A(I)
IF(G(NS).EQ.0) GO TO 40
N=NS
IF(N.EQ.11) GO TO 30
IF(N.EQ.22) GO TO 40
NS=NS+1
I=I+1
GO TO 140
END

```

INPUT FORMAT FOR PROGRAM TIMCORR

| A1D1 | | A1D2 | | | | | | | | | |
|------|------|------|------|------|------|------|------|------|------|------|------|
| DBBM | DBBM | DBBM | DBBM | DBBM | DBBM | DBBM | DBBM | DBBM | DBBM | DBBM | DBBM |
| SHOT | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM |
| | G1 | G2 | G3 | G4 | G5 | G6 | G7 | G8 | G9 | G10 | |
| SHOT | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM | ITIM |

A1D1, A1D2 : Line identification

- DBBM : Depth to bottom at the receiver in meters; offset depth based on some average basement velocity.
- DBBM : Depth to bottom at the beginning of the line in meters; DBBM and DBEM establish the reference slope.
- DBEM : Depth to bottom at the end of the line in meters.
- TOTS : Water wave travel time at most distant shot (total direct time in seconds with corrections).
- DHM : Depth of the receiver in meters (hydrophone depth).
- V1 : Velocity of the water layer in km/s.
- SVMS : Ship's velocity in meters per seconds.
- CLM : Cable length in meters.
- SLM : Streamer length (active section only) in meters.
- SDM : Streamer depth in meters.
- SHOT : Shot number.
- ITIM : Time of shot.
- DBSH : Depth to the bottom at the shot point in meters. This should be the offset depth.
- V2 : Velocity of the uppermost earth layer (usually sediment) in km/s.
- V3 : Apparent velocity of waves for this shot; taken from apparent velocity of line on which this point lies.
- BT : Burn time in seconds.
- TS : Seismogram time correction. Time in seconds between shot break and zeroth second tlc.
- D : Direct water wave travel time from zeroth second.
- R1, R2, R3, R4 : Travel time in seconds from zeroth second of waves reflected one, two, three or four times from the bottom.
- G1, G2, ..., G10 : Seismic travel times from zeroth second.

OUTPUT FORMAT FOR PROGRAM TIMECORR

| AI01 | AI02 | DBBM | DBEM | TOTS | TC | DM | VI | SVMS | G1 | G2 | CLM | G3 | SLM | G4 | SDM | G5 | G6 |
|------|------|------|------|------|----|----|----|------|----|----|-----|----|-----|----|-----|----|----|
| SHOT | TIME | SHOT | TIME | TS | TC | DM | VI | SVMS | G1 | G2 | CLM | G3 | SLM | G4 | SDM | G5 | G6 |

AI01, AI02, DBBM, DBEM, TOTS, DM, VI, SVMS, CLM, SLM, SDM, SHOT, TIME : All the same as in input file.

TS : Seismogram time correction : time in seconds between shot break and zeroth second ttc.

TC : Shot instant correction due to separation of shot and streamer.

TCOR : Surface and bottom corrections at shot and receiver.

DISTS : Corrected direct water wave travel time (includes TS and TC).

G1, G2, ..., G6 : Corrected ground wave travel times (include TS, TC and TCOR).

| RURTON ISL 1-2 | | | | | | | | | |
|----------------|------|-------|--------|----------|---------|-------|------|--|--|
| 37 | 40 | 40.10 | 3010.3 | 1.44 | 4.7961 | 4.57 | 1. | | |
| 1 | 2245 | 37. | 3.13 | 3.1348 | .70 | .56 | | | |
| 2 | 2248 | 37. | 3.13 | 3.1337.5 | .42 | 1.50 | | | |
| 3 | 2251 | 37. | 3.13 | 3.1348.6 | .86 | 1.68 | | | |
| 4 | 2254 | 37. | 3.13 | 3.7447.6 | .97 | 2.19 | | | |
| 5 | 2257 | 37. | 3.13 | 3.7445.6 | .89 | 2.85 | | | |
| 6 | 2300 | 37. | 3.13 | 3.7448.0 | .65 | 3.73 | | | |
| 7 | 2303 | 37. | 3.13 | 3.7446.1 | .51 | 4.44 | | | |
| 8 | 2306 | 37. | 3.13 | 3.7448.0 | .57 | 4.94 | | | |
| 9 | 2310 | 37. | 3.13 | 3.7445.2 | .48 | 5.79 | | | |
| 11 | 2316 | 37. | 3.13 | 5.4346.6 | .23 | 7.20 | | | |
| 12 | 2319 | 37. | 3.13 | 5.4345.8 | .88 | 7.15 | | | |
| 13 | 2322 | 37. | 3.13 | 5.4346.8 | .92 | 7.71 | | | |
| 14 | 2325 | 37. | 3.13 | 5.4347. | .87 | 7.48 | | | |
| 15 | 2328 | 37. | 3.13 | 5.4348.9 | .23 | 9.65 | | | |
| 16 | 2331 | 37. | 3.13 | 5.4345.5 | .47 | 11.09 | | | |
| 99999 | 37. | 3.56 | 3.98 | 4.68 | 5.94 | 6.27 | 6.45 | | |
| RURTON ISL 1-2 | | | | | | | | | |
| 37 | 40. | 40.10 | 3010.3 | 1.44 | 2.7361. | 4.57 | 1. | | |
| 17 | 0110 | 28. | 3.13 | 5.4347.1 | .68 | 13.31 | | | |
| 18 | 0113 | 28. | 3.13 | 5.4347.5 | .70 | 13.85 | | | |
| 19 | 0116 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 20 | 0119 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 21 | 0122 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 22 | 0125 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 23 | 0128 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 24 | 0131 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 25 | 0134 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 26 | 0137 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 27 | 0140 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |

| RURTON ISL 1-2 CORRECTED | | | | | | | | | |
|--------------------------|------|-------|--------|----------|------|-------|------|------|--|
| 37 | 40 | 40.10 | 3010.3 | 1.44 | 4.79 | 61.00 | 4.57 | 1.00 | |
| 1 | 2245 | 37. | 3.13 | 3.1348 | .70 | .56 | | | |
| 2 | 2248 | 37. | 3.13 | 3.1337.5 | .42 | 1.50 | | | |
| 3 | 2251 | 37. | 3.13 | 3.1348.6 | .86 | 1.68 | | | |
| 4 | 2254 | 37. | 3.13 | 3.7447.6 | .97 | 2.19 | | | |
| 5 | 2257 | 37. | 3.13 | 3.7445.6 | .89 | 2.85 | | | |
| 6 | 2300 | 37. | 3.13 | 3.7448.0 | .65 | 3.73 | | | |
| 7 | 2303 | 37. | 3.13 | 3.7446.1 | .51 | 4.44 | | | |
| 8 | 2306 | 37. | 3.13 | 3.7448.0 | .57 | 4.94 | | | |
| 9 | 2310 | 37. | 3.13 | 3.7445.2 | .48 | 5.79 | | | |
| 11 | 2316 | 37. | 3.13 | 5.4346.6 | .23 | 7.20 | | | |
| 12 | 2319 | 37. | 3.13 | 5.4345.8 | .88 | 7.15 | | | |
| 13 | 2322 | 37. | 3.13 | 5.4346.8 | .92 | 7.71 | | | |
| 14 | 2325 | 37. | 3.13 | 5.4347. | .87 | 7.48 | | | |
| 15 | 2328 | 37. | 3.13 | 5.4348.9 | .23 | 9.65 | | | |
| 16 | 2331 | 37. | 3.13 | 5.4345.5 | .47 | 11.09 | | | |
| 99999 | 37. | 3.56 | 3.98 | 4.68 | 5.94 | 6.27 | 6.45 | | |
| RURTON ISL 1-2 | | | | | | | | | |
| 37 | 40 | 40.10 | 3010.3 | 1.44 | 2.73 | 61.00 | 4.57 | 1.00 | |
| 17 | 0110 | 28. | 3.13 | 5.4347.1 | .68 | 13.31 | | | |
| 18 | 0113 | 28. | 3.13 | 5.4347.5 | .70 | 13.85 | | | |
| 19 | 0116 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 20 | 0119 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 21 | 0122 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 22 | 0125 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 23 | 0128 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 24 | 0131 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 25 | 0134 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 26 | 0137 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |
| 27 | 0140 | 28. | 3.13 | 5.4347.5 | .25 | 14.21 | | | |

| BURTON ISL 3-4 | | | | | | | | | | BURTON ISL 3-4 CORRECTED | | | | | | | | | |
|----------------|-------|--------|---------|-----|-----|-----|-----|-----|-----|--------------------------|-------|--------|---------|-----|-----|-----|-----|-----|-----|
| DATE | DRM | DRM | DRM | DRM | DRM | DRM | DRM | DRM | DRM | DATE | DRM | DRM | DRM | DRM | DRM | DRM | DRM | DRM | DRM |
| 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 |
| 57.19.3018.3 | 1.44 | 4.9661 | 4.57 1. | | | | | | | 57.19.3018.3 | 1.44 | 4.9661 | 4.57 1. | | | | | | |
| 2.93 2.9339.0 | .73 | .10 | | | | | | | | 2.93 2.9339.0 | .73 | .10 | | | | | | | |
| 2.93 2.9342.5 | .08 | 1.23 | | | | | | | | 2.93 2.9342.5 | .08 | 1.23 | | | | | | | |
| 2.93 2.9344.0 | .20 | 1.71 | | | | | | | | 2.93 2.9344.0 | .20 | 1.71 | | | | | | | |
| 2.93 2.9346.0 | .40 | 2.05 | | | | | | | | 2.93 2.9346.0 | .40 | 2.05 | | | | | | | |
| 2.93 2.9348.0 | .60 | 2.39 | | | | | | | | 2.93 2.9348.0 | .60 | 2.39 | | | | | | | |
| 2.93 2.9350.0 | .80 | 2.73 | | | | | | | | 2.93 2.9350.0 | .80 | 2.73 | | | | | | | |
| 2.93 2.9352.0 | 1.00 | 3.07 | | | | | | | | 2.93 2.9352.0 | 1.00 | 3.07 | | | | | | | |
| 2.93 2.9354.0 | 1.20 | 3.41 | | | | | | | | 2.93 2.9354.0 | 1.20 | 3.41 | | | | | | | |
| 2.93 2.9356.0 | 1.40 | 3.75 | | | | | | | | 2.93 2.9356.0 | 1.40 | 3.75 | | | | | | | |
| 2.93 2.9358.0 | 1.60 | 4.09 | | | | | | | | 2.93 2.9358.0 | 1.60 | 4.09 | | | | | | | |
| 2.93 2.9360.0 | 1.80 | 4.43 | | | | | | | | 2.93 2.9360.0 | 1.80 | 4.43 | | | | | | | |
| 2.93 2.9362.0 | 2.00 | 4.77 | | | | | | | | 2.93 2.9362.0 | 2.00 | 4.77 | | | | | | | |
| 2.93 2.9364.0 | 2.20 | 5.11 | | | | | | | | 2.93 2.9364.0 | 2.20 | 5.11 | | | | | | | |
| 2.93 2.9366.0 | 2.40 | 5.45 | | | | | | | | 2.93 2.9366.0 | 2.40 | 5.45 | | | | | | | |
| 2.93 2.9368.0 | 2.60 | 5.79 | | | | | | | | 2.93 2.9368.0 | 2.60 | 5.79 | | | | | | | |
| 2.93 2.9370.0 | 2.80 | 6.13 | | | | | | | | 2.93 2.9370.0 | 2.80 | 6.13 | | | | | | | |
| 2.93 2.9372.0 | 3.00 | 6.47 | | | | | | | | 2.93 2.9372.0 | 3.00 | 6.47 | | | | | | | |
| 2.93 2.9374.0 | 3.20 | 6.81 | | | | | | | | 2.93 2.9374.0 | 3.20 | 6.81 | | | | | | | |
| 2.93 2.9376.0 | 3.40 | 7.15 | | | | | | | | 2.93 2.9376.0 | 3.40 | 7.15 | | | | | | | |
| 2.93 2.9378.0 | 3.60 | 7.49 | | | | | | | | 2.93 2.9378.0 | 3.60 | 7.49 | | | | | | | |
| 2.93 2.9380.0 | 3.80 | 7.83 | | | | | | | | 2.93 2.9380.0 | 3.80 | 7.83 | | | | | | | |
| 2.93 2.9382.0 | 4.00 | 8.17 | | | | | | | | 2.93 2.9382.0 | 4.00 | 8.17 | | | | | | | |
| 2.93 2.9384.0 | 4.20 | | | | | | | | | 2.93 2.9384.0 | 4.20 | | | | | | | | |
| 2.93 2.9386.0 | 4.40 | | | | | | | | | 2.93 2.9386.0 | 4.40 | | | | | | | | |
| 2.93 2.9388.0 | 4.60 | | | | | | | | | 2.93 2.9388.0 | 4.60 | | | | | | | | |
| 2.93 2.9390.0 | 4.80 | | | | | | | | | 2.93 2.9390.0 | 4.80 | | | | | | | | |
| 2.93 2.9392.0 | 5.00 | | | | | | | | | 2.93 2.9392.0 | 5.00 | | | | | | | | |
| 2.93 2.9394.0 | 5.20 | | | | | | | | | 2.93 2.9394.0 | 5.20 | | | | | | | | |
| 2.93 2.9396.0 | 5.40 | | | | | | | | | 2.93 2.9396.0 | 5.40 | | | | | | | | |
| 2.93 2.9398.0 | 5.60 | | | | | | | | | 2.93 2.9398.0 | 5.60 | | | | | | | | |
| 2.93 2.9400.0 | 5.80 | | | | | | | | | 2.93 2.9400.0 | 5.80 | | | | | | | | |
| 2.93 2.9402.0 | 6.00 | | | | | | | | | 2.93 2.9402.0 | 6.00 | | | | | | | | |
| 2.93 2.9404.0 | 6.20 | | | | | | | | | 2.93 2.9404.0 | 6.20 | | | | | | | | |
| 2.93 2.9406.0 | 6.40 | | | | | | | | | 2.93 2.9406.0 | 6.40 | | | | | | | | |
| 2.93 2.9408.0 | 6.60 | | | | | | | | | 2.93 2.9408.0 | 6.60 | | | | | | | | |
| 2.93 2.9410.0 | 6.80 | | | | | | | | | 2.93 2.9410.0 | 6.80 | | | | | | | | |
| 2.93 2.9412.0 | 7.00 | | | | | | | | | 2.93 2.9412.0 | 7.00 | | | | | | | | |
| 2.93 2.9414.0 | 7.20 | | | | | | | | | 2.93 2.9414.0 | 7.20 | | | | | | | | |
| 2.93 2.9416.0 | 7.40 | | | | | | | | | 2.93 2.9416.0 | 7.40 | | | | | | | | |
| 2.93 2.9418.0 | 7.60 | | | | | | | | | 2.93 2.9418.0 | 7.60 | | | | | | | | |
| 2.93 2.9420.0 | 7.80 | | | | | | | | | 2.93 2.9420.0 | 7.80 | | | | | | | | |
| 2.93 2.9422.0 | 8.00 | | | | | | | | | 2.93 2.9422.0 | 8.00 | | | | | | | | |
| 2.93 2.9424.0 | 8.20 | | | | | | | | | 2.93 2.9424.0 | 8.20 | | | | | | | | |
| 2.93 2.9426.0 | 8.40 | | | | | | | | | 2.93 2.9426.0 | 8.40 | | | | | | | | |
| 2.93 2.9428.0 | 8.60 | | | | | | | | | 2.93 2.9428.0 | 8.60 | | | | | | | | |
| 2.93 2.9430.0 | 8.80 | | | | | | | | | 2.93 2.9430.0 | 8.80 | | | | | | | | |
| 2.93 2.9432.0 | 9.00 | | | | | | | | | 2.93 2.9432.0 | 9.00 | | | | | | | | |
| 2.93 2.9434.0 | 9.20 | | | | | | | | | 2.93 2.9434.0 | 9.20 | | | | | | | | |
| 2.93 2.9436.0 | 9.40 | | | | | | | | | 2.93 2.9436.0 | 9.40 | | | | | | | | |
| 2.93 2.9438.0 | 9.60 | | | | | | | | | 2.93 2.9438.0 | 9.60 | | | | | | | | |
| 2.93 2.9440.0 | 9.80 | | | | | | | | | 2.93 2.9440.0 | 9.80 | | | | | | | | |
| 2.93 2.9442.0 | 10.00 | | | | | | | | | 2.93 2.9442.0 | 10.00 | | | | | | | | |
| 2.93 2.9444.0 | 10.20 | | | | | | | | | 2.93 2.9444.0 | 10.20 | | | | | | | | |
| 2.93 2.9446.0 | 10.40 | | | | | | | | | 2.93 2.9446.0 | 10.40 | | | | | | | | |
| 2.93 2.9448.0 | 10.60 | | | | | | | | | 2.93 2.9448.0 | 10.60 | | | | | | | | |
| 2.93 2.9450.0 | 10.80 | | | | | | | | | 2.93 2.9450.0 | 10.80 | | | | | | | | |
| 2.93 2.9452.0 | 11.00 | | | | | | | | | 2.93 2.9452.0 | 11.00 | | | | | | | | |
| 2.93 2.9454.0 | 11.20 | | | | | | | | | 2.93 2.9454.0 | 11.20 | | | | | | | | |
| 2.93 2.9456.0 | 11.40 | | | | | | | | | 2.93 2.9456.0 | 11.40 | | | | | | | | |
| 2.93 2.9458.0 | 11.60 | | | | | | | | | 2.93 2.9458.0 | 11.60 | | | | | | | | |
| 2.93 2.9460.0 | 11.80 | | | | | | | | | 2.93 2.9460.0 | 11.80 | | | | | | | | |
| 2.93 2.9462.0 | 12.00 | | | | | | | | | 2.93 2.9462.0 | 12.00 | | | | | | | | |
| 2.93 2.9464.0 | 12.20 | | | | | | | | | 2.93 2.9464.0 | 12.20 | | | | | | | | |
| 2.93 2.9466.0 | 12.40 | | | | | | | | | 2.93 2.9466.0 | 12.40 | | | | | | | | |
| 2.93 2.9468.0 | 12.60 | | | | | | | | | 2.93 2.9468.0 | 12.60 | | | | | | | | |
| 2.93 2.9470.0 | 12.80 | | | | | | | | | 2.93 2.9470.0 | 12.80 | | | | | | | | |
| 2.93 2.9472.0 | 13.00 | | | | | | | | | 2.93 2.9472.0 | 13.00 | | | | | | | | |
| 2.93 2.9474.0 | 13.20 | | | | | | | | | 2.93 2.9474.0 | 13.20 | | | | | | | | |
| 2.93 2.9476.0 | 13.40 | | | | | | | | | 2.93 2.9476.0 | 13.40 | | | | | | | | |
| 2.93 2.9478.0 | 13.60 | | | | | | | | | 2.93 2.9478.0 | 13.60 | | | | | | | | |
| 2.93 2.9480.0 | 13.80 | | | | | | | | | 2.93 2.9480.0 | 13.80 | | | | | | | | |
| 2.93 2.9482.0 | 14.00 | | | | | | | | | 2.93 2.9482.0 | 14.00 | | | | | | | | |
| 2.93 2.9484.0 | 14.20 | | | | | | | | | 2.93 2.9484.0 | 14.20 | | | | | | | | |
| 2.93 2.9486.0 | 14.40 | | | | | | | | | 2.93 2.9486.0 | 14.40 | | | | | | | | |
| 2.93 2.9488.0 | 14.60 | | | | | | | | | 2.93 2.9488.0 | 14.60 | | | | | | | | |
| 2.93 2.9490.0 | 14.80 | | | | | | | | | 2.93 2.9490.0 | 14.80 | | | | | | | | |
| 2.93 2.9492.0 | 15.00 | | | | | | | | | 2.93 2.9492.0 | 15.00 | | | | | | | | |
| 2.93 2.9494.0 | 15.20 | | | | | | | | | 2.93 2.9494.0 | 15.20 | | | | | | | | |
| 2.93 2.9496.0 | 15.40 | | | | | | | | | 2.93 2.9496.0 | 15.40 | | | | | | | | |
| 2.93 2.9498.0 | 15.60 | | | | | | | | | 2.93 2.9498.0 | 15.60 | | | | | | | | |
| 2.93 2.9500.0 | 15.80 | | | | | | | | | 2.93 2.9500.0 | 15.80 | | | | | | | | |
| 2.93 2.9502.0 | 16.00 | | | | | | | | | 2.93 2.9502.0 | 16.00 | | | | | | | | |
| 2.93 2.9504.0 | 16.20 | | | | | | | | | 2.93 2.9504.0 | 16.20 | | | | | | | | |
| 2.93 2.9506.0 | 16.40 | | | | | | | | | 2.93 2.9506.0 | 16.40 | | | | | | | | |
| 2.93 2.9508.0 | 16.60 | | | | | | | | | 2.93 2.9508.0 | 16.60 | | | | | | | | |
| 2.93 2.9510.0 | 16.80 | | | | | | | | | 2.93 2.9510.0 | 16.80 | | | | | | | | |
| 2.93 2.9512.0 | 17.00 | | | | | | | | | 2.93 2.9512.0 | 17.00 | | | | | | | | |
| 2.93 2.9514.0 | 17.20 | | | | | | | | | 2.93 2.9514.0 | 17.20 | | | | | | | | |
| 2.93 2.9516.0 | 17.40 | | | | | | | | | 2.93 2.9516.0 | 17.40 | | | | | | | | |
| 2.93 2.9518.0 | 17.60 | | | | | | | | | 2.93 2.9518.0 | 17.60 | | | | | | | | |
| 2.93 2.9520.0 | 17.80 | | | | | | | | | 2.93 2.9520.0 | 17.80 | | | | | | | | |
| 2.93 2.9522.0 | 18.00 | | | | | | | | | 2.93 2.9522.0 | 18.00 | | | | | | | | |
| 2.93 2.9524.0 | 18.20 | | | | | | | | | 2.93 2.9524.0 | 18.20 | | | | | | | | |
| 2.93 2.9526.0 | 18.40 | | | | | | | | | 2.93 2.9526.0 | 18.40 | | | | | | | | |
| 2.93 2.9528.0 | 18.60 | | | | | | | | | 2.93 2.9528.0 | 18.60 | | | | | | | | |
| 2.93 2.9530.0 | 18.80 | | | | | | | | | | | | | | | | | | |

| BURTON ISL 4-5 | | | | | | | | | |
|----------------|------|-------|----------------|-------|--------|-----------|------|----|--|
| 52 | 57 | 45 | 19.30 | 18.30 | 1.440 | 4.9661 | 4.57 | 1. | |
| 58 | 0444 | 54 | 2.77 2.7744.0 | | | .65 -1.14 | | | |
| -335 | | | | | | | | | |
| 59 | 0447 | 55 | 2.77 2.7744.3 | | | .81 .43 | | | |
| -116 | | | | | | | | | |
| 60 | 0450 | 56 | 2.77 2.7742.7 | | | .75 1.03 | | | |
| -25 | | | | | | | | | |
| 61 | 0453 | 56 | 2.77 2.7743.0 | | | .17 2.07 | | | |
| .92 | | | | | | | | | |
| 62 | 0456 | 55 | 2.77 3.7847.0 | | | .49 2.59 | | | |
| 1.06 | | | | | | | | | |
| 63 | 0459 | 54 | 2.77 3.7842.5 | | | .90 2.00 | | | |
| .83 | | | | | | | | | |
| 64 | 0502 | 53 | 2.77 3.7844.9 | | | .74 3.69 | | | |
| 1.35 | | | | | | | | | |
| 65 | 0505 | 52 | 2.77 3.7844.0 | | | .49 4.59 | | | |
| 1.85 | | | | | | | | | |
| 66 | 0508 | 51 | 2.77 3.7844.1 | | | .60 5.14 | | | |
| 1.98 | | | | | | | | | |
| 67 | 0511 | 51 | 2.77 3.7848.3 | | | .47 5.09 | | | |
| 2.34 | | | | | | | | | |
| 68 | 0514 | 51 | 2.77 3.7844.1 | | | .52 6.44 | | | |
| 2.50 | | | | | | | | | |
| 69 | 0517 | 51 | 2.77 3.7845.1 | | | .72 6.05 | | | |
| 2.98 | | | | | | | | | |
| 71 | 0523 | 51 | 2.77 3.7847.2 | | | .37 8.41 | | | |
| 1.27 | | | | | | | | | |
| 72 | 0526 | 50 | 2.77 3.7866.5 | | | .90 8.43 | | | |
| 2.86 | | | | | | | | | |
| 73 | 0529 | 49 | 2.77 3.7867.5 | | | .33 9.69 | | | |
| 3.80 | | | | | | | | | |
| 74 | 0534 | 49 | 2.77 4.7867.1 | | | .93 9.71 | | | |
| 4.35 | | | | | | | | | |
| 75 | 0536 | 49 | 2.77 4.7869.5 | | | .47 10.94 | | | |
| 4.86 | | | | | | | | | |
| 76 | 0540 | 49 | 2.77 4.7869.6 | | | .09 12.12 | | | |
| 4.60 | | | | | | | | | |
| 77 | 0545 | 49 | 2.77 4.7869.0 | | | .51 12.94 | | | |
| 5.86 | | | | | | | | | |
| 99999 | | | | | | | | | |
| 57 | 45 | 19.30 | 18.30 | 1.440 | 2.1661 | 4.57 | 1. | | |
| 58 | 0553 | 48 | 2.77 4.78112.7 | | | .38 14.10 | | | |
| 5.20 | | | | | | | | | |
| 79 | 0601 | 46 | 2.77 4.78165.3 | | | .69 14.47 | | | |
| 4.98 | | | | | | | | | |
| 80 | 0609 | 44 | 2.77 4.78166.6 | | | .27 15.63 | | | |
| 5.67 | | | | | | | | | |

BURTON ISL 4-5 CORRECTED

| BURTON ISL 4-5 | | | | | | | | | |
|----------------|-------|-------|-------|-------|-------|------|-------|------|-------|
| DRM | DRBM | DRFM | TOTS | DRM | V1 | SVMS | CLM | SLM | SOM |
| 52 | 57 | 45 | 19.30 | 18.30 | 1.440 | 4.96 | 61.00 | 4.57 | 1.00 |
| SHOT TIME | OISTS | | TS | IC | ICOR | G1 | G2 | G3 | G4 |
| 58 | 444 | .62 | .65 | .11 | .03 | .44 | | | G5 |
| 59 | 447 | 1.35 | .81 | .11 | .03 | .79 | | | |
| 60 | 450 | 1.08 | .75 | .10 | .03 | 1.13 | | | |
| 61 | 453 | 2.54 | .37 | .10 | .03 | 1.42 | 1.65 | 2.11 | |
| 62 | 456 | 3.20 | .49 | .12 | .03 | 1.70 | 1.81 | 2.14 | |
| 63 | 459 | 3.88 | .98 | .10 | .03 | 1.94 | 2.11 | 2.31 | 2.48 |
| 64 | 502 | 4.54 | .74 | .11 | .03 | 2.23 | 2.53 | | |
| 65 | 505 | 5.19 | .49 | .11 | .03 | 2.48 | 2.74 | 2.90 | |
| 66 | 508 | 5.85 | .60 | .11 | .03 | 2.72 | 3.02 | 3.16 | 3.47 |
| 67 | 511 | 6.48 | .47 | .12 | .04 | 2.97 | 3.06 | 3.43 | 3.79 |
| 68 | 514 | 7.07 | .52 | .11 | .03 | 3.16 | 3.68 | 4.20 | 4.48 |
| 69 | 517 | 7.68 | .72 | .11 | .03 | 3.84 | 4.51 | | |
| 71 | 523 | 8.97 | .37 | .19 | .05 | 3.88 | 4.41 | 4.81 | 5.21 |
| 72 | 526 | 9.60 | .98 | .19 | .05 | 4.07 | 4.56 | 5.01 | 5.49 |
| 73 | 529 | 10.21 | .33 | .19 | .05 | 4.37 | 4.75 | 5.27 | 5.88 |
| 74 | 534 | 10.83 | .43 | .19 | .05 | 5.52 | 5.84 | 6.22 | 6.73 |
| 75 | 536 | 11.69 | .47 | .28 | .05 | 4.86 | 5.45 | 6.08 | 6.75 |
| 76 | 540 | 12.50 | .09 | .29 | .05 | 5.02 | 5.70 | 6.67 | 7.22 |
| 77 | 545 | 13.53 | .31 | .28 | .05 | 6.50 | 7.14 | 7.78 | 8.44 |
| BURTON ISL 4-5 | | | | | | | | | |
| DRM | DRBM | DRFM | TOTS | DRM | V1 | SVMS | CLM | SLM | SOM |
| 52 | 57 | 45 | 19.30 | 18.30 | 1.440 | 2.16 | 61.00 | 4.57 | 1.00 |
| SHOT TIME | OISTS | | TS | IC | ICOR | G1 | G2 | G3 | G4 |
| 78 | 553 | 14.62 | .38 | .14 | .05 | 5.76 | 6.38 | 7.11 | 7.58 |
| 79 | 601 | 15.36 | .44 | .20 | .04 | 5.92 | 6.96 | 7.61 | 8.61 |
| 80 | 609 | 16.11 | .27 | .21 | .04 | 6.19 | 7.15 | 8.27 | 9.15 |
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| AURTON ISL 6-7 | | | | | | | | | |
|---------------------------|-----|---------------|-----------|---------|------------|-----|-----|----|----|
| 33 | 37 | 37.21-1518.3 | 5.2461.1 | 4.57 1. | 5.24 61.00 | SLM | SDM | | |
| 01 2156 | 32 | 2.70 2.7042.0 | -12 1.04 | | | | | | |
| SHOE TIME DISIS | | | | | | | | | |
| 33 | 37 | 37 21.15 | IS | IC | ICOP | G1 | G2 | G3 | G4 |
| AURTON ISL 6-7 CORRELATED | | | | | | | | | |
| 01 2156 | 32 | 2.70 2.7041.0 | -56 1.00 | | | | | | |
| 02 2159 | 33 | 2.70 2.7041.0 | -56 1.00 | | | | | | |
| 03 2202 | 34 | 2.70 3.7143.3 | .16 2.09 | | | | | | |
| 04 2205 | 34 | 2.70 3.7143.5 | -00 2.04 | | | | | | |
| 05 2208 | 35 | 2.70 3.7144.3 | .20 3.33 | | | | | | |
| 06 2211 | 36 | 2.70 3.7142.5 | .49 3.76 | | | | | | |
| 07 2214 | 36 | 2.70 3.7142.5 | .52 4.43 | | | | | | |
| 08 2217 | 37 | 2.70 3.7144.1 | .04 5.55 | | | | | | |
| 09 2220 | 37 | 2.70 3.7145.2 | .41 5.86 | | | | | | |
| 10 2223 | 38 | 2.70 3.7143.9 | .58 6.38 | | | | | | |
| 11 2226 | 40 | 2.70 4.9745.8 | .44 7.20 | | | | | | |
| 12 2229 | 41 | 2.70 4.9746.0 | .42 7.08 | | | | | | |
| 13 2232 | 42 | 2.70 4.9745.7 | .81 6.08 | | | | | | |
| 14 2235 | 43 | 2.70 4.9746.2 | .40 5.31 | | | | | | |
| 15 2238 | 44 | 2.70 4.9747.6 | .40 5.31 | | | | | | |
| 16 2241 | 45 | 2.70 4.9746.2 | .54 6.10 | | | | | | |
| 17 2244 | 46 | 2.70 4.9746.9 | .93 11.44 | | | | | | |
| 18 2247 | 47 | 2.70 4.9746.7 | .94 10.60 | | | | | | |
| 19 2250 | 48 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 20 2253 | 49 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 21 2256 | 50 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 22 2259 | 51 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 23 2302 | 52 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 24 2305 | 53 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 25 2308 | 54 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 26 2311 | 55 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 27 2314 | 56 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 28 2317 | 57 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 29 2320 | 58 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 30 2323 | 59 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 31 2326 | 60 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 32 2329 | 61 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 33 2332 | 62 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 34 2335 | 63 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 35 2338 | 64 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 36 2341 | 65 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 37 2344 | 66 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 38 2347 | 67 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 39 2350 | 68 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 40 2353 | 69 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 41 2356 | 70 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 42 2359 | 71 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 43 2402 | 72 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 44 2405 | 73 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 45 2408 | 74 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 46 2411 | 75 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 47 2414 | 76 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 48 2417 | 77 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 49 2420 | 78 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 50 2423 | 79 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 51 2426 | 80 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 52 2429 | 81 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 53 2432 | 82 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 54 2435 | 83 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 55 2438 | 84 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 56 2441 | 85 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 57 2444 | 86 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 58 2447 | 87 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 59 2450 | 88 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 60 2453 | 89 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 61 2456 | 90 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 62 2459 | 91 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 63 2502 | 92 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 64 2505 | 93 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 65 2508 | 94 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 66 2511 | 95 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 67 2514 | 96 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 68 2517 | 97 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 69 2520 | 98 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 70 2523 | 99 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 71 2526 | 100 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 72 2529 | 101 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 73 2532 | 102 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 74 2535 | 103 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 75 2538 | 104 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 76 2541 | 105 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 77 2544 | 106 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 78 2547 | 107 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 79 2550 | 108 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 80 2553 | 109 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 81 2556 | 110 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 82 2559 | 111 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 83 2602 | 112 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 84 2605 | 113 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 85 2608 | 114 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 86 2611 | 115 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 87 2614 | 116 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 88 2617 | 117 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 89 2620 | 118 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 90 2623 | 119 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 91 2626 | 120 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 92 2629 | 121 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 93 2632 | 122 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 94 2635 | 123 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 95 2638 | 124 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 96 2641 | 125 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 97 2644 | 126 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 98 2647 | 127 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 99 2650 | 128 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 100 2653 | 129 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 101 2656 | 130 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 102 2659 | 131 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 103 2702 | 132 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 104 2705 | 133 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 105 2708 | 134 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 106 2711 | 135 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 107 2714 | 136 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 108 2717 | 137 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 109 2720 | 138 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 110 2723 | 139 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 111 2726 | 140 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 112 2729 | 141 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 113 2732 | 142 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 114 2735 | 143 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 115 2738 | 144 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 116 2741 | 145 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 117 2744 | 146 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 118 2747 | 147 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 119 2750 | 148 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 120 2753 | 149 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 121 2756 | 150 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 122 2759 | 151 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 123 2802 | 152 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 124 2805 | 153 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 125 2808 | 154 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 126 2811 | 155 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 127 2814 | 156 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 128 2817 | 157 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 129 2820 | 158 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 130 2823 | 159 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 131 2826 | 160 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 132 2829 | 161 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 133 2832 | 162 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 134 2835 | 163 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 135 2838 | 164 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 136 2841 | 165 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 137 2844 | 166 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 138 2847 | 167 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 139 2850 | 168 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 140 2853 | 169 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 141 2856 | 170 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 142 2859 | 171 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 143 2902 | 172 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 144 2905 | 173 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 145 2908 | 174 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 146 2911 | 175 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 147 2914 | 176 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 148 2917 | 177 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 149 2920 | 178 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 150 2923 | 179 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 151 2926 | 180 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 152 2929 | 181 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 153 2932 | 182 | 2.70 4.9746.2 | .54 10.15 | | | | | | |
| 154 2935 | | | | | | | | | |

BEAU76 8A-9A

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|------|------|---------|------|----------|-----|------|------|----|
| 13. | 13. | 12.24.5 | 13. | 1.44 | 4.1 | 61. | 4.57 | 1. |
| 105 | 1050 | 13. | 3.07 | 3.0745.3 | -33 | 1.21 | | |
| .86 | | | | | | | | |
| 107 | 1056 | 13. | 3.07 | 3.0745. | -28 | 2.95 | | |
| 108 | 1059 | 13. | 3.07 | 3.0741.9 | -17 | 3.12 | | |
| 109 | 1902 | 13. | 3.07 | 3.0739.1 | -31 | 4.27 | | |
| 111 | 1910 | 13. | 3.07 | 5.6245.3 | -04 | 5.10 | | |
| 112 | 1913 | 13. | 3.07 | 5.6245. | -36 | 5.37 | | |
| 113 | 1916 | 13. | 3.07 | 5.6245.9 | -3 | 5.50 | | |
| 114 | 1920 | 13. | 3.07 | 5.6248. | -17 | 6.44 | | |
| 115 | 1923 | 13. | 3.07 | 5.6248.2 | -41 | 7.46 | | |
| 3.49 | | | | | | | | |

BEAU76 8A-9A COMPLETED

| DNM | UBRM | DRM | TOTS | DRM | V1 | SVMS | CLM | SLM | SDM |
|-----|------|------|-------|-------|-------|------|-------|------|------|
| 13 | 13 | 12 | 24.50 | 13.00 | 1.440 | 4.10 | 61.00 | 4.57 | 1.00 |
| 105 | 1050 | 1.62 | .33 | .08 | .02 | 1.29 | G2 | G3 | G4 |
| 107 | 1056 | 2.75 | -0.28 | .09 | .02 | 1.09 | 2.16 | | |
| 108 | 1059 | 3.36 | .17 | .07 | .02 | 2.18 | 2.62 | | |
| 109 | 1902 | 4.03 | -0.31 | .07 | .02 | 2.50 | 2.92 | 3.29 | |
| 111 | 1910 | 5.44 | -0.04 | .08 | .02 | 2.91 | 3.09 | 3.76 | |
| 112 | 1913 | 5.81 | .36 | .08 | .02 | 3.00 | 3.14 | | |
| 113 | 1916 | 6.37 | .30 | .09 | .02 | 3.24 | 3.49 | 4.12 | |
| 114 | 1920 | 6.76 | -0.17 | .09 | .02 | 3.43 | 3.76 | 4.62 | |
| 115 | 1923 | 7.54 | -0.41 | .09 | .02 | 3.59 | | | |

| BEAUF6 88-9R | | | | | | | | | |
|--------------|------|---------|----------|-----------|---------|--|--|--|--|
| 11 | 13 | 12.24.5 | 13.1.44 | 4.1.61. | 4.57 1. | | | | |
| 119 | 1946 | 12.3.07 | 5.6244.8 | -5.2.72 | | | | | |
| 2.04 | | | | | | | | | |
| 120 | 1949 | 12.3.07 | 5.6244.2 | .38 2.41 | | | | | |
| 1.48 | | | | | | | | | |
| 122 | 1955 | 12.3.07 | 5.6244.4 | .53 3.23 | | | | | |
| 1.73 | | | | | | | | | |
| 123 | 1958 | 12.3.07 | 5.6239.5 | 0.4.21 | | | | | |
| 2.41 | | | | | | | | | |
| 124 | 2008 | 12.3.07 | 5.6245. | .47 3.95 | | | | | |
| 1.96 | | | | | | | | | |
| 125 | 2006 | 12.3.07 | 5.6247.1 | -.34 5.52 | | | | | |
| 3.12 | | | | | | | | | |
| 126 | 2009 | 12.3.07 | 5.6247.7 | .45 5.74 | | | | | |
| 2.47 | | | | | | | | | |
| 128 | 2015 | 11.3.07 | 5.6248.8 | -.11 7.17 | | | | | |
| 3.28 | | | | | | | | | |
| 128 | 2018 | 11.3.07 | 5.6247.7 | -.2 7.98 | | | | | |
| 3.57 | | | | | | | | | |
| 132 | 2031 | 11.3.07 | 5.6243.2 | -.07 9.97 | | | | | |
| 3.94 | | | | | | | | | |
| 133 | 2034 | 11.3.07 | 5.6268. | .1510.25 | | | | | |
| 3.84 | | | | | | | | | |
| 134 | 2037 | 11.3.07 | 5.6276.4 | .0718.83 | | | | | |
| 4.06 | | | | | | | | | |
| 135 | 2041 | 11.3.07 | 5.6271.6 | .1511.41 | | | | | |
| 4.17 | | | | | | | | | |
| 136 | 2045 | 11.3.07 | 5.6273. | .4511.85 | | | | | |
| 3.86 | | | | | | | | | |
| 137 | 2049 | 11.3.07 | 5.6276.5 | .1912.81 | | | | | |
| 4.22 | | | | | | | | | |
| 138 | 2053 | 11.3.07 | 5.6277. | -.1213.82 | | | | | |
| 4.66 | | | | | | | | | |
| 139 | 2057 | 11.3.07 | 5.6276.8 | .3513.55 | | | | | |
| 4.33 | | | | | | | | | |
| 140 | 2101 | 11.3.07 | 5.6276.9 | .0814.92 | | | | | |
| 4.73 | | | | | | | | | |
| 141 | 2105 | 11.3.07 | 5.6276.7 | .5215.18 | | | | | |
| 4.57 | | | | | | | | | |
| 142 | 2109 | 12.3.07 | 5.6273.7 | .2216.14 | | | | | |
| 5.02 | | | | | | | | | |

BEAUF6 88-9R CORRECTED

| BEAUF6 88-9R CORRECTED | | | | | | | | | |
|------------------------|------|-------|-------|-------|-------|------|------|------|------|
| 13 | 13 | 12 | 24.50 | 13.00 | 1.440 | SVMS | CLM | SUM | SDM |
| 119 | 1946 | 2.30 | -0.50 | .08 | .02 | 1.64 | | | |
| 120 | 1949 | 2.87 | .38 | .08 | .02 | 1.96 | | | |
| 122 | 1955 | 3.84 | .53 | .08 | .02 | 2.36 | | | |
| 123 | 1958 | 4.24 | 0 | .07 | .02 | 2.49 | | | |
| 124 | 2008 | 4.59 | .47 | .17 | .02 | 2.62 | 3.53 | | |
| 125 | 2006 | 5.67 | -0.34 | .09 | .02 | 2.89 | 3.41 | 3.49 | |
| 126 | 2009 | 6.28 | .45 | .09 | .02 | 3.03 | 3.18 | 3.66 | 4.05 |
| 128 | 2015 | 7.15 | -0.11 | .09 | .02 | 3.28 | 3.57 | 4.48 | |
| 128 | 2018 | 7.87 | -0.20 | .09 | .02 | 3.48 | 3.77 | 4.17 | 4.72 |
| 132 | 2031 | 9.98 | -0.07 | .08 | .02 | 3.96 | 4.87 | 5.58 | 6.36 |
| 134 | 2037 | 11.07 | .07 | .17 | .02 | 4.15 | 5.75 | 6.56 | |
| 135 | 2041 | 11.72 | .15 | .16 | .02 | 4.32 | 6.46 | | |
| 136 | 2045 | 12.46 | .45 | .16 | .02 | 4.49 | | | |
| 137 | 2049 | 13.17 | .19 | .17 | .02 | 4.60 | 5.12 | 6.17 | 7.02 |
| 138 | 2053 | 13.87 | -0.12 | .17 | .02 | 4.73 | 4.96 | 7.76 | |
| 139 | 2057 | 14.47 | .35 | .17 | .02 | 4.87 | 5.11 | 8.03 | |
| 140 | 2101 | 15.17 | .08 | .17 | .02 | 5.00 | 8.25 | | |
| 141 | 2105 | 15.87 | .52 | .17 | .02 | 5.28 | 5.63 | 6.64 | |
| 142 | 2109 | 16.56 | .22 | .16 | .02 | 5.42 | | | |

| REURS 10-11 | | | |
|-------------|------|--------------------|--------------|
| 12. | 12. | 12.21.7610.3 | 1.44 4.9261. |
| 143 | 2329 | 12. 2.66 2.6639.6 | -31 .60 |
| | -55 | | |
| 145 | 2335 | 12. 2.66 2.6637.4 | -15 1.12 |
| | -92 | | |
| 146 | 2346 | 12. 2.66 2.6638.9 | -01 1.80 |
| | 1.40 | | |
| 147 | 2349 | 12. 2.66 2.6637.1 | -20 2.05 |
| | 1.44 | | |
| 148 | 2352 | 12. 2.66 2.6638.3 | -53 2.44 |
| | 1.49 | | |
| 149 | 2355 | 12. 2.66 2.6639.1 | -19 3.68 |
| | 2.45 | | |
| 150 | 2358 | 12. 2.66 6.4039.3 | -29 4.53 |
| | 2.83 | | |
| 151 | 0001 | 12. 2.66 6.4039.2 | -32 4.54 |
| | 2.37 | 2.64 3.10 3.63 | |
| 152 | 0004 | 12. 2.66 6.4037.3 | -34 5.76 |
| | 3.18 | 3.52 3.90 4.47 | |
| 153 | 0007 | 12. 2.66 6.4045.5 | -14 5.61 |
| | 2.60 | 2.96 3.44 4.07 | |
| 154 | 0010 | 12. 2.66 6.4047.2 | -27 6.43 |
| | 2.83 | 3.12 3.70 4.54 | |
| 155 | 0013 | 12. 2.66 6.4046.6 | -26 7.58 |
| | 3.44 | 3.86 4.44 5.16 | |
| 156 | 0017 | 12. 2.66 6.4047.7 | -40 7.62 |
| | 2.92 | 3.50 4.04 4.97 | |
| 157 | 0020 | 12. 2.66 6.4045.5 | -30 9.0 |
| | 3.82 | 4.39 5.21 5.96 | |
| 158 | 0023 | 12. 2.66 6.4041.7 | -13 5.48 |
| | 3.79 | 4.33 5.29 6.0 | |
| 159 | 0026 | 12. 2.66 6.4073.0 | -08 5.87 |
| | 3.63 | 4.32 5.38 6.08 | |
| 160 | 0057 | 12. 2.66 6.4075.2 | -3916.00 |
| | 4.86 | | |
| 161 | 0102 | 12. 2.66 6.40117.5 | -4318.11 |
| | 8.55 | | |
| 162 | 0106 | 12. 2.66 6.40114.5 | -1115.54 |
| | 5.55 | | |
| 163 | 0111 | 12. 2.66 6.40140.1 | -4026.37 |
| | 6.46 | | |

| REF: AUG 6 10-11 CORRECTED | | | | | | | | | |
|----------------------------|------|-------|-------|------|-------|-------|------|------|------|
| DRAM | DRAM | DRAM | DRAM | DRAM | DRAM | DRAM | DRAM | DRAM | DRAM |
| 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| SHOT | TIME | TIME | TIME | TIME | TIME | TIME | TIME | TIME | TIME |
| 143 | 2329 | 1.38 | -0.31 | 0.09 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 145 | 2335 | 1.35 | 0.15 | 0.04 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 146 | 2346 | 1.90 | 0.01 | 0.09 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 147 | 2349 | 2.41 | 0.28 | 0.04 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 148 | 2352 | 3.06 | 0.53 | 0.09 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 149 | 2355 | 3.58 | -0.19 | 0.09 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 150 | 2358 | 4.13 | -0.24 | 0.09 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 151 | 1 | 4.45 | 0.32 | 0.09 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 152 | 4 | 5.48 | -0.34 | 0.08 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 153 | 7 | 6.06 | 0.34 | 0.11 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 154 | 10 | 6.42 | 0.27 | 0.12 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 155 | 13 | 7.43 | -0.26 | 0.11 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 156 | 17 | 8.22 | 0.48 | 0.12 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 157 | 20 | 8.81 | -0.30 | 0.11 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 158 | 23 | 9.45 | -0.13 | 0.10 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 159 | 26 | 10.15 | 0.08 | 0.20 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 160 | 57 | 17.40 | 0.39 | 0.21 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 161 | 102 | 18.90 | 0.43 | 0.36 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 162 | 106 | 20.00 | 0.11 | 0.35 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |
| 163 | 111 | 21.28 | 0.48 | 0.43 | -0.02 | 1.440 | 0.35 | 0.09 | 0.05 |

| BEAU76 12-13 | | | | | | | | | |
|--------------|------|----------|------|-----------|-----------|------|----|--|--|
| 12. | 12. | 15.22.96 | 18.3 | 1.44 | 4.0861. | 4.57 | 1. | | |
| 164 | 0142 | 12. | 2.65 | 2.6537.2 | -07 | .49 | | | |
| | | .74 | | | | | | | |
| 165 | 0145 | 12. | 2.65 | 2.6538.9 | -02 | 1.34 | | | |
| | | 1.15 | | | | | | | |
| 166 | 0148 | 11. | 2.65 | 2.6540.1 | -04 | 1.87 | | | |
| | | 1.58 | | | | | | | |
| 167 | 0151 | 11. | 2.65 | 2.6542.5 | .57 | 1.80 | | | |
| | | 1.20 | 1.87 | | | | | | |
| 168 | 0154 | 11. | 2.65 | 2.6546.7 | .06 | 2.72 | | | |
| | | 1.94 | | | | | | | |
| 169 | 0157 | 10. | 2.65 | 2.6547.7 | .53 | 2.87 | | | |
| | | 1.77 | 2.38 | | | | | | |
| 171 | 0203 | 11. | 2.65 | 5.8848.0 | .69 | 3.77 | | | |
| | | 2.05 | 2.39 | 2.80 | 3.10 | | | | |
| 172 | 0206 | 11. | 2.65 | 5.8844.5 | .10 | 4.08 | | | |
| | | 2.77 | 3.24 | 1.54 | 4.07 | | | | |
| 173 | 0209 | 11. | 2.65 | 5.8847.1 | -.05 | 5.40 | | | |
| | | 3.02 | 3.47 | 3.75 | 4.12 | 4.53 | | | |
| 175 | 0214 | 12. | 2.65 | 5.8844.9 | .18 | 6.0 | | | |
| | | 3.0 | 3.28 | 3.76 | 4.12 | 4.55 | | | |
| 176 | 0217 | 12. | 2.65 | 5.8847.4 | .65 | 6.07 | | | |
| | | 2.65 | 3.88 | 3.47 | 3.82 | 4.43 | | | |
| 177 | 0220 | 12. | 2.65 | 5.8846.3 | .13 | 7.11 | | | |
| | | 3.32 | 3.61 | 4.11 | 4.61 | 5.03 | | | |
| 178 | 0223 | 12. | 2.65 | 5.8844.2 | -.17 | 8.03 | | | |
| | | 3.76 | 4.16 | 4.58 | 5.30 | 5.68 | | | |
| 179 | 0226 | 13. | 2.65 | 5.8846.4 | .08 | 1.38 | | | |
| | | 3.54 | 4.0 | 4.56 | 5.05 | 5.79 | | | |
| 180 | 0229 | 13. | 2.65 | 5.8845.0 | -.15 | 9.1 | | | |
| | | 4.0 | 4.42 | 4.87 | 5.62 | 6.12 | | | |
| 181 | 0232 | 13. | 2.65 | 5.8873.5 | -.14 | 9.56 | | | |
| | | 4.04 | 4.42 | 4.91 | 5.72 | 6.27 | | | |
| 182 | 0235 | 13. | 2.65 | 5.8871.5 | -.12 | 9.90 | | | |
| | | 2.31 | 4.13 | 5.13 | 5.92 | | | | |
| 183 | 0238 | 13. | 2.65 | 5.8870.0 | .1710.47 | | | | |
| | | 3.41 | | | | | | | |
| 184 | 0307 | 13. | 2.65 | 5.8868.1 | -.0714.91 | | | | |
| | | 4.74 | | | | | | | |
| 185 | 0312 | 13. | 2.65 | 5.8872.5 | -.4916.21 | | | | |
| | | 5.82 | | | | | | | |
| 186 | 0317 | 13. | 2.65 | 5.8872.7 | .6116.17 | | | | |
| | | 4.38 | | | | | | | |
| 188 | 0329 | 13. | 2.65 | 5.88117.5 | .3518.62 | | | | |
| | | 5.0 | | | | | | | |
| 190 | 0340 | 14. | 2.65 | 5.88137.3 | -.2021.13 | | | | |
| | | 6.0 | | | | | | | |
| 191 | 0346 | 14. | 2.65 | 5.88138.1 | .5821.57 | | | | |
| | | 5.45 | | | | | | | |

| BEAU76 12-13 CORRECTED | | | | | | | | | |
|------------------------|------|-------|-------|-------|-------|------|-------|------|------|
| OPRM | DBRM | DBRM | TNTS | ICM | V1 | SVMS | CLM | SLM | SDM |
| 12 | 12 | 15 | 22.96 | 18.50 | 1.440 | 4.08 | 61.00 | 4.57 | 1.00 |
| SHOT | TIME | DISTS | IS | IC | TCOR | G1 | G2 | G3 | G4 |
| 164 | 142 | .88 | -0.07 | .06 | .02 | .75 | | | |
| 165 | 145 | 1.39 | -0.02 | .07 | .02 | 1.21 | | | |
| 166 | 148 | 1.90 | -0.04 | .07 | .02 | 1.55 | | | |
| 167 | 151 | 2.45 | .57 | .08 | .02 | 1.86 | 2.13 | | |
| 168 | 154 | 2.97 | .06 | .09 | .02 | 2.10 | | | |
| 169 | 157 | 3.49 | .53 | .09 | .02 | 2.41 | 3.02 | | |
| 171 | 203 | 4.55 | .69 | .09 | .02 | 2.85 | 3.19 | 3.60 | 3.90 |
| 172 | 206 | 4.98 | .10 | .08 | .02 | 2.97 | 3.44 | 3.74 | 4.27 |
| 173 | 209 | 5.44 | -0.05 | .09 | .02 | 3.08 | 3.53 | 3.81 | 4.18 |
| 175 | 214 | 6.26 | .18 | .08 | .02 | 3.28 | 3.56 | 4.04 | 4.40 |
| 176 | 217 | 6.81 | .65 | .09 | .02 | 3.41 | 3.76 | 4.23 | 4.58 |
| 177 | 220 | 7.31 | .13 | .09 | .02 | 3.56 | 3.85 | 4.35 | 4.85 |
| 178 | 223 | 7.94 | -0.17 | .08 | .02 | 3.69 | 4.09 | 4.51 | 5.23 |
| 179 | 226 | 8.47 | .08 | .09 | .02 | 3.78 | 4.19 | 4.75 | 5.24 |
| 180 | 229 | 9.03 | -0.15 | .08 | .02 | 3.95 | 4.37 | 4.82 | 5.57 |
| 181 | 232 | 9.58 | -0.14 | .16 | .02 | 4.08 | 4.46 | 4.97 | 5.76 |
| 182 | 235 | 9.94 | -0.12 | .16 | .02 | 2.37 | 4.19 | 5.19 | 5.98 |
| 183 | 238 | 10.79 | .17 | .15 | .02 | 4.15 | | | |
| 184 | 307 | 16.99 | -0.07 | .15 | .02 | 4.84 | | | |
| 185 | 312 | 15.88 | -0.49 | .16 | .02 | 5.01 | | | |
| 186 | 317 | 16.84 | .61 | .16 | .02 | 5.17 | | | |
| 188 | 329 | 19.26 | .35 | .29 | .02 | 5.66 | | | |
| 190 | 340 | 21.27 | -0.20 | .34 | .02 | 6.17 | | | |
| 191 | 346 | 22.48 | .58 | .33 | .02 | 6.39 | | | |

| REAUFS 16-17 | | | | | | | | | |
|--------------|-----|---------------|------|---------|---------|--|--|--|--|
| 12. | 12. | 14-20-0512. | 1.44 | 4.9261. | 4.57 1. | | | | |
| 201 0986 | 12. | 1.91 1.9162.9 | .22 | .10 | | | | | |
| 202 0909 | 12. | 1.91 1.9139.1 | .19 | .61 | | | | | |
| 203 0912 | 12. | 1.91 1.9161.2 | .50 | .86 | | | | | |
| 204 0915 | 12. | 1.91 1.9163.7 | .69 | 1.24 | | | | | |
| 205 0918 | 12. | 1.91 1.9164.1 | .47 | 2.13 | | | | | |
| 206 0921 | 12. | 1.91 1.9165.1 | .95 | | | | | | |
| 207 0924 | 12. | 1.91 1.9166.1 | .36 | 2.88 | | | | | |
| 208 0927 | 12. | 1.91 1.9167.1 | .09 | 3.69 | | | | | |
| 209 0930 | 12. | 1.91 1.9168.1 | .55 | 3.80 | | | | | |
| 210 0933 | 12. | 1.91 1.9169.1 | .55 | 3.80 | | | | | |
| 211 0936 | 12. | 1.91 1.9170.1 | .07 | 5.46 | | | | | |
| 212 0939 | 12. | 1.91 1.9171.1 | .07 | 5.46 | | | | | |
| 213 0942 | 12. | 1.91 1.9172.1 | .07 | 5.46 | | | | | |
| 214 0945 | 12. | 1.91 1.9173.1 | .07 | 5.46 | | | | | |
| 215 0948 | 12. | 1.91 1.9174.1 | .07 | 5.46 | | | | | |
| 216 0951 | 12. | 1.91 1.9175.1 | .07 | 5.46 | | | | | |
| 217 0954 | 12. | 1.91 1.9176.1 | .07 | 5.46 | | | | | |
| 218 0957 | 12. | 1.91 1.9177.1 | .07 | 5.46 | | | | | |
| 219 0960 | 12. | 1.91 1.9178.1 | .07 | 5.46 | | | | | |
| 220 0963 | 12. | 1.91 1.9179.1 | .07 | 5.46 | | | | | |
| 221 0966 | 12. | 1.91 1.9180.1 | .07 | 5.46 | | | | | |
| 222 0969 | 12. | 1.91 1.9181.1 | .07 | 5.46 | | | | | |
| 223 0972 | 12. | 1.91 1.9182.1 | .07 | 5.46 | | | | | |
| 224 0975 | 12. | 1.91 1.9183.1 | .07 | 5.46 | | | | | |
| 225 0978 | 12. | 1.91 1.9184.1 | .07 | 5.46 | | | | | |
| 226 0981 | 12. | 1.91 1.9185.1 | .07 | 5.46 | | | | | |
| 227 0984 | 12. | 1.91 1.9186.1 | .07 | 5.46 | | | | | |
| 228 0987 | 12. | 1.91 1.9187.1 | .07 | 5.46 | | | | | |
| 229 0990 | 12. | 1.91 1.9188.1 | .07 | 5.46 | | | | | |
| 230 0993 | 12. | 1.91 1.9189.1 | .07 | 5.46 | | | | | |
| 231 0996 | 12. | 1.91 1.9190.1 | .07 | 5.46 | | | | | |
| 232 0999 | 12. | 1.91 1.9191.1 | .07 | 5.46 | | | | | |
| 233 1002 | 12. | 1.91 1.9192.1 | .07 | 5.46 | | | | | |
| 234 1005 | 12. | 1.91 1.9193.1 | .07 | 5.46 | | | | | |
| 235 1008 | 12. | 1.91 1.9194.1 | .07 | 5.46 | | | | | |
| 236 1011 | 12. | 1.91 1.9195.1 | .07 | 5.46 | | | | | |
| 237 1014 | 12. | 1.91 1.9196.1 | .07 | 5.46 | | | | | |
| 238 1017 | 12. | 1.91 1.9197.1 | .07 | 5.46 | | | | | |
| 239 1020 | 12. | 1.91 1.9198.1 | .07 | 5.46 | | | | | |
| 240 1023 | 12. | 1.91 1.9199.1 | .07 | 5.46 | | | | | |
| 241 1026 | 12. | 1.91 1.9200.1 | .07 | 5.46 | | | | | |
| 242 1029 | 12. | 1.91 1.9201.1 | .07 | 5.46 | | | | | |
| 243 1032 | 12. | 1.91 1.9202.1 | .07 | 5.46 | | | | | |
| 244 1035 | 12. | 1.91 1.9203.1 | .07 | 5.46 | | | | | |
| 245 1038 | 12. | 1.91 1.9204.1 | .07 | 5.46 | | | | | |
| 246 1041 | 12. | 1.91 1.9205.1 | .07 | 5.46 | | | | | |
| 247 1044 | 12. | 1.91 1.9206.1 | .07 | 5.46 | | | | | |
| 248 1047 | 12. | 1.91 1.9207.1 | .07 | 5.46 | | | | | |
| 249 1050 | 12. | 1.91 1.9208.1 | .07 | 5.46 | | | | | |
| 250 1053 | 12. | 1.91 1.9209.1 | .07 | 5.46 | | | | | |
| 251 1056 | 12. | 1.91 1.9210.1 | .07 | 5.46 | | | | | |
| 252 1059 | 12. | 1.91 1.9211.1 | .07 | 5.46 | | | | | |
| 253 1062 | 12. | 1.91 1.9212.1 | .07 | 5.46 | | | | | |
| 254 1065 | 12. | 1.91 1.9213.1 | .07 | 5.46 | | | | | |
| 255 1068 | 12. | 1.91 1.9214.1 | .07 | 5.46 | | | | | |
| 256 1071 | 12. | 1.91 1.9215.1 | .07 | 5.46 | | | | | |
| 257 1074 | 12. | 1.91 1.9216.1 | .07 | 5.46 | | | | | |
| 258 1077 | 12. | 1.91 1.9217.1 | .07 | 5.46 | | | | | |
| 259 1080 | 12. | 1.91 1.9218.1 | .07 | 5.46 | | | | | |
| 260 1083 | 12. | 1.91 1.9219.1 | .07 | 5.46 | | | | | |
| 261 1086 | 12. | 1.91 1.9220.1 | .07 | 5.46 | | | | | |
| 262 1089 | 12. | 1.91 1.9221.1 | .07 | 5.46 | | | | | |
| 263 1092 | 12. | 1.91 1.9222.1 | .07 | 5.46 | | | | | |
| 264 1095 | 12. | 1.91 1.9223.1 | .07 | 5.46 | | | | | |
| 265 1098 | 12. | 1.91 1.9224.1 | .07 | 5.46 | | | | | |
| 266 1101 | 12. | 1.91 1.9225.1 | .07 | 5.46 | | | | | |
| 267 1104 | 12. | 1.91 1.9226.1 | .07 | 5.46 | | | | | |
| 268 1107 | 12. | 1.91 1.9227.1 | .07 | 5.46 | | | | | |
| 269 1110 | 12. | 1.91 1.9228.1 | .07 | 5.46 | | | | | |
| 270 1113 | 12. | 1.91 1.9229.1 | .07 | 5.46 | | | | | |
| 271 1116 | 12. | 1.91 1.9230.1 | .07 | 5.46 | | | | | |
| 272 1119 | 12. | 1.91 1.9231.1 | .07 | 5.46 | | | | | |
| 273 1122 | 12. | 1.91 1.9232.1 | .07 | 5.46 | | | | | |
| 274 1125 | 12. | 1.91 1.9233.1 | .07 | 5.46 | | | | | |
| 275 1128 | 12. | 1.91 1.9234.1 | .07 | 5.46 | | | | | |
| 276 1131 | 12. | 1.91 1.9235.1 | .07 | 5.46 | | | | | |
| 277 1134 | 12. | 1.91 1.9236.1 | .07 | 5.46 | | | | | |
| 278 1137 | 12. | 1.91 1.9237.1 | .07 | 5.46 | | | | | |
| 279 1140 | 12. | 1.91 1.9238.1 | .07 | 5.46 | | | | | |
| 280 1143 | 12. | 1.91 1.9239.1 | .07 | 5.46 | | | | | |
| 281 1146 | 12. | 1.91 1.9240.1 | .07 | 5.46 | | | | | |
| 282 1149 | 12. | 1.91 1.9241.1 | .07 | 5.46 | | | | | |
| 283 1152 | 12. | 1.91 1.9242.1 | .07 | 5.46 | | | | | |
| 284 1155 | 12. | 1.91 1.9243.1 | .07 | 5.46 | | | | | |
| 285 1158 | 12. | 1.91 1.9244.1 | .07 | 5.46 | | | | | |
| 286 1161 | 12. | 1.91 1.9245.1 | .07 | 5.46 | | | | | |
| 287 1164 | 12. | 1.91 1.9246.1 | .07 | 5.46 | | | | | |
| 288 1167 | 12. | 1.91 1.9247.1 | .07 | 5.46 | | | | | |
| 289 1170 | 12. | 1.91 1.9248.1 | .07 | 5.46 | | | | | |
| 290 1173 | 12. | 1.91 1.9249.1 | .07 | 5.46 | | | | | |
| 291 1176 | 12. | 1.91 1.9250.1 | .07 | 5.46 | | | | | |
| 292 1179 | 12. | 1.91 1.9251.1 | .07 | 5.46 | | | | | |
| 293 1182 | 12. | 1.91 1.9252.1 | .07 | 5.46 | | | | | |
| 294 1185 | 12. | 1.91 1.9253.1 | .07 | 5.46 | | | | | |
| 295 1188 | 12. | 1.91 1.9254.1 | .07 | 5.46 | | | | | |
| 296 1191 | 12. | 1.91 1.9255.1 | .07 | 5.46 | | | | | |
| 297 1194 | 12. | 1.91 1.9256.1 | .07 | 5.46 | | | | | |
| 298 1197 | 12. | 1.91 1.9257.1 | .07 | 5.46 | | | | | |
| 299 1200 | 12. | 1.91 1.9258.1 | .07 | 5.46 | | | | | |
| 300 1203 | 12. | 1.91 1.9259.1 | .07 | 5.46 | | | | | |
| 301 1206 | 12. | 1.91 1.9260.1 | .07 | 5.46 | | | | | |
| 302 1209 | 12. | 1.91 1.9261.1 | .07 | 5.46 | | | | | |
| 303 1212 | 12. | 1.91 1.9262.1 | .07 | 5.46 | | | | | |
| 304 1215 | 12. | 1.91 1.9263.1 | .07 | 5.46 | | | | | |
| 305 1218 | 12. | 1.91 1.9264.1 | .07 | 5.46 | | | | | |
| 306 1221 | 12. | 1.91 1.9265.1 | .07 | 5.46 | | | | | |
| 307 1224 | 12. | 1.91 1.9266.1 | .07 | 5.46 | | | | | |
| 308 1227 | 12. | 1.91 1.9267.1 | .07 | 5.46 | | | | | |
| 309 1230 | 12. | 1.91 1.9268.1 | .07 | 5.46 | | | | | |
| 310 1233 | 12. | 1.91 1.9269.1 | .07 | 5.46 | | | | | |
| 311 1236 | 12. | 1.91 1.9270.1 | .07 | 5.46 | | | | | |
| 312 1239 | 12. | 1.91 1.9271.1 | .07 | 5.46 | | | | | |
| 313 1242 | 12. | 1.91 1.9272.1 | .07 | 5.46 | | | | | |
| 314 1245 | 12. | 1.91 1.9273.1 | .07 | 5.46 | | | | | |
| 315 1248 | 12. | 1.91 1.9274.1 | .07 | 5.46 | | | | | |
| 316 1251 | 12. | 1.91 1.9275.1 | .07 | 5.46 | | | | | |
| 317 1254 | 12. | 1.91 1.9276.1 | .07 | 5.46 | | | | | |
| 318 1257 | 12. | 1.91 1.9277.1 | .07 | 5.46 | | | | | |
| 319 1260 | 12. | 1.91 1.9278.1 | .07 | 5.46 | | | | | |
| 320 1263 | 12. | 1.91 1.9279.1 | .07 | 5.46 | | | | | |
| 321 1266 | 12. | 1.91 1.9280.1 | .07 | 5.46 | | | | | |
| 322 1269 | 12. | 1.91 1.9281.1 | .07 | 5.46 | | | | | |
| 323 1272 | 12. | 1.91 1.9282.1 | .07 | 5.46 | | | | | |
| 324 1275 | 12. | 1.91 1.9283.1 | .07 | 5.46 | | | | | |
| 325 1278 | 12. | 1.91 1.9284.1 | .07 | 5.46 | | | | | |
| 326 1281 | 12. | 1.91 1.9285.1 | .07 | 5.46 | | | | | |
| 327 1284 | 12. | 1.91 1.9286.1 | .07 | 5.46 | | | | | |
| 328 1287 | 12. | 1.91 1.9287.1 | .07 | 5.46 | | | | | |
| 329 1290 | 12. | 1.91 1.9288.1 | .07 | 5.46 | | | | | |
| 330 1293 | 12. | 1.91 1.9289.1 | .07 | 5.46 | | | | | |
| 331 1296 | 12. | 1.91 1.9290.1 | .07 | 5.46 | | | | | |
| 332 1299 | 12. | 1.91 1.9291.1 | .07 | 5.46 | | | | | |
| 333 1302 | 12. | 1.91 1.9292.1 | .07 | 5.46 | | | | | |
| 334 1305 | 12. | 1.91 1.9293.1 | .07 | 5.46 | | | | | |
| 335 1308 | 12. | 1.91 1.9294.1 | .07 | 5.46 | | | | | |
| 336 1311 | 12. | 1.91 1.9295.1 | .07 | 5.46 | | | | | |
| 337 1314 | 12. | 1.91 1.9296.1 | .07 | 5.46 | | | | | |
| 338 1317 | 12. | 1.91 1.9297.1 | .07 | 5.46 | | | | | |
| 339 1320 | 12. | 1.91 1.9298.1 | .07 | 5.46 | | | | | |
| 340 1323 | 12. | 1.91 1.9299.1 | .07 | 5.46 | | | | | |
| 341 1326 | 12. | 1.91 1.9300.1 | .07 | 5.46 | | | | | |
| 342 1329 | 12. | 1.91 1.9301.1 | .07 | 5.46 | | | | | |
| 343 1332 | 12. | 1.91 1.9302.1 | .07 | 5.46 | | | | | |
| 344 1335 | 12. | 1.91 1.9303.1 | .07 | 5.46 | | | | | |
| 345 1338 | 12. | 1.91 1.9304.1 | .07 | 5.46 | | | | | |
| 346 1341 | 12. | 1.91 1.9305.1 | .07 | 5.46 | | | | | |
| 347 1344 | 12. | 1.91 1.9306.1 | .07 | 5.46 | | | | | |
| 348 1347 | 12. | 1.91 1.9307.1 | .07 | 5.46 | | | | | |
| 349 1350 | 12. | 1.91 1.9308.1 | .07 | 5.46 | | | | | |
| 350 1353 | 12. | 1.91 1.9309.1 | .07 | 5.46 | | | | | |
| 351 1356 | 12. | 1.91 1.9310.1 | .07 | 5.46 | | | | | |
| 352 1359 | 12. | 1.91 1.9311.1 | .0 | | | | | | |

[illegible]

| | | | | |
|---------------|-------|-------------------|-----------|-----------------|
| 9FAU76 228-23 | | | | |
| 19. | 19. | 20.21.0918.3 | 1.44 | 4.7461. 4.57 1. |
| 305 | 0506 | 19. 2.16 2.1640.8 | .15 | .64 |
| | 58 | | | |
| 306 | 0509 | 19. 2.16 2.1639.9 | .05 | 1.18 |
| | 1.00 | | | |
| 307 | 0512 | 19. 2.16 2.1640.4 | -.12 | 1.96 |
| | 1.72 | | | |
| 308 | 0515 | 19. 2.16 2.1640. | -.54 | 2.57 |
| | 2.18 | | | |
| 309 | 0518 | 19. 2.16 2.1640. | .05 | 2.44 |
| | 1.87 | | | |
| 310 | 0521 | 19. 2.16 2.1639. | .15 | 2.87 |
| | 2.08 | | | |
| 311 | 0524 | 19. 2.16 5.0541.7 | .06 | 3.52 |
| | 2.45 | | | |
| 312 | 0527 | 19. 2.16 5.0540.4 | -.18 | 4.34 |
| | 2.89 | | | |
| 313 | 0530 | 19. 2.16 5.0540.4 | .11 | 4.68 |
| | 2.71 | | | |
| 314 | 0533 | 19. 2.16 5.0539.7 | -.31 | 5.58 |
| | 3.25 | | | |
| 315 | 0536 | 19. 2.16 5.0539.2 | -.17 | 6.02 |
| | 3.25 | | | |
| 316 | 0539 | 19. 2.16 5.0539.3 | .53 | 5.89 |
| | 3.23 | | | |
| 317 | 0542 | 19. 2.16 5.0540. | -.08 | 7.05 |
| | 3.42 | | | |
| 318 | 0545 | 19. 2.16 5.0541.1 | .62 | 7.04 |
| | 2.99 | | | |
| 319 | 0548 | 19. 2.16 5.0542.2 | .31 | 7.65 |
| | 3.20 | | | |
| 320 | 0551 | 19. 2.16 5.0543.1 | .32 | 8.27 |
| | 3.41 | | | |
| 321 | 0554 | 19. 2.16 5.0542.1 | -.22 | 5.39 |
| | 4.05 | | | |
| 322 | 0557 | 19. 2.16 5.0542.9 | .32 | 6.45 |
| | 3.66 | | | |
| 322 | 0600 | 19. 2.16 5.0544.9 | .61 | 5.96 |
| | 3.68 | | | |
| 324 | 0603 | 19. 2.16 5.0542.6 | -.2711.12 | |
| | 4.61 | | | |
| 325 | 0606 | 19. 2.16 5.0544.8 | .41:1.19 | |
| | 4. 5. | | | |
| 326 | 0609 | 19. 2.16 5.0568. | -.1612.15 | |
| | 4.70 | | | |
| 327 | 0612 | 19. 2.16 5.0568.3 | -.1512.56 | |
| | 4.87 | | | |
| 328 | 0615 | 19. 2.16 5.0568.9 | .1813.19 | |
| | 4.72 | | | |
| 330 | 0622 | 19. 2.16 5.0577.7 | -.2514.58 | |
| | 4.93 | | | |

| | | | | |
|---------------|------|--------------------|-----------|-----------------|
| 9FAU76 228-23 | | | | |
| 331 | 0625 | 19. 2.16 5.0582.5 | -.3215.16 | |
| | 5.06 | | | |
| 332 | 0628 | 19. 2.16 5.0581.3 | -.3516.45 | |
| | 5.09 | | | |
| 333 | 0631 | 18. 2.16 5.0578.8 | .0716.65 | |
| | 5.62 | | | |
| 334 | 0634 | 18. 2.16 5.0572.4 | -.1117.49 | |
| | 6.01 | | | |
| 335 | 0637 | 18. 2.16 5.0572.2 | .2817.76 | |
| | 5.8 | | | |
| 336 | 0640 | 18. 2.16 5.0572. | -.2418.39 | |
| | 5.98 | | | |
| 337 | 0643 | 18. 2.16 5.05112.2 | .4218.68 | |
| | 7.07 | | | |
| 338 | 0646 | 19. 2.16 5.05112.4 | .0519.69 | |
| | 6.43 | | | |
| 339 | 0650 | 20. 2.16 5.05166.2 | -.3120.78 | |
| | 6.48 | | | |
| 340 | 0655 | 20. 2.16 5.05134.5 | .4821.89 | |
| | 6.37 | | | |
| 9FAU76 228-23 | | | | |
| 20. | 20. | 20.22.6018.3 | 1.44 | 4.5661. 4.57 1. |
| 341 | 0736 | 20. 1.94 1.94135. | -.62 | .76 |
| | .75 | | | |
| 342 | 0741 | 20. 1.94 1.94135. | .46 | .81 |
| | .44 | | | |
| 343 | 0751 | 20. 1.94 3.36190. | -.14 | 3.28 |
| | 2.21 | | | |
| 344 | 0759 | 20. 1.94 3.36192.3 | .01 | 4.75 |
| | 2.72 | | | |
| 345 | 0805 | 20. 1.94 3.36198.3 | -.29 | 6.48 |
| | 3.43 | | | |
| 346 | 0813 | 20. 1.94 3.36192.9 | .50 | 7.38 |
| | 3.08 | | | |
| 347 | 0820 | 20. 1.94 3.36188.5 | -.07 | 9.67 |
| | 4.14 | | | |
| 348 | 0832 | 20. 1.94 3.36265.7 | -.1810.74 | |
| | 4.10 | | | |
| 349 | 0846 | 19. 1.94 3.36340. | -.1413.29 | |
| | 4.80 | | | |
| 350 | 0904 | 19. 1.94 3.36195.8 | -.1517.44 | |
| | 6.16 | | | |
| 351 | 0929 | 20. 1.94 3.36192.9 | -.4222.60 | |
| | 7.70 | | | |

DEAU76 24A-25

| | | | | |
|-----------|-------------------|-----------|---------|---------|
| 17. 17. | 16.44.63 | 17. 1.44 | 4.0261. | 4.57 1. |
| 352 0311 | 17. 1.99 1.9939.0 | -12 1.27 | | |
| 1.26 | | | | |
| 353 0314 | 17. 1.99 1.9942.2 | -32 1.14 | | |
| 1.01 | | | | |
| 354 0317 | 17. 1.99 1.9940.2 | .03 2.15 | | |
| 1.76 | | | | |
| 355 0320 | 18. 1.99 1.9939.0 | -07 2.03 | | |
| 2.11 2.28 | | | | |
| 356 0323 | 18. 1.99 3.3440.1 | .12 3.21 | | |
| 2.33 2.52 | | | | |
| 357 0326 | 18. 1.99 3.3439.0 | .12 3.22 | | |
| 2.66 2.87 | | | | |
| 358 0329 | 18. 1.99 3.3441.7 | -13 4.65 | | |
| 3.15 3.32 | | | | |
| 359 0332 | 18. 1.99 3.3439.0 | .32 4.04 | | |
| 2.97 3.72 | | | | |
| 360 0335 | 18. 1.99 3.3439.4 | .06 5.7 | | |
| 3.47 4.18 | | | | |
| 361 0338 | 18. 1.99 3.3439.6 | -21 6.4 | | |
| 4.01 4.28 | | | | |
| 362 0341 | 18. 1.99 3.3440.6 | .46 6.56 | | |
| 3.68 5.23 | | | | |
| 363 0344 | 18. 1.99 3.3436.2 | -35 8.03 | | |
| 4.72 5.86 | | | | |
| 364 0347 | 18. 1.99 3.3443.8 | .33 7.91 | | |
| 3.89 6.19 | | | | |
| 365 0350 | 18. 1.99 3.3444.4 | -01 8.91 | | |
| 4.38 5.32 | | | | |
| 366 0353 | 18. 1.99 3.3444.3 | -26 9.74 | | |
| 4.86 5.87 | | | | |
| 367 0356 | 18. 1.99 3.3445. | -95 10.13 | | |
| 4.60 | | | | |
| 368 0359 | 18. 1.99 3.3455.0 | .04 11.55 | | |
| 4.73 6.77 | | | | |
| 369 0402 | 18. 1.99 3.3459. | -30 11.03 | | |
| 5.31 8.97 | | | | |
| 370 0405 | 18. 1.99 3.3450.9 | -20 12.1 | | |
| 5.43 6.04 | | | | |
| 371 0408 | 19. 1.99 3.3472.3 | -33 12.7 | | |
| 5.52 | | | | |
| 372 0411 | 19. 1.99 3.3473.2 | .19 12.83 | | |
| 5.27 8.53 | | | | |
| 373 0414 | 19. 1.99 3.3470.6 | .37 12.26 | | |
| 5.18 9.1 | | | | |
| 374 0417 | 19. 1.99 3.3483.3 | -42 14.6 | | |
| 6.06 7.55 | | | | |
| 375 0420 | 19. 1.99 3.3486.9 | -44 15.3 | | |
| 6.06 | | | | |

| | | |
|-----------|--------------------|-----------|
| 376 0423 | 19. 1.99 3.3484.6 | .04 15.54 |
| 6.07 | | |
| 377 0427 | 19. 1.99 3.3470.7 | .46 15.75 |
| 6.66 | | |
| 378 0430 | 19. 1.99 3.3472.3 | .43 16.28 |
| 5.76 | | |
| 379 0433 | 19. 1.99 3.34110.6 | .05 17.16 |
| 6.45 | | |
| 380 0437 | 18. 1.99 3.34141.3 | -22 18.15 |
| 6.64 7.13 | | |
| 381 0442 | 18. 1.99 3.34133.4 | .15 18.03 |
| 6.72 6.88 | | |
| 382 0517 | 18. 1.99 3.34137.7 | .00 21.70 |
| 7.42 | | |
| 383 0521 | 18. 1.99 3.34138.5 | -13 22.75 |
| 7.07 8.48 | | |
| 384 0525 | 18. 1.99 3.34138.2 | 0. 23.51 |
| 7.52 | | |
| 385 0536 | 18. 1.99 3.34163. | .09 25.56 |
| 8.52 9.21 | | |

DEAU76 24B-25

| | | | | |
|----------|--------------------|-----------|---------|---------|
| 17. 17. | 16.24.60 | 17. 1.44 | 4.0261. | 4.57 1. |
| 383 0521 | 18. 2.27 2.27138.5 | -12 1.31 | | |
| 8.3 | | | | |
| 384 0525 | 18. 2.27 2.27138.2 | .00 2.14 | | |
| 385 0536 | 18. 2.27 6.02163. | .09 4.31 | | |
| 2.40 | | | | |
| 386 0547 | 18. 2.27 6.02192.1 | -04 6.50 | | |
| 3.09 | | | | |
| 387 0555 | 18. 2.27 6.02192.3 | .35 7.77 | | |
| 3.15 | | | | |
| 388 0604 | 18. 2.27 6.02182.7 | .14 9.97 | | |
| 3.84 | | | | |
| 389 0617 | 18. 2.27 6.02200.4 | .06 12.79 | | |
| 4.51 | | | | |
| 390 0630 | 18. 2.27 6.02210. | .05 15.65 | | |
| 5.17 | | | | |
| 391 0647 | 18. 2.27 6.02211.2 | .05 19.35 | | |
| 6.01 | | | | |
| 392 0706 | 16. 2.27 6.02217.8 | -02 23.50 | | |
| 7.14 | | | | |
| 393 0723 | 16. 2.27 6.02313. | .01 24.60 | | |
| 7.69 | | | | |

REFU76 268-278 CORRECTED

| OPRM | DBM | DBM | TOTS | DRM | W1 | SVMS | CLM | SLM | SOM |
|--------------------|------|-------|-------|-------|-------|------|-------|------|------|
| 23 | 23 | 18 | 23.92 | 18.00 | 1.440 | 5.30 | 61.00 | 4.57 | 1.00 |
| SNOT TIME DISIS IS | | | | | | | | | |
| 417 | 1158 | .88 | -0.35 | .25 | .02 | .92 | | | |
| 418 | 1202 | 1.69 | -0.02 | .24 | .02 | 1.51 | | | |
| 419 | 1205 | 2.27 | .03 | .23 | .02 | 1.92 | | | |
| 420 | 1208 | 2.85 | -0.17 | .20 | .02 | 2.25 | | | |
| 421 | 1213 | 4.10 | -0.24 | .40 | .03 | 2.78 | | | |
| 422 | 1218 | 5.16 | -0.58 | .32 | .03 | 3.18 | | | |
| 423 | 1222 | 6.11 | -0.01 | .33 | .03 | 3.51 | | | |
| 424 | 1226 | 7.10 | -0.65 | .44 | .03 | 3.81 | | | |
| 425 | 1230 | 8.04 | -0.73 | .44 | .03 | 4.12 | | | |
| 426 | 1234 | 8.96 | -0.51 | .43 | .03 | 4.50 | | | |
| 427 | 1239 | 10.14 | -0.57 | .42 | .03 | 4.82 | | | |
| 428 | 1243 | 11.03 | -0.22 | .42 | .03 | 5.09 | | | |
| 429 | 1254 | 13.42 | -0.22 | .62 | .02 | 5.64 | | | |
| 430 | 1304 | 15.76 | .17 | .61 | .02 | 6.17 | | | |
| 431 | 1321 | 19.50 | -0.14 | .92 | .02 | 6.97 | | | |
| 432 | 1340 | 23.92 | -0.13 | .92 | .02 | 7.84 | | | |

REFU76 268-278

| 23 | 23 | 18 | 21.9218 | 1.44 | 5.3061 | 4.57 | 1. |
|-----|------|----|----------|-------|--------|------|----|
| 417 | 1158 | 23 | 2.3476.6 | -0.35 | .98 | | |
| 418 | 1202 | 23 | 2.3476.6 | -0.62 | 1.47 | | |
| 419 | 1205 | 22 | 2.3476.0 | .03 | 2.01 | | |
| 420 | 1208 | 22 | 2.3467.8 | -0.17 | 2.62 | | |
| 421 | 1213 | 22 | 2.3476.0 | -0.24 | 3.94 | | |
| 422 | 1218 | 22 | 2.3476.0 | -0.56 | 5.42 | | |
| 423 | 1222 | 22 | 2.3476.0 | -0.01 | 5.79 | | |
| 424 | 1226 | 22 | 2.3476.0 | -0.65 | 7.31 | | |
| 425 | 1230 | 22 | 2.3476.0 | -0.73 | 8.33 | | |
| 426 | 1234 | 21 | 2.3476.0 | -0.51 | 9.04 | | |
| 427 | 1239 | 21 | 2.3476.0 | -0.57 | 10.29 | | |
| 428 | 1243 | 20 | 2.3476.0 | -0.22 | 10.68 | | |
| 429 | 1254 | 19 | 2.3476.0 | -0.22 | 13.82 | | |
| 430 | 1304 | 19 | 2.3476.0 | .17 | 14.98 | | |
| 431 | 1321 | 18 | 2.3476.0 | -0.14 | 18.86 | | |
| 432 | 1340 | 18 | 2.3476.0 | -0.13 | 23.13 | | |

III

COMPUTER PROGRAMS TO
PLOT DATA (REFPLOTT, REDPLOT2)
AND PROGRAM TO COMPUTE
STRUCTURE (MULTLAY)


```

PROGRAM REFPLOTT
DIMENSION XAXIS(5),YAXIS(3),SHOT(1),AT(11),R(4)
INTEGER PLOTEND,PSUP,PSDOWN,PENUP,PENDOWN
PLOTEND=-3 $ PSUP=-1 $ PSDOWN=-2
PENUP=3 $ PENDOWN=2
XAXIS(1)=8HDISTANCE
XAXIS(2)=9H 2 SEC P
XAXIS(3)=8HER INCH
YAXIS(1)=8HTIME 1 S
YAXIS(2)=8HEC PER I
YAXIS(3)=8HNCH
READ(5,8) XAXIS(4),XAXIS(5)
8 FORMAT(A8,A8,)
9 FORMAT(15X,F5.2)
9 FORMAT(15X,F5.2)
NX=TOTAL/2.04.
IF(NX.LT.13)NX=13
NXAXIS=40
NYAXIS=24
CALL PLOTINT(-6.,6.,10)
CALL PLOT(28.,0.,PLOTEND)
CALL ROTATEXY
DO 10 I=1,NX
X=I
10 CALL PLOTSYMB(X,3.,20,13,0.,PSDOWN)
C GO BACK TO (4,-1)
CALL PLOTSYMB(4.,-1.,25,XAXIS,0.,NXAXIS)
CALL PLOT(0.,0.,PENUP)
DO 20 I=1,27
Y=I
20 CALL PLOTSYMB(0.,Y.,20,13,90.,PSDOWN)
C GO BACK TO (-1,4)
CALL PLOTSYMB(-1.,4.,25,YAXIS,90.,NYAXIS)
30 READ(5,40)ACE,(AT(I),I=1,11)
40 FORMAT(A5,2F5.0,9F5.2)
IF(EOF(5))GO TO 80
IF(ACE.EQ.5H ) GO TO 60
SHOT(1)=ACE
ITIM=AT(1)
Z=27.-AT(2)*.00192.
TS=AT(6)
DIST=AT(7)+TS
X=DIST/2.
CALL PLOTSYMB(X,1.,10,SHOT,90.,5)
C TIME=T(I)*1 SEC/INCH,DIST=2SEC/INCH,AND X AND Y IN INCHES
II=1
DO 100 I=1,4
R(I)=AT(I+7)
IF(R(I).EQ.0) GO TO 30
100 II=I
GO TO 30
60 DO 70 I=1,11
IF(AT(I).EQ.0.) GO TO 70
Y=AT(I)+TS
IF(Y.GT.28.) GO TO 70
CALL PLOTSYMB(X,Y.,10,3,0.,PSUP)
70 CONTINUE
CALL PLOTSYMB(X,Z.,13,90.,PSUP)
GO TO 30
80 NX=NX+4
CALL PLOT(XN,30.,PLOTEND)
END

```

```

PROGRAM REDPLOT2
DIMENSION XAXIS(5),YAXIS(5),SHOT(1),AT(11),R(4)
DIMENSION DEPI(100),XD(100)
INTEGER PLOTEND,PSUP,PSDOWN,PENUP,PENDOWN
PLOTEND=-3 $ PSUP=-1 $ PSDOWN=-2
PENUP=3 $ PENDOWN=2 $ DEPTH=0. $ NC=0
WRITE(61,3)
3 FORMAT(4 GIVE REDUCING VELOCITY, F5.2)
READ(60,4)REDVEL
4 FORMAT(F5.2)
XAXIS(1)=8HDISTANCE
XAXIS(2)=8H 1 SEC P
XAXIS(3)=8HER INCH
YAXIS(1)=8HTIME .5
YAXIS(2)=8HSEC PER
YAXIS(3)=8HINCH
YAXIS(4)=8HT - X /
READ(5,8) XAXIS(4),XAXIS(5)
8 FORMAT(A8,A4)
9 READ(5,9)TDTS,V1
9 FORMAT(15X,F5.2,5X,F5.3)
NX=TDTS/1.04.
IF(NX.LT.13)NX=13
NXAXIS=40
NYAXIS=40
ENCODE(8,101,YAXIS(5))REDVEL
101 FORMAT(F5.2,3X)
CALL PLOTINT(-6.,6.,10)
CALL PLOT(29.,0.,PLOTEND)
CALL ROTATEXY
DO 10 I=1,NX
X=I
10 CALL PLOTSYMB(X,0.,20,13,0.,PSDOWN)
C GO BACK TO (4,-1)
CALL PLOTSYMB(4.,-1.,25,XAXIS,0.,NXAXIS)
CALL PLOT(8.,0.,PENUP)
DO 20 I=1,27
Y=I
20 CALL PLOTSYMB(0.,Y.,20,13,90.,PSDOWN)
C GO BACK TO (-1,4)
CALL PLOTSYMB(-1.,4.,25,YAXIS,90.,NYAXIS)
30 READ(5,40)ACE,(AT(I),I=1,11)
40 FORMAT(A5,2F5.0,9F5.2)
IF(EOF(5))GO TO 80
IF(ACE.EQ.5H 1 GO TO 60
SHOT(1)=ACE
ITIM=AT(1)
ND=ND+1
DEP(ND)=27.-AT(2)*.001*2.
YS=AT(6)
DIST=AT(7)+YS
REDUCE=DIST*V1/REDVEL
XD(ND)=X
XD(ND)=Y
IF(X.GT.37.) GO TO 55
CALL PLOTSYMB(X,1.,10,SHOT,90.,5)
C TIME=T(I)=.5 SEC/INCH,DIST=2 SEC/INCH,AND X AND Y IN INCHES
55 II=1
DO 100 I=1,4
P(I)=AT(I+7)
IF(R(II).EQ.0) GO TO 30
100 II=I
GO TO 30
60 DO 70 I=1,11
IF(AT(II).EQ.0.) GO TO 30
Y=AT(II)+YS
Y=(Y-REDUCE)*2.05.
IF(Y.GT.27.) GO TO 70
IF(X.GT.37.) GO TO 70
CALL PLOTSYMB(X,Y.,10,3,0.,PSUP)
70 CONTINUE
GO TO 30
80 DO 90 I=1,ND
X=XD(I)
DEPTH=DEP(I)
90 CALL PLOTSYMB(X,DEPTH.,1,13,90.,PSUP)
XN=NX+4
CALL PLOT(XN,30.,PLOTEND)
END

```

```

PROGRAM MULTLAY
DIMENSION W(20),V(20),VA(20),VB(20),ALPH(20),BETA(20),C(20),
1 A(20),B(20),TAI(20),TBI(20),MA(20),MB(20),DA(20),CB(20),P(20)
DIMENSION TITLE(N)
C IF TBI INTERCEPT TIMES ARE NOT READ IN, INSERT A BLANK
C CARD WHERE THEY ARE CALLED FOR IN THE DATA DECK. THEY
C WILL THEN BE COMPUTED BY FORMULA AFTER STEP 421. IF THEY
C ARE READ IN, THEY WILL BE CHECKED FOR CONSISTENCY WITHIN 10 PC
402 WRITE (61,401)

401 FORMAT (X0#)
C N=NUMBER OF LAYERS OR TRAVEL TIME SEGMENTS, X=END-TO-END
C SPREAD LENGTH
READ (5,403)N,X,(TITLE(I),I=1,6)
IF(EOF(5)) CALL EXIT
405 FORMAT (I4,F8.0,6A8)
IF (N) 640,640,407
407 READ (5,410)(VA(I),I=1,N)
410 FORMAT (9F8.0)
READ (5,410) (VB(I),I = 1,N)
TAI(1) = .0
READ (5,410) (TAI(I),I=2,N)
TBI(1) = .0
READ (5,410) (TBI(I),I=2,N)
WRITE (61,415)X,(TITLE(I),I=1,6)
415 FORMAT (X,X,OVERSAL DISTANCE = X ,F10.3,3X,6A8,/)
WRITE (61,420)
420 FORMAT (X INPUT DATA///X LAYER APPARENT APPARENTX,
1X INTERCEPT INTERCEPTX VELOCITIES A VELOX,
2XCITIES B TIMES A TIMES B)
DO 425 I=2,N
TBB = TAI(I) + X*(1./VA(I) - 1./VB(I))
IF (TBI(I)) 422,422,423
422 TBI(I) = TBB
GO TO 425
423 TAEND = TAI(I) + X/VA(I)
TBEND = TBI(I) + X/VB(I)
ERROR = ABSF(TAEND/TBEND - 1.)
IF (ERROR - .10) 425,424,424
424 WRITE (61,1424) I
1424 FORMAT (X0 APPARENT VELOCITY AND TIME INTERCEPT DATA AREX,
1X INCONSISTENT AT LAYER XX NUMBER X,I2,X END-TO-END X,
2X TRAVEL TIMES DIFFER BY MORE THAN 10 PERCENT.X/)
GO TO 425
425 CONTINUE
WRITE (61,1425) (I,VA(I),VB(I),TAI(I),TBI(I),I=1,N)
1425 FORMAT (X X,I4,F13.3,F14.3,F12.3,F10.3)
V(1) = (VA(1) + VB(1))* .5
DO 570 M = 2,N
K = 1
ALPH(1) = ASINF(V(1)/VB(M))
BETA(1) = ASINF(V(1)/VA(M))
IF (M-2) 500,500,510
500 A(1) = (ALPH(1) + BETA(1))* .5
W(2) = (ALPH(1) - BETA(1))* .5
V(2) = V(1)/SINF(A(1))
GO TO 550
510 A(1) = ALPH(1) - W(2)
B(1) = BETA(1) + W(2)
520 K = K+1
VV = V(K)/V(K-1)
P(K) = ASINF(VV*SINF(A(K-1)))

```



```

      Q(K) = ASINF(VV*SINF(B(K-1)))
      IF (K+1-M) 530,540,540
530  A(K) = P(K) - W(K+1) + W(K)
      R(K) = Q(K) + W(K+1) - W(K)
      ALPH(K) = A(K) + W(K+1)
      BETA(K) = B(K) - W(K+1)
      GO TO 520
540  A(K) = (P(K) + Q(K))*0.5
      B(K) = A(K)
      W(K+1) = W(K) + (P(K) - Q(K))*0.5
      ALPH(K) = A(K) + W(K+1)
      BETA(K) = B(K) - W(K+1)
      V(K+1) = V(K)/SINF(A(K))
550  KK = K-1
      MMA=0.
      HMB = 0.
      IF(K.EQ.1)GO TO 561
      DO 560 I = 1, KK
      HH = COSF(ALPH(I)) + COSF(BETA(I))
      HH = HH/V(I)
      MMA = MMA + HH*HA(I)
560  HMB = HMB + HH*HB(I)
561  R = V(K)/(COSF(ALPH(K)) + COSF(BETA(K)))
      HA(K) = R*(TAI(K+1) - MMA)
      HB(K) = R*(TBI(K+1) - HMB)
      DA(1) = HA(1)
      DB(1) = HB(1)
      DA(K) = DA(K-1) + HA(K)
      DB(K) = DB(K-1) + HB(K)
570  CONTINUE
      RTOD=190./3.1415926
      DO 580 J = 2, N
580  W(J) = W(J)*RTOD
      WRITE (61,620)
620  FORMAT(20COMPUTED STRUCTURE///: LAYER VELOCITY :.
      :THICKNESS A THICKNESS B DIP DEPTH A DEPTH B:)
      I = 1
      WRITE (61,625) I, V(I), HA(I), HB(I), DA(I), DB(I)
625  FORMAT(: :I4,F12.3,F11.3,F14.3,9X,F8.3,F9.3)
      VN = N-1
      WRITE (61,630) (I, V(I), HA(I), HB(I), W(I), DA(I), DB(I),
      1 I=2, NN)
630  FORMAT(: :I4,F12.3,F11.3,F14.3,F9.3,F8.3,F9.3)
      WRITE (61,635) N, V(N), W(N)
635  FORMAT(: :I4,F12.3,23X,F11.3)
      GO TO 402
640  CONTINUE
      END

```

INPUT FORMAT FOR PROGRAM MULTLAY

| N | X | TITLE(I) | | |
|--------|--------|-----------|--------|--|
| VA(1) | VA(2) | • • • • • | VA(N) | |
| VB(1) | VB(2) | • • • • • | VB(N) | |
| TAI(1) | TAI(2) | • • • • • | TAI(N) | |
| TBI(1) | TBI(2) | • • • • • | TBI(N) | |

N : Number of layers (equal to number of velocities).

X : End to end profile length.

TITLE(I) : Line identification.

I=1,....,N : Layer number.

VA(I) : Apparent velocities from the A-end of the profile.

VB(I) : Apparent velocities from the B-end of the profile.

TAI(I) : Intercept times for layers 2 through N at A-end of the profile.

TBI(I) : Intercept times for layers 2 through N at B-end of the profile.

All distances in meters or kilometers.

All velocities in meters per seconds or kilometers per seconds.

All times in seconds.

With single-ended line : $VB(I) = VA(I)$ and $TBI(I) = TAI(I)$.

OUTPUT FORMAT FOR PROGRAM MULTILAY

| | | | | | | |
|---------------------|-----------------------|-----------------------|-------------------|-------------------|---------|---------|
| REVERSAL DISTANCE = | | X | TITLE(1) | | | |
| INPUT DATA | | | | | | |
| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B | | |
| 1 | VA(1) | VB(1) | TAI(1) | TBI(1) | | |
| 2 | VA(2) | VB(2) | TAI(2) | TBI(2) | | |
| ... | ... | ... | ... | ... | | |
| N | VA(N) | VB(N) | TAI(N) | TBI(N) | | |
| COMPUTED STRUCTURE | | | | | | |
| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
| 1 | V(1) | HA(1) | HB(1) | | DA(1) | DB(1) |
| 2 | V(2) | HA(2) | HB(2) | W(2) | DA(2) | DB(2) |
| ... | ... | ... | ... | ... | ... | ... |
| N-1 | V(N-1) | HA(N-1) | HB(N-1) | W(N-1) | DA(N-1) | DB(N-1) |
| N | V(N) | | | W(N) | | |

X : End to end spread length.

TITLE(1) : Line identification.

I=1,...,N : Layer number.

VA(I) : Apparent velocities from the A-end of the profile.

VB(I) : Apparent velocities from the B-end of the profile.

TAI(I) : Intercept times for layers 2 through N at A-end of the profile.

TBI(I) : Intercept times for layers 2 through N at B-end of the profile.

V(I) : True layer velocities.

HA(I) : Layer thicknesses at A-end.

HB(I) : Layer thicknesses at B-end.

W(I) : Layer dips in degrees.

DA(I) : Depths from surface to bottom of layers at A-end.

DB(I) : Depths from surface to bottom of layers at B-end.

All times in seconds.

All distances in meters or kilometers.

All velocities in meters per seconds or kilometers per seconds.

IV
INTERCEPT TIMES AND APPARENT
VELOCITIES (INPUT OF MULTLAY)
AND COMPUTED STRUCTURES
(OUTPUT OF MULTLAY)
FOR ALL LINES

4 21.62 MGL1
 1.44 2.14 2.77 5.02
 1.44 2.14 2.77 5.02
 0.044 0.080 0.680
 0.044 0.080 0.680

REVERSAL DISTANCE = 21.620 MGL1S

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1.440 | 1.440 | 0 | 0 |
| 2 | 2.140 | 2.140 | .044 | .044 |
| 3 | 2.770 | 2.770 | .080 | .080 |
| 4 | 5.020 | 5.020 | .680 | .680 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|-----|---------|---------|
| 1 | 1.440 | .043 | .043 | | .043 | .043 |
| 2 | 2.140 | .049 | .049 | 0 | .092 | .092 |
| 3 | 2.770 | .966 | .966 | 0 | 1.058 | 1.058 |
| 4 | 5.020 | | 0 | | | |

4 12.77 MGL2
 1.44 2.14 2.99 5.26
 1.44 2.14 2.99 5.26
 0.031 0.230 0.760
 0.031 0.230 0.760

REVERSAL DISTANCE = 12.770 MGL2S

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1.440 | 1.440 | 0 | 0 |
| 2 | 2.140 | 2.140 | .031 | .031 |
| 3 | 2.990 | 2.990 | .230 | .230 |
| 4 | 5.260 | 5.260 | .760 | .760 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|-----|---------|---------|
| 1 | 1.440 | .030 | .030 | | .030 | .030 |
| 2 | 2.140 | .296 | .296 | 0 | .326 | .326 |
| 3 | 2.990 | .040 | .040 | 0 | 1.175 | 1.175 |
| 4 | 5.260 | | 0 | | | |

6 26.61 91 6 TO 1 M1267
 1.44 2.25 2.46 3.01 3.727 5.387
 1.44 2.25 2.46 3.01 3.716 5.259
 0.10 0.15 0.20 0.45 1.40
 0.10 0.15 0.20 0.43 1.28

REVERSAL DISTANCE = 26.610 91 6 TO 1 M1267S

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1.440 | 1.440 | 0 | 0 |
| 2 | 2.250 | 2.250 | .100 | .100 |
| 3 | 2.460 | 2.460 | .150 | .150 |
| 4 | 3.010 | 3.010 | .200 | .200 |
| 5 | 3.727 | 3.716 | .450 | .430 |
| 6 | 5.387 | 5.259 | 1.400 | 1.280 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|------|---------|---------|
| 1 | 1.440 | .094 | .094 | | .094 | .094 |
| 2 | 2.250 | .124 | .124 | 0 | .217 | .217 |
| 3 | 2.460 | .027 | .027 | 0 | .244 | .244 |
| 4 | 3.010 | .578 | .527 | 0 | .823 | .771 |
| 5 | 3.721 | 2.183 | 1.944 | .116 | 3.006 | 2.715 |
| 6 | 5.322 | | | .624 | | |

6 29.39 91 4 TO 3 M345
 1.44 2.29 2.56 2.99 3.898 4.904
 1.44 2.29 2.56 2.99 3.867 4.674
 0.10 0.16 0.20 0.56 1.375
 0.10 0.16 0.20 0.50 1.000

REVERSAL DISTANCE = 29.390 91 4 TO 3 M345S

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1.440 | 1.440 | 0 | 0 |
| 2 | 2.290 | 2.290 | .100 | .100 |
| 3 | 2.560 | 2.560 | .160 | .160 |
| 4 | 2.990 | 2.990 | .200 | .200 |
| 5 | 3.898 | 3.867 | .560 | .500 |
| 6 | 4.904 | 4.674 | 1.375 | 1.000 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|-------|---------|---------|
| 1 | 1.440 | .093 | .093 | | .093 | .093 |
| 2 | 2.290 | .137 | .137 | 0 | .230 | .230 |
| 3 | 2.560 | .025 | .025 | 0 | .255 | .255 |
| 4 | 2.990 | .771 | .630 | 0 | 1.026 | .885 |
| 5 | 3.892 | 2.419 | 1.623 | .276 | 3.665 | 2.568 |
| 6 | 4.784 | | | 1.707 | | |

5 10958. ARC WEST 76 BEAUFORT W8A9A
 1440. 1600. 2230. 3020. 4680.
 1440. 1600. 2230. 3020. 4680.
 .010 .215 .575 1.255
 .010 .215 .575 1.255

REVERSAL DISTANCE = 10958.000 ARC WEST 76 BEAUFORT W8A9AS

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1440.000 | 1440.000 | 0 | 0 |
| 2 | 1600.000 | 1600.000 | .010 | .010 |
| 3 | 2230.000 | 2230.000 | .215 | .215 |
| 4 | 3020.000 | 3020.000 | .575 | .575 |
| 5 | 4680.000 | 4680.000 | 1.255 | 1.255 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|-----|-----------|----------|
| 1 | 1440.000 | 16.518 | 16.518 | | 16.518 | 16.518 |
| 2 | 1600.000 | 226.906 | 226.806 | 0 | 243.324 | 243.324 |
| 3 | 2230.000 | 519.818 | 519.818 | 0 | 763.142 | 763.142 |
| 4 | 3020.000 | 1100.723 | 1100.723 | | 01863.865 | 1863.865 |
| 5 | 4680.000 | | | 0 | | |

7 23846. ARC WEST 76 BEAUFORT W8B9B
 1440. 1600. 2230. 2830. 4240. 5630. 7070.
 1440. 1600. 2230. 2830. 4240. 5630. 7070.
 .010 .215 .470 1.050 1.440 1.925
 .010 .215 .470 1.050 1.440 1.925

REVERSAL DISTANCE = 23846.000 ARC WEST 76 BEAUFORT W8B9BS

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1440.000 | 1440.000 | 0 | 0 |
| 2 | 1600.000 | 1600.000 | .010 | .010 |
| 3 | 2230.000 | 2230.000 | .215 | .215 |
| 4 | 2830.000 | 2830.000 | .470 | .470 |
| 5 | 4240.000 | 4240.000 | 1.050 | 1.050 |
| 6 | 5630.000 | 5630.000 | 1.440 | 1.440 |
| 7 | 7070.000 | 7070.000 | 1.925 | 1.925 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|-----|-----------|----------|
| 1 | 1440.000 | 16.518 | 16.518 | | 16.518 | 16.518 |
| 2 | 1600.000 | 226.806 | 226.806 | 0 | 243.324 | 243.324 |
| 3 | 2230.000 | 391.899 | 391.899 | 0 | 635.223 | 635.223 |
| 4 | 2830.000 | 887.279 | 887.279 | | 01522.501 | 1522.501 |
| 5 | 4240.000 | 906.128 | 906.128 | | 02428.629 | 2428.629 |
| 6 | 5630.000 | 1750.786 | 1750.786 | | 04179.415 | 4179.415 |
| 7 | 7070.000 | | | 0 | | |

7 28.07 LINE 10-11 12-13 WITH 6.0 AND 7.0 LAYERS M1012
 1.440 1.650 2.509 3.044 4.056 6.000 6.906
 1.440 1.650 2.509 3.090 3.804 6.000 7.129
 0.008 0.440 0.675 1.130 1.760 1.805
 7.008 0.440 0.820 1.360 1.760 1.830

REVERSAL DISTANCE = 28.070 LINE 10-11 12-13 WITH 6.0 AND 7.0 LAYERS M1012S

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1.440 | 1.440 | 0 | 0 |
| 2 | 1.650 | 1.650 | .008 | .008 |
| 3 | 2.509 | 2.509 | .440 | .440 |
| 4 | 3.044 | 3.090 | .675 | .820 |
| 5 | 4.056 | 3.804 | 1.130 | 1.360 |
| 6 | 6.000 | 6.000 | 1.760 | 1.760 |
| 7 | 6.906 | 7.129 | 1.805 | 1.830 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|--------|---------|---------|
| 1 | 1.440 | .012 | .012 | | .012 | .012 |
| 2 | 1.650 | .467 | .467 | 0 | .479 | .479 |
| 3 | 2.509 | .400 | .716 | 0 | .879 | 1.195 |
| 4 | 3.067 | .877 | .966 | -0.611 | 1.756 | 2.161 |
| 5 | 3.921 | 1.045 | .362 | 2.615 | 2.841 | 2.523 |
| 6 | 5.994 | -0.186 | .063 | -0.927 | 2.655 | 2.586 |
| 7 | 7.006 | | | -2.886 | | |

6 29736.000 WEST 76 BEAUFORT M1617
 1440. 1600. 1820. 2440. 3620. 6080.
 1440. 1600. 1820. 2440. 3620. 6080.
 .010 .100 .380 1.025 1.745
 .010 .100 .380 1.025 1.745

REVERSAL DISTANCE = 29736.000 WEST 76 BEAUFORT M1617S

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1440.000 | 1440.000 | 0 | 0 |
| 2 | 1600.000 | 1600.000 | .010 | .010 |
| 3 | 1820.000 | 1820.000 | .100 | .100 |
| 4 | 2440.000 | 2440.000 | .380 | .380 |
| 5 | 3620.000 | 3620.000 | 1.025 | 1.025 |
| 6 | 6080.000 | 6080.000 | 1.745 | 1.745 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|-----|----------|----------|
| 1 | 1440.000 | 16.518 | 16.518 | | 16.518 | 16.518 |
| 2 | 1600.000 | 144.306 | 144.306 | 0 | 160.824 | 160.824 |
| 3 | 1820.000 | 307.807 | 307.807 | 0 | 468.631 | 468.631 |
| 4 | 2440.000 | 907.940 | 907.945 | | 1376.575 | 1376.575 |
| 5 | 3620.000 | 1226.193 | 1226.193 | | 2602.768 | 2602.768 |
| 6 | 6080.000 | | | 0 | | |

6 26699. ARC WEST 76 BEAUFORT M1819
 1440. 1600. 1840. 2320. 3310. 5660.
 1440. 1600. 1840. 2320. 3310. 5660.
 .010 .125 .465 1.205 2.310
 .010 .125 .465 1.205 2.310

REVERSAL DISTANCE = 26698.000 ARC WEST 76 BEAUFORT M1819S

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1440.000 | 1440.000 | 0 | 0 |
| 2 | 1600.000 | 1600.000 | .010 | .010 |
| 3 | 1840.000 | 1840.000 | .125 | .125 |
| 4 | 2320.000 | 2320.000 | .465 | .465 |
| 5 | 3310.000 | 3310.000 | 1.205 | 1.205 |
| 6 | 5660.000 | 5660.000 | 2.310 | 2.310 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|-----|----------|----------|
| 1 | 1440.000 | 16.518 | 16.518 | | 16.518 | 16.518 |
| 2 | 1600.000 | 179.367 | 179.367 | 0 | 195.885 | 195.885 |
| 3 | 1840.000 | 429.958 | 429.958 | 0 | 625.843 | 625.843 |
| 4 | 2320.000 | 975.136 | 975.136 | 0 | 1600.979 | 1600.979 |
| 5 | 3310.000 | 1762.815 | 1762.815 | 0 | 3363.794 | 3363.794 |
| 6 | 5660.000 | | | 0 | | |

6 22651. ARC WEST 76 BEAUFORT M2021
 1440. 1600. 1890. 2350. 3390. 5680.
 1440. 1600. 1890. 2350. 3390. 5680.
 .010 .125 .490 1.105 2.075
 .010 .125 .490 1.105 2.075

REVERSAL DISTANCE = 22651.000 ARC WEST 76 BEAUFORT M2021S

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1440.000 | 1440.000 | 0 | 0 |
| 2 | 1600.000 | 1600.000 | .010 | .010 |
| 3 | 1890.000 | 1890.000 | .125 | .125 |
| 4 | 2350.000 | 2350.000 | .490 | .490 |
| 5 | 3390.000 | 3390.000 | 1.105 | 1.105 |
| 6 | 5680.000 | 5680.000 | 2.075 | 2.075 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|-----|----------|----------|
| 1 | 1440.000 | 16.518 | 16.518 | | 16.518 | 16.518 |
| 2 | 1600.000 | 165.535 | 165.535 | 0 | 182.053 | 182.053 |
| 3 | 1890.000 | 509.354 | 509.354 | 0 | 691.407 | 691.407 |
| 4 | 2350.000 | 740.727 | 740.727 | 0 | 1432.134 | 1432.134 |
| 5 | 3390.000 | 1630.983 | 1630.983 | 0 | 3063.117 | 3063.117 |
| 6 | 5680.000 | | | 0 | | |

6 45770.000 ARC WEST 76 BEAUFORT M22A24B REVERSE
 1440. 1600. 1832. 2348. 2932. 5781.
 1440. 1600. 1826. 2315. 2880. 6034.
 .010 .175 .450 .810 1.715
 .010 .100 .170 .525 2.050

REVERSAL DISTANCE = 41000.000 ARC WEST 76 BEAUFORT M24A22BS REVERSE

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1440.000 | 1440.000 | 0 | 0 |
| 2 | 1600.000 | 1600.000 | .010 | .010 |
| 3 | 1937.000 | 1945.000 | .120 | .215 |
| 4 | 3395.000 | 3398.000 | 1.165 | 1.175 |
| 5 | 5687.000 | 5750.000 | 2.210 | 2.290 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|--------|----------|----------|
| 1 | 1440.000 | 16.518 | 16.518 | | 16.518 | 16.518 |
| 2 | 1600.000 | 147.839 | 282.887 | 0 | 164.357 | 298.605 |
| 3 | 1940.983 | 1160.407 | 997.175 | -0.172 | 1324.764 | 1295.781 |
| 4 | 3396.490 | 1869.649 | 2032.408 | .035 | 194.413 | 3328.189 |
| 5 | 5718.294 | | | -0.195 | | |

5 41000.000 ARC WEST 76 BEAUFORT M24A22B REVERSE
 1440. 1600. 1937. 3395. 5687.
 1440. 1600. 1945. 3398. 5750.
 .010 .120 1.165 2.210
 .010 .215 1.175 2.290

REVERSAL DISTANCE = 45770.000 ARC WEST 76 BEAUFORT M22A24BS REVERSE

INPUT DATA

| LAYER | APPARENT VELOCITIES A | APPARENT VELOCITIES B | INTERCEPT TIMES A | INTERCEPT TIMES B |
|-------|--------------------------|--------------------------|----------------------|----------------------|
| 1 | 1440.000 | 1440.000 | 0 | 0 |
| 2 | 1600.000 | 1600.000 | .010 | .010 |
| 3 | 1832.000 | 1826.000 | .175 | .100 |
| 4 | 2348.000 | 2315.000 | .450 | .170 |
| 5 | 2932.000 | 2880.000 | .810 | .525 |
| 6 | 5781.000 | 6034.000 | 1.715 | 2.050 |

COMPUTED STRUCTURE

| LAYER | VELOCITY | THICKNESS A | THICKNESS B | DIP | DEPTH A | DEPTH B |
|-------|----------|-------------|-------------|--------|----------|----------|
| 1 | 1440.000 | 16.518 | 16.518 | | 16.518 | 16.518 |
| 2 | 1600.000 | 265.613 | 141.769 | 0 | 282.131 | 158.287 |
| 3 | 1828.987 | 280.927 | 24.827 | .170 | 563.058 | 192.315 |
| 4 | 2331.318 | 535.554 | 641.824 | .455 | 1098.612 | 833.338 |
| 5 | 2905.706 | 1100.886 | 2157.800 | .325 | 2198.698 | 3031.138 |
| 6 | 5903.385 | | | -1.034 | | |

[illegible]

| 日期 | 品名 | 数量 | 单价 | 金额 |
|------------|----|-----|------|--------|
| 1950.10.1 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.2 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.3 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.4 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.5 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.6 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.7 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.8 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.9 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.10 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.11 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.12 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.13 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.14 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.15 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.16 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.17 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.18 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.19 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.20 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.21 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.22 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.23 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.24 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.25 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.26 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.27 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.28 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.29 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.30 | 大米 | 100 | 1.20 | 120.00 |
| 1950.10.31 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.1 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.2 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.3 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.4 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.5 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.6 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.7 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.8 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.9 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.10 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.11 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.12 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.13 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.14 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.15 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.16 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.17 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.18 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.19 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.20 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.21 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.22 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.23 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.24 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.25 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.26 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.27 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.28 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.29 | 大米 | 100 | 1.20 | 120.00 |
| 1950.11.30 | 大米 | 100 | 1.20 | 120.00 |
| 1950.12.1 | 大米 | 100 | 1.20 | 120.00 |
| 1950.12.2 | 大米 | 100 | 1.20 | 120.00 |
| 1950.12.3 | 大米 | 100 | 1.20 | 120.00 |
| 1950.12.4 | 大米 | 100 | 1.20 | 120.00 |
| 1950.12.5 | 大米 | 100 | 1.20 | 120.00 |
| 1950.12.6 | 大米 | 100 | | |

REFUGEE DISTANCE: 10,000-100

| LAYER | VELOCITY | THICKNESS | | DIP | DENSITY | |
|-------|------------|-----------|-----------|-----|---------|---|
| | | 1 | 2 | | 1 | 2 |
| 1 | 1400-1000 | 10-51.5 | 10-51.5 | 0 | 1.8-1.8 | |
| 2 | 1600-1000 | 4.4-3.2 | 4.4-3.2 | 0 | 1.8-1.8 | |
| 3 | 2100-1000 | 18.6-13.2 | 18.6-13.2 | 0 | 1.8-1.8 | |
| 4 | 3400-1000 | 44.9-34.9 | 44.9-34.9 | 0 | 1.8-1.8 | |
| 5 | 4600-1000 | 52.5-50.9 | 52.5-50.9 | 0 | 1.8-1.8 | |
| 6 | 698.7-1000 | | | 0 | 1.8-1.8 | |

V

PROGRAM TO COMPUTE THE OFFSET
DISTANCES OF THE RAYS (WAREFRA)
AND INPUT AND OUTPUT DATA
FOR PROCESSED LINES

```

      PROGRAM WAREFRA
C THIS PROGRAM COMPUTES PLANE DIPPING LAYER MODEL
C PARAMETERS, SECTIONS OF LAYERS ALONG WHICH RAY IS REFRACTED
C AND THE CRITICAL DISTANCE. THE INPUT DATA REQUIRES
C KNOWN OR APPARENT LAYER VELOCITIES (VA) AND EITHER
C INTERCEPT TIME FROM REFRACTED ARRIVAL OR LAYER THICKNESS
C VERTICALLY UNDER THE ORIGIN. LAYER DIP IS ASSUMED ZERO
C IF LEFT BLANK. IF LAYER THICKNESS IS GIVEN, GIVEN
C VELOCITY IS TAKEN TO BE THE TRUE LAYER VELOCITY.
      DIMENSION V(10), HDR(10), W(10), VA(10), TIA(10), HA(10)
      DIMENSION R (10), ALPHA (10), BETA (10), HB (10), A (10)
      DIMENSION XA(10), XB(10), YA(10), YB(10), XC(10), P(10)
      DIMENSION Q (10)
      RTOD = 180. / 3.14159265
      OTOR = 1. / RTOD
C READ HDR CARD
10 READ (5, 100) N, V(1), X, HDR
      IF (EOF(5)) CALL EXIT
C N IS NUMBER OF LAYERS, V(1) IS VELOCITY OF FIRST LAYER,
C X IS LENGTH OF LINE, HDR IS IDENTIFIER MAX LENGTH OF 8
100 FORMAT (I5,F5.3,F5.2,10A8)
      IF (EOF(1)) CALL EXIT
      IF (N .LT. 10) GO TO 15
      WRITE (61, 110) N
110 FORMAT (2-N LARGER THAN DIMENSIONS N =2,T5)
      CALL EXIT
15 K = 2
      VA (1) = V (1)
      W (1) = 0.0
C READ SUCCEEDING CARDS
C IF HA(1) IS NOT GIVEN, COMPUTE MODEL FROM TIA INTERCEPT
      READ (5, 101) VA (2), TIA (2), W (2), HA (1)
101 FORMAT (4F5.3)
      W (2) = W (2) * OTOR
      BETA (1) = ASINF (V (1) / VA (2))
      A (1) = R (1) = BETA (1) * W (2)
      ALPHA (1) = A (1) + W (2)
      V (2) = V (1) / SIN (A (1))
      IF (HA(1) .NE. 0.0) V(2) = VA(2)
C FIND OUT IF THICKNESS GIVEN. IF NOT, CALCULATE VELOCITY AND
C ANGLES.
      IF (HA (1) .NE. 0.0) GO TO 30
      IF (TIA (2) .NE. 0.0) GO TO 25
22 WRITE (61, 111)
111 FORMAT (2-HA AND TIA .EQ. 0.0)
      CALL EXIT
C COMPUTE DEPTHS TO LAYERS
25 HA(1) = (TIA(2)*V(1)) / (COS(ALPHA(1))*COS(BETA(1)))
30 HB (1) = HA (1) - X * TANF(W (2))
C COMPUTE CRITICAL DISTANCES AND END POINTS IN LAYER
C WHERE RAY TRAVELS AS REFRACTED WAVE
      XA (1) = HA (1) * TANF(ALPHA (1))
1 / (1.0 + TANF(W (2)) * TANF(ALPHA (1)))
      YA (1) = HA (1) - XA (1) * TANF(W (2))
      XC(1) = (HA(1) - XA(1) * TANF(W(2))) * TANF(B(1)) + XA(1)
      YB (1) = HB (1) * TANF(BETA (1))
1 / (1.0 - TANF(BETA (1)) * TANF(W (2)))
      YB (1) = HB (1) * XB (1) * TANF(W (2))
      XB (1) = X - XB (1)
40 K = K + 1
C DO LAYERS 3 THROUGH N
      READ (5, 101) VA (K), TIA (K), W (K), HA (K-1)
C COMPUTE ANGLES
      W (K) = W (K) * OTOR
      BETA (1) = ASINF (V (1) / VA (K))
      R (1) = BETA (1) * W (2)
      I = 1
      KM1 = K - 1
50 I = I + 1
      Q (I) = ASINF (V (I) / V (I-1) * SIN (B (I-1)))
      BETA (I) = Q (I) - W (I)
      R (I) = BETA (I) * W (I+1)
      IF (I .LT. KM1) GO TO 50
      A (K-1) = R (K-1)
      ALPHA (K-1) = A (K-1) + W (K)
      V (K) = V (K-1) / SIN (A (K-1))
      IF (HA(K-1) .NE. 0.0) V(K) = VA(K)
      P (K-1) = A (K-1) - W (K-1) + W (K)
      I = K - 1
70 I = I - 1
      A (I) = ASINF (V (I) / V (I+1) * SIN (P (I+1)))
      ALPHA (I) = A (I) + W (I+1)
      P (I) = A (I) - W (I) + W (I+1)
      IF (I .NE. 1) GO TO 70
      KM2 = K - 2
      TEMP1 = TEMP2 = TEMP3 = 0.0
      DO 80 I = 1, KM2
      TEMP1 = TEMP1 + HA (I) / V (I) * (COS (ALPHA (I))

```


INPUT FORMAT FOR PROGRAM WAREFRA

| N | V1 | X | TITLE(I) |
|-------|--------|------|----------|
| VA(1) | TAI(1) | | |
| VA(2) | TAI(2) | W(2) | HA(1) |
| ... | ... | ... | ... |
| VA(N) | TAI(N) | W(N) | HA(N-1) |

N : Number of layers (equal to number of velocities).

V1 : Water velocity.

X : End to end spread length.

TITLE(I) : Line identification.

I=1,...,N : Layer number.

VA(I) : Apparent velocities at A-end or true velocities.

TAI(I) : Intercept times at A-end.

W(I) : Layer dips in degrees.

HA(I) : Layer thicknesses at A-end.

All times in seconds.

All distances in kilometers.

All velocities in kilometers per seconds.

The program needs intercept times or layer thicknesses.

The layer dip is assumed zero if left blank.

If the layer thickness is given, the given velocity is taken to be the true layer velocity.

OUTPUT FORMAT FOR PROGRAM WAREFRA

| - TITLE(1) | | | | | |
|------------|--------------|---------|-----------|-----------------|----------|
| N | N | SPREAD | | X | |
| N | APPARENT | | DIP | LAYER THICKNESS | |
| VELOCITY | | | AT ORIGIN | | |
| 1 | VA(1) | | W(1) | | HA(1) |
| 2 | VA(2) | | W(2) | | HA(2) |
| ... | ... | | ... | | ... |
| N-1 | VA(N-1) | | W(N-1) | | HA(N-1) |
| N | VA(N) | | W(N) | | |
| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
| 1 | SHA(1) | HA(1) | V(1) | HB(1) | SHB(1) |
| 2 | SHA(2) | HA(2) | V(2) | HB(2) | SHB(2) |
| ... | ... | ... | ... | ... | ... |
| N-1 | SHA(N-1) | HA(N-1) | V(N-1) | HB(N-1) | SHB(N-1) |
| N | | | V(N) | | |
| LAYER | RAY TO LAYER | | CRITICAL | RAY FROM LAYER | |
| | X | Y | | X | Y |
| | 0.00 | 0.00 | | X | 0.00 |
| 1 | XA(1) | YA(1) | XC(1) | XB(1) | YB(1) |
| 2 | XA(2) | YA(2) | XC(2) | XB(2) | YB(2) |
| ... | ... | ... | ... | ... | ... |
| N-1 | XA(N-1) | YA(N-1) | XC(N-1) | XB(N-1) | YB(N-1) |

TITLE(I) : Line identification.
 N : Number of layers including the water layer.
 X : End to end spread length.
 I=1, ..., N : Layer number.
 VA(I) : Apparent velocities at the A-end of the profile or true velocities.
 W(I) : Layer dips in degrees.
 HA(I) : Layer thicknesses at A-end.
 HB(I) : Layer thicknesses at B-end.
 V(I) : True velocities.
 SHA(I) : Layer depths at A-end.
 SHB(I) : Layer depths at B-end.
 XA(I) : Offset distances from A-end.
 XB(I) : Offset distances from B-end.
 XC(I) : Critical distances.
 YA(I) : Layer depths at the offset distances at A-end.
 YB(I) : Layer depths at the offset distances at B-end.

All distances in kilometers.

All velocities in kilometers per seconds.

41.44 21.62 WGL1
 2.136 .044
 2.769 .049
 5.017 .966

WGL1S
 N = 4 SPREAD = 21.6

| N | APPARENT VELOCITY | DIP | LAYER THICKNESS AT ORIGIN |
|---|-------------------|-----|---------------------------|
| 1 | 1.440 | 0 | .043 |
| 2 | 2.136 | 0 | .049 |
| 3 | 2.769 | 0 | .966 |
| 4 | 5.017 | 0 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .043 | .043 | 1.440 | .043 | .043 |
| 2 | .092 | .049 | 2.136 | .049 | .092 |
| 3 | 1.057 | .966 | 2.769 | .966 | 1.057 |
| 4 | | | 5.02 | | |

| LAYER | RAY TO LAYER X | RAY TO LAYER Y | CRITICAL DIST | RAY FROM LAYER X | RAY FROM LAYER Y |
|-------|----------------|----------------|---------------|------------------|------------------|
| | 0.00 | 0.00 | | 21.62 | 0.00 |
| 1 | .039 | .043 | .078 | 21.581 | .043 |
| 2 | .085 | .092 | .171 | 21.535 | .092 |
| 3 | .675 | 1.057 | 1.350 | 20.945 | 1.057 |

41.44 12.77 WGL2
 2.136 .031
 2.994 .230
 5.255 .852

WGL2S
 N = 4 SPREAD = 12.9

| N | APPARENT VELOCITY | DIP | LAYER THICKNESS AT ORIGIN |
|---|-------------------|-----|---------------------------|
| 1 | 1.440 | 0 | .030 |
| 2 | 2.136 | 0 | .294 |
| 3 | 2.994 | 0 | .852 |
| 4 | 5.255 | 0 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .030 | .030 | 1.440 | .030 | .030 |
| 2 | .325 | .294 | 2.136 | .294 | .325 |
| 3 | 1.177 | .852 | 2.994 | .852 | 1.177 |
| 4 | | | 5.26 | | |

| LAYER | RAY TO LAYER X | RAY TO LAYER Y | CRITICAL DIST | RAY FROM LAYER X | RAY FROM LAYER Y |
|-------|----------------|----------------|---------------|------------------|------------------|
| | 0.00 | 0.00 | | 12.77 | 0.00 |
| 1 | .020 | .030 | .055 | 12.742 | .030 |
| 2 | .316 | .325 | .633 | 12.454 | .325 |
| 3 | .730 | 1.177 | 1.461 | 12.040 | 1.177 |

61.44 26.61 BI 6 TO 1 W1267
 2.249 .100
 2.463 .150
 3.013 .200
 3.721 .116 .578
 5.322 .6242.183

BI 6 TO 1 W1267S
 N = 6 SPREAD = 26.6

| N | APPARENT VELOCITY | DIP | LAYER THICKNESS AT ORIGIN |
|---|-------------------|------|---------------------------|
| 1 | 1.440 | 0 | .094 |
| 2 | 2.249 | 0 | .122 |
| 3 | 2.463 | 0 | .028 |
| 4 | 3.013 | 0 | .578 |
| 5 | 3.721 | .116 | 2.183 |
| 6 | 5.322 | .624 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .094 | .094 | 1.440 | .094 | .094 |
| 2 | .216 | .122 | 2.249 | .122 | .216 |
| 3 | .244 | .028 | 2.463 | .028 | .244 |
| 4 | .422 | .578 | 3.013 | .524 | .769 |
| 5 | 3.005 | 2.183 | 3.721 | 1.947 | 2.716 |
| 6 | | | 5.32 | | |

| LAYER | PAY TO LAYER X | Y | CRITICAL DIST | RAY FROM LAYER X | Y |
|-------|----------------|-------|---------------|------------------|-------|
| 1 | 0.00 | 0.00 | | 26.61 | 0.00 |
| 2 | .078 | .094 | .156 | 26.532 | .094 |
| 3 | .342 | .216 | .683 | 26.268 | .216 |
| 4 | .228 | .244 | .497 | 26.382 | .244 |
| 5 | .960 | .820 | 1.912 | 25.727 | .770 |
| 6 | 2.716 | 2.976 | 5.323 | 24.219 | 2.742 |

61.44 29.39 BI 4 TO 3 W345
 2.289 .100
 2.556 .160
 2.993 .280
 3.882 .276 .771
 4.794 1.7072.419

BI 4 TO 3 W345S
 N = 6 SPREAD = 29.4

| N | APPARENT VELOCITY | DIP | LAYER THICKNESS AT ORIGIN |
|---|-------------------|-------|---------------------------|
| 1 | 1.440 | 0 | .093 |
| 2 | 2.289 | 0 | .138 |
| 3 | 2.556 | 0 | .023 |
| 4 | 2.993 | 0 | .771 |
| 5 | 3.882 | .276 | 2.419 |
| 6 | 4.794 | 1.707 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .093 | .093 | 1.440 | .093 | .093 |
| 2 | .231 | .138 | 2.289 | .138 | .231 |
| 3 | .254 | .023 | 2.556 | .023 | .254 |
| 4 | 1.025 | .771 | 2.993 | .629 | .883 |
| 5 | 3.444 | 2.419 | 3.882 | 1.685 | 2.562 |
| 6 | | | 4.78 | | |

| LAYER | PAY TO LAYER X | Y | CRITICAL DIST | RAY FROM LAYER X | Y |
|-------|----------------|-------|---------------|------------------|-------|
| 1 | 0.00 | 0.00 | | 29.39 | 0.00 |
| 2 | .075 | .093 | .150 | 29.315 | .093 |
| 3 | .341 | .231 | .682 | 29.049 | .231 |
| 4 | .253 | .254 | .506 | 29.137 | .254 |
| 5 | 1.105 | 1.020 | 2.191 | 28.464 | .888 |
| 6 | 4.436 | 3.312 | 8.394 | 26.281 | 2.661 |

51.44 10.86 WAA9A
 1.600 .010 .016
 2.230 .215 .227
 3.020 .520 .520
 4.680 1.101 1.101

WAA9AS

N = 5 SPREAD = 10.9

| N | APPARENT VELOCITY | DIP | LAYER THICKNESS AT ORIGIN |
|---|----------------------|-----|------------------------------|
| 1 | 1.440 | 0 | .016 |
| 2 | 1.600 | 0 | .227 |
| 3 | 2.230 | 0 | .520 |
| 4 | 3.020 | 0 | 1.101 |
| 5 | 4.680 | 0 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .016 | .016 | 1.440 | .016 | .016 |
| 2 | .243 | .227 | 1.600 | .227 | .243 |
| 3 | .763 | .520 | 2.230 | .520 | .763 |
| 4 | 1.864 | 1.101 | 3.020 | 1.101 | 1.864 |
| 5 | | | 4.680 | | |

| LAYER | RAY TO LAYER X Y | CRITICAL DIST | RAY FROM LAYER X Y |
|-------|------------------------|---------------|--------------------------|
| | 0.00 0.00 | | 10.86 0.00 |
| 1 | .033 .016 | .066 | 10.927 .016 |
| 2 | .247 .243 | .495 | 10.613 .243 |
| 3 | .720 .763 | 1.440 | 10.140 .763 |
| 4 | 1.300 1.864 | 2.599 | 9.580 1.864 |

71.44 23.85 WBB9B
 1.600 .010 .016
 2.230 .215 .227
 2.830 .392 .392
 4.240 1.050 .887
 5.630 1.440 .906
 7.070 1.925 1.751

WBB9BS

N = 7 SPREAD = 23.9

| N | APPARENT VELOCITY | DIP | LAYER THICKNESS AT ORIGIN |
|---|----------------------|-----|------------------------------|
| 1 | 1.440 | 0 | .016 |
| 2 | 1.600 | 0 | .227 |
| 3 | 2.230 | 0 | .392 |
| 4 | 2.830 | 0 | .887 |
| 5 | 4.240 | 0 | .906 |
| 6 | 5.630 | 0 | 1.751 |
| 7 | 7.070 | 0 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .016 | .016 | 1.440 | .016 | .016 |
| 2 | .243 | .227 | 1.600 | .227 | .243 |
| 3 | .635 | .392 | 2.230 | .392 | .635 |
| 4 | 1.522 | .887 | 2.830 | .887 | 1.522 |
| 5 | 2.428 | .906 | 4.240 | .906 | 2.428 |
| 6 | 4.179 | 1.751 | 5.630 | 1.751 | 4.179 |
| 7 | | | 7.070 | | |

| LAYER | RAY TO LAYER X Y | CRITICAL DIST | RAY FROM LAYER X Y |
|-------|------------------------|---------------|--------------------------|
| | 0.00 0.00 | | 23.85 0.00 |
| 1 | .033 .016 | .066 | 23.817 .016 |
| 2 | .247 .243 | .495 | 23.603 .243 |
| 3 | .667 .635 | 1.333 | 23.183 .635 |
| 4 | 1.136 1.522 | 2.271 | 22.714 1.522 |
| 5 | 1.793 2.428 | 3.587 | 22.057 2.428 |
| 6 | 3.558 4.179 | 7.116 | 20.292 4.179 |

71.44 30.6 W1011
 1.650 .030 .044
 2.320 .365 .372
 3.030 .670 .429
 4.100 1.140 .821
 5.610 1.565 .787
 6.910 1.805 .782

W1011S

N = 7 SPREAD = 30.6
 N APPARENT DIP LAYER THICKNESS
 VELOCITY AT ORIGIN
 1 1.440 0 .044
 2 1.650 0 .372
 3 2.320 0 .429
 4 3.030 0 .821
 5 4.100 0 .787
 6 5.610 1 .782
 7 6.910 0

N DEPTH A THICK A VELOCITY THICK B DEPTH B
 1 .044 .044 1.440 .044 .044
 2 .416 .372 1.650 .372 .416
 3 .845 .429 2.320 .429 .845
 4 1.666 .821 3.030 .821 1.666
 5 2.453 .787 4.100 .787 2.453
 6 3.235 .782 5.610 .782 3.235
 7 6.91

LAYER RAY TO LAYER CRITICAL DIST RAY FROM LAYER
 X Y X Y
 1 0.00 0.00 30.60 0.00
 2 .079 .044 .157 30.521 .044
 3 .411 .416 .822 30.189 .416
 4 .776 .845 1.552 29.824 .845
 5 1.375 1.666 2.750 29.225 1.666
 6 1.691 2.453 3.381 28.909 2.453
 7 2.322 3.235 4.644 28.279 3.235

71.44 32.4 W1213
 1.650 .030 .044
 2.540 .450 .433
 3.460 .960 .827
 4.000 1.290 .965
 5.980 1.755 .519
 7.140 1.940 .942

W1213S

N = 7 SPREAD = 32.4
 N APPARENT DIP LAYER THICKNESS
 VELOCITY AT ORIGIN
 1 1.440 0 .044
 2 1.650 0 .433
 3 2.540 0 .827
 4 3.460 0 .965
 5 4.000 0 .519
 6 5.980 0 .042
 7 7.140 0

N DEPTH A THICK A VELOCITY THICK B DEPTH B
 1 .044 .044 1.440 .044 .044
 2 .477 .433 1.650 .433 .477
 3 1.304 .827 2.540 .827 1.304
 4 2.169 .865 3.460 .865 2.169
 5 2.688 .519 4.000 .519 2.688
 6 2.730 .042 5.980 .042 2.730
 7 7.14

LAYER RAY TO LAYER CRITICAL DIST RAY FROM LAYER
 X Y X Y
 1 0.00 0.00 32.40 0.00
 2 .079 .044 .157 32.321 .044
 3 .400 .477 .801 32.000 .477
 4 1.149 1.304 2.298 31.291 1.304
 5 2.384 2.169 4.768 30.016 2.169
 6 1.604 2.688 3.208 30.796 2.688
 7 1.321 2.730 2.648 31.079 2.730

61.44 29.74 W1617
 1.600 .010 .016
 1.820 .100 .144
 2.440 .300 .308
 3.620 1.025 .908
 6.088 1.745 1.226

W1617S

N = 6 SPREAD = 29.7

| N | APPARENT VELOCITY | DIP | LAYER THICKNESS AT ORIGIN |
|---|----------------------|-----|------------------------------|
| 1 | 1.440 | 0 | .016 |
| 2 | 1.600 | 0 | .144 |
| 3 | 1.820 | 0 | .308 |
| 4 | 2.440 | 0 | .908 |
| 5 | 3.620 | 0 | 1.226 |
| 6 | 6.080 | 0 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .016 | .016 | 1.440 | .016 | .016 |
| 2 | .160 | .144 | 1.600 | .144 | .160 |
| 3 | .468 | .308 | 1.820 | .308 | .468 |
| 4 | 1.376 | .908 | 2.440 | .908 | 1.376 |
| 5 | 2.602 | 1.226 | 3.620 | 1.226 | 2.602 |
| 6 | | | 6.08 | | |

| LAYER | RAY TO LAYER X Y | CRITICAL DIST | RAY FROM LAYER X Y |
|-------|------------------------|---------------|--------------------------|
| | 0.00 0.00 | | 29.74 0.00 |
| 1 | .033 .016 | .066 | 29.707 .016 |
| 2 | .286 .160 | .573 | 29.454 .160 |
| 3 | .482 .468 | .963 | 29.258 .468 |
| 4 | 1.086 1.376 | 2.171 | 28.654 1.376 |
| 5 | 1.446 2.602 | 2.892 | 28.294 2.602 |

61.44 26.70 W1819
 1.600 .010 .016
 1.840 .125 .179
 2.320 .430 .430
 3.310 1.205 .975
 5.660 2.310 1.763

W1819S

N = 6 SPREAD = 26.7

| N | APPARENT VELOCITY | DIP | LAYER THICKNESS AT ORIGIN |
|---|----------------------|-----|------------------------------|
| 1 | 1.440 | 0 | .016 |
| 2 | 1.600 | 0 | .179 |
| 3 | 1.840 | 0 | .430 |
| 4 | 2.320 | 0 | .975 |
| 5 | 3.310 | 0 | 1.763 |
| 6 | 5.660 | 0 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .016 | .016 | 1.440 | .016 | .016 |
| 2 | .195 | .179 | 1.600 | .179 | .195 |
| 3 | .625 | .430 | 1.840 | .430 | .625 |
| 4 | 1.600 | .975 | 2.320 | .975 | 1.600 |
| 5 | 3.363 | 1.763 | 3.310 | 1.763 | 3.363 |
| 6 | | | 5.66 | | |

| LAYER | RAY TO LAYER X Y | CRITICAL DIST | RAY FROM LAYER X Y |
|-------|------------------------|---------------|--------------------------|
| | 0.00 0.00 | | 26.70 0.00 |
| 1 | .033 .016 | .066 | 26.667 .016 |
| 2 | .335 .195 | .671 | 26.365 .195 |
| 3 | .743 .625 | 1.486 | 25.957 .625 |
| 4 | 1.352 1.600 | 2.704 | 25.348 1.600 |
| 5 | 1.914 3.363 | 3.828 | 24.786 3.363 |

61.44 22.65 W2021
 1.600 .010 .016
 1.890 .125 .165
 2.350 .490 .509
 3.390 1.105 .741
 5.680 2.075 1.631

W20215

N = 6 SPREAD = 22.6

N APPARENT DIP LAYER THICKNESS
VELOCITY AT ORIGIN

| | | | |
|---|-------|---|-------|
| 1 | 1.440 | 0 | .016 |
| 2 | 1.600 | 0 | .165 |
| 3 | 1.890 | 0 | .509 |
| 4 | 2.350 | 0 | .741 |
| 5 | 3.390 | 9 | 1.631 |
| 6 | 5.640 | 0 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .016 | .016 | 1.440 | .016 | .016 |
| 2 | .181 | .165 | 1.600 | .165 | .181 |
| 3 | .690 | .509 | 1.890 | .509 | .690 |
| 4 | 1.431 | .741 | 2.350 | .741 | 1.431 |
| 5 | 3.062 | 1.631 | 3.390 | 1.631 | 3.062 |
| 6 | | | 5.68 | | |

| LAYER | RAY TO LAYER | CRITICAL DIST | RAY FROM LAYER |
|-------|--------------|---------------|----------------|
| | X Y | | X Y |
| 1 | 0.00 0.00 | | 22.65 0.00 |
| 2 | .033 .016 | .066 | 22.617 .016 |
| 3 | .281 .181 | .562 | 22.369 .181 |
| 4 | .855 .690 | 1.709 | 21.795 .690 |
| 5 | 1.150 1.431 | 2.301 | 21.500 1.431 |
| 6 | 1.782 3.062 | 3.564 | 20.868 3.062 |

61.44 45.77 W224248
 1.600 .010 .016
 1.829 +0.17 .266
 2.331 +0.45 .281
 2.906 +0.32 .535
 5.903 -1.031 1.100

W224248S

N = 6 SPREAD = 45.8

N APPARENT DIP LAYER THICKNESS
VELOCITY AT ORIGIN

| | | | |
|---|-------|--------|-------|
| 1 | 1.440 | 9 | .016 |
| 2 | 1.600 | 8 | .266 |
| 3 | 1.829 | .170 | .281 |
| 4 | 2.331 | .450 | .535 |
| 5 | 2.906 | .320 | 1.100 |
| 6 | 5.903 | -1.030 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .016 | .016 | 1.440 | .016 | .016 |
| 2 | .292 | .266 | 1.600 | .130 | .146 |
| 3 | .563 | .281 | 1.829 | .057 | .204 |
| 4 | 1.098 | .535 | 2.331 | .639 | .842 |
| 5 | 2.198 | 1.100 | 2.906 | 2.179 | 3.021 |
| 6 | | | 5.90 | | |

| LAYER | RAY TO LAYER | CRITICAL DIST | RAY FROM LAYER |
|-------|--------------|---------------|----------------|
| | X Y | | X Y |
| 1 | 0.00 0.00 | | 45.77 0.00 |
| 2 | .033 .016 | .066 | 45.737 .016 |
| 3 | .505 .281 | 1.003 | 45.513 .147 |
| 4 | .633 .558 | 1.247 | 45.500 .205 |
| 5 | 1.162 1.092 | 2.303 | 44.752 .848 |
| 6 | .967 2.215 | 2.014 | 44.281 2.993 |

51.44 41.00 W24A229
 1.600 .310 .016
 1.941 -0.17 .148
 3.396 +0.031.160
 5.718 -0.181.870

W24A229S

N = 5 SPREAD = 41.0

| N | APPARENT VELOCITY | DIP | LAYER THICKNESS AT ORIGIN |
|---|----------------------|--------|------------------------------|
| 1 | 1.440 | 0 | .016 |
| 2 | 1.600 | 0 | .148 |
| 3 | 1.941 | -0.170 | 1.160 |
| 4 | 3.396 | .030 | 1.870 |
| 5 | 5.718 | -0.181 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .016 | .016 | 1.440 | .016 | .016 |
| 2 | .164 | .148 | 1.600 | .270 | .286 |
| 3 | 1.324 | 1.160 | 1.941 | 1.017 | 1.303 |
| 4 | 3.194 | 1.870 | 3.396 | 2.020 | 3.323 |
| 5 | | | 5.72 | | |

| LAYER | RAY TO LAYER X Y | CRITICAL DIST | RAY FROM LAYER X Y |
|-------|------------------------|---------------|--------------------------|
| 1 | 0.00 0.00 | | 41.00 0.00 |
| 2 | .033 .016 | .066 | 40.967 .016 |
| 3 | .231 .165 | .466 | 40.591 .274 |
| 4 | .894 1.324 | 1.786 | 40.141 1.303 |
| 5 | 1.825 3.290 | 3.672 | 39.067 3.317 |

51.44 32.14 W26A27A
 1.600 .310 .016
 2.130 .270 .307
 2.990 .750 .616
 4.140 1.340 1.013
 5.280 1.735 .866

W26A27AS

N = 5 SPREAD = 32.1

| N | APPARENT VELOCITY | DIP | LAYER THICKNESS AT ORIGIN |
|---|----------------------|-----|------------------------------|
| 1 | 1.440 | 0 | .016 |
| 2 | 1.600 | 0 | .307 |
| 3 | 2.130 | 0 | .616 |
| 4 | 2.990 | 0 | 1.013 |
| 5 | 4.140 | 0 | .866 |
| 6 | 5.280 | 0 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .016 | .016 | 1.440 | .016 | .016 |
| 2 | .323 | .307 | 1.600 | .307 | .323 |
| 3 | .939 | .616 | 2.130 | .616 | .939 |
| 4 | 1.952 | 1.013 | 2.990 | 1.013 | 1.952 |
| 5 | 2.818 | .866 | 4.140 | .866 | 2.818 |
| 6 | | | 5.28 | | |

| LAYER | RAY TO LAYER X Y | CRITICAL DIST | RAY FROM LAYER X Y |
|-------|------------------------|---------------|--------------------------|
| 1 | 0.00 0.00 | | 32.14 0.00 |
| 2 | .033 .016 | .066 | 32.107 .016 |
| 3 | .364 .323 | .728 | 31.776 .323 |
| 4 | .829 .939 | 1.657 | 31.311 .939 |
| 5 | 1.562 1.952 | 3.124 | 30.579 1.952 |
| 6 | 2.164 2.818 | 4.328 | 29.976 2.818 |

61.44 34.44 W268279
 1.600 .010 .016
 2.100 .360 .424
 3.430 1.060 .757
 4.430 1.959 .959
 6.880 2.830 3.243

W268279S

N = 6 SPREAD = 34.4

| N | APPARENT VELOCITY | DIP | LAYER THICKNESS AT ORIGIN |
|---|----------------------|-----|------------------------------|
|---|----------------------|-----|------------------------------|

| | | | |
|---|-------|---|-------|
| 1 | 1.440 | 0 | .016 |
| 2 | 1.600 | 0 | .424 |
| 3 | 2.100 | 0 | .757 |
| 4 | 3.430 | 0 | .959 |
| 5 | 4.430 | 0 | 3.243 |
| 6 | 6.880 | 0 | |

| N | DEPTH A | THICK A | VELOCITY | THICK B | DEPTH B |
|---|---------|---------|----------|---------|---------|
| 1 | .016 | .016 | 1.440 | .016 | .016 |
| 2 | .440 | .424 | 1.600 | .424 | .440 |
| 3 | 1.197 | .757 | 2.100 | .757 | 1.197 |
| 4 | 2.156 | .959 | 3.430 | .959 | 2.156 |
| 5 | 5.399 | 3.243 | 4.430 | 3.243 | 5.399 |
| 6 | | | 6.88 | | |

| LAYER | RAY TO LAYER | | CRITICAL DIST | RAY FROM LAYER | |
|-------|--------------|-------|---------------|----------------|-------|
| | X | Y | | X | Y |
| | 0.00 | 0.00 | | 34.44 | 0.00 |
| 1 | .033 | .016 | .066 | 34.407 | .016 |
| 2 | .514 | .440 | 1.028 | 33.926 | .440 |
| 3 | .817 | 1.197 | 1.634 | 33.623 | 1.197 |
| 4 | 1.751 | 2.156 | 3.501 | 32.609 | 2.156 |
| 5 | 3.628 | 5.399 | 7.256 | 30.812 | 5.399 |

VI

PROGRAM TO COMPUTE CORRECTIONS TO
HELICOPTER-RECORDED DATA (BEAUHELI)
AND INPUT AND OUTPUT DATA FOR PROCESSED LINES


```

PROGRAM PEAUHETI
PI=3.1415926536
DTR=PI/180.
PTD=180./PI
READ(5,100)AID1,AID2
100 FORMAT(2A8)
READ(5,105)IYRM01,IDA1,IHR1,MIN1,DIF1,IYRM02,
1 IDA2,IHR2,MIN2,DIF2
IF(IYRM01.NE.IYRM02)GO TO 5
105 FORMAT(2(I4,I2,X,2I2,X,F6.2))
GO TO 10
5 WRITE(6,110)IYRM01,IYRM02
110 FORMAT(12 CLOCK CORR YN *,I4,*, DIFFERS FROM YN *,I4)
CALL EXIT
10 TIM1=IDA1*86200+IHR1*3600+MIN1*60
TIM2=IDA2*86200+IHR2*3600+MIN2*60
READ(5,115)ISBYN,ISBD,ISBH,ISBP,ISBN,ISBP
115 FORMAT(I4,I2,X,2I2,X,2I2)
SBTIM=ISBD*86200+ISBH*3600+ISBP*60
READ(5,120)CLK,SLK,WATVELK,DBE,DBE,TDIST,DR,DBR
120 FORMAT(8F8.3)
WRITE(6,125)AID1,AID2
125 FORMAT(2 *,2A8)
WRITE(6,130)IYRM01,IDA1,IHR1,MIN1,DIF1
130 FORMAT(12 PRESOT TIME CHECK *,I4,I2,X,2I2,*, DELTA T= *,
1 F7.3)
WRITE(6,135)IYRM02,IDA2,IHR2,MIN2,DIF2
135 FORMAT(12 POSTSHOT TIME CHECK *,I4,I2,X,2I2,
1 *, DELTA T= *,F7.3)
WRITE(6,140)
140 FORMAT(12 ALL DISTANCES IN KILOMETERS, ALL VELOCITIES *,
1 *,IN KM/SEC, ALL TIMES ARE UNIVERSAL TIME*)
WRITE(6,145)CLK,SLK,WATVELK
145 FORMAT(12 CARLE LENGTH= *,F8.3,*, ACTIVE SECTION *,
1 LENGTH= *,F8.3,*, WATER VELOCITY= *,F8.3)
WRITE(6,147)DBE,DBE,TDIST,DR,DBR
147 FORMAT(12 START DEPTH= *,
1 F8.3,*, END DEPTH= *,F8.3,*, LINE LENGTH= *,F8.3,
2 *, RECEIVER DEPTH= *,F8.3,*, DEPTH AT RECEIVER= *,F8.3)
READ(4,150)NYRM01,NDA1,NHR1,NMN1,NLAT1,ALATM1,NLON1,ALCNM1
150 FORMAT(I4,I2,X,2I2,X,I3,X,F5.2,X,I4,X,F5.2)
ANTIM1=NDA1*86200+NHR1*3600+NMN1*60
ALAT1=(NLAT1+ALATM1/60.)*DTR
ALON1=(NLON1-ALONM1/60.)*DTR
KIT=0
15 READ(4,150)NYRM02,NDA2,NHR2,NMN2,NLAT2,ALATM2,NLON2,ALCNM2
ANTIM2=NDA2*86200+NHR2*3600+NMN2*60
ALAT2=(NLAT2+ALATM2/60.)*DTR
ALON2=(NLON2-ALONM2/60.)*DTR
IF(KIT.EQ.1) GO TO 20
IF(SBTIM.GE.ANTIM1.AND.SBTIM.LE.ANTIM2) GO TO 20
ANTIM1=ANTIM2
ALAT1=ALAT2
ALON1=ALON2
GO TO 15
20 FACTOR=(SBTIM-ANTIM1)/(ANTIM2-ANTIM1)
SBLON=(ALON2-ALON1)*FACTOR+ALON1
SBLAT=(ALAT2-ALAT1)*FACTOR+ALAT1
SBLDP=SBLON*PTD
SBLAP=SBLAT*PTD
WRITE(6,155)ISBN,ISBP,ISBYN,ISBD,ISBH,ISBN,SELAP,SBLDP
155 FORMAT(12 SONOBUOY *,I2,*, AT POSITION *,I2,

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```

1 * TIME #,I4,I2,X,2I2,# LAT #,F7.3,# LONG #,F8.3)
WRITE(6,160)
160 FORMAT(10YRMODA SHOT LATITUDE LONGITUDE SIZE BURN #,
1 * DEPTH SDIST CADIS TRAVT TTRAW SURF BOTC #,
2 *CLKC SCOR SHOTTIME SPVEL SPVELC#)
KIT=1
25 READ(5,165) ISHOT,SIZE,BURN,DEPK,DIST,KSYM,KSDA,
1 KSHR,KSMN,SSEC,KHHR,KHMN,HSEC,SPVEL
IF(EOF(5)) CALL EXIT
165 FORMAT(1I5,4F5.2,X,I4,I2,X,2I2,X,F5.2,X,2I2,X,F5.2,X,F6.5)
SHORTIM=KSDA*86200+KSHR*3600+KSMN*60+SSEC-BURN
28 IF(SHORTIM.GE.ANTIM1.AND.SHORTIM.LT.ANTIM2)GO TO 30
ANTIM1=ANTIM2
ALAT1=ALAT2
ALON1=ALON2
GO TO 15
30 FACTOR=(SHORTIM-ANTIM1)/(ANTIM2-ANTIM1)
SHLON=(ALON2-ALON1)*FACTOR+ALON1
SHLAT=(ALAT2-ALAT1)*FACTOR+ALAT1
ARG=SINF(ALAT1)*SINF(ALAT2)+
1 COSF(ALAT1)*COSF(ALAT2)*COSF(ALON2-ALON1)
PDIST=6359.859*ACOSF(ARG)
ARG=SINF(SBLAT)*SINF(SHLAT)+
1 COSF(SBLAT)*COSF(SHLAT)*COSF(SHLON-SBLON)
SDIST=6359.859*ACOSF(ARG)
SPVELC=PDIST/(ANTIM2-ANTIM1)
SHOTX=SPVEL*BURN-SLK-CLK
SHOTZ=(-40.55+1.513*BURN)/1000.
IF(SHOTZ.GT.DEPK)SHOTZ=DEPK
SHCOR=SQRT(SHOTX*SHOTX+SHOTZ*SHOTZ)/WATVELK
STIMC=SSEC-SHGOR
SHTIMC=SHORTIM+BURN-SHGOR
CKCOR=DIF1+(DIF2-DYF1)*(SHORTIM-TIM1)/(TIM2-TIM1)
ARTIMH=KSDA*86200+KHHR*3600+KHMN*60+HSEC+CKCOR
TTRAW=ARTIMH-SHTIMC
TDEP=DBB+(DBE-DBB)*DIST/TDIST
S1=SQRT(1.-WATVELK*WATVELK/5./5.)
SURFCOR=(DR+SHOTZ)*S1/WATVELK
BOTCOR=(TDEP-DEPK+DBB-CBR)*S1/WATVELK
TTCOR=TTRAW+SURFCOR+BOTCOR
SHLON=SHLON*OTD
LLON=SHLON
ALONH=-(SHLON-LLON)*60.
SHLAT=SHLAT*OTD
LLAT=SHLAT
ALATH=(SHLAT-LLAT)*60.
WRITE(6,170)KSYM,KSDA,ISHOT,LLAT,ALATH,LLON,ALONH,
1 SIZE,BURN,DEPK,SDIST,DIST,TTCOR,TTRAW,SURFCOR,BOTCOR,
2 CKCOR,SHCOR,KSHR,KSMN,STIMC,SPVEL,SPVELC
WRITE(7,175)KSYM,KSDA,ISHOT,LLAT,ALATH,LLON,ALONH,
1 SIZE,BURN,DEPK,SDIST,DIST,TTCOR,TTRAW,SURFCOR,BOTCOR,
2 CKCOR,SHCOR,KSHR,KSMN,STIMC,SPVEL,SPVELC
170 FORMAT(1X,I4,I2,X,I4,X,I3,X,F5.2,X,I4,X,F5.2,X,F5.1,F5.1,
1 F6.3,4F6.2,4F5.2,X,2I2,F6.2,2F7.5)
175 FORMAT(1I4,I2,X,I4,X,I3,X,F5.2,X,I4,X,F5.2,X,F5.1,F6.1,
1 F6.3,4F6.2,4F5.2,X,2I2,F6.2,2F7.5)
GO TO 25
END

```

[illegible]

AID1, AID2 : Line Identification.

IYRMOI, IDA1, IHR1, MIN1: Year, month, day, hour and minute of the preshot time check.

LYRM02,IDA2,IHK2,MIN2: Year,month,day,hour and minute of the postshot time check.

DIF) : Clock correction (Time difference between the ship's master clock and the helicopter's clock) of preshot time check.

DIF2 : Clock correction of postshot time check.

ISBYM, ISBU, ISBH, ISBM : Year, month, day, hour and minute of the sunobuuy's drop.

ISBN : Sonobuoy number.

158P : Sonobuoy position.

CLK : Cable length in kilometers.

SLK : Streamer length (active section only) in kilometers.

WATER VELOCITY: Water velocity.

: Depth to the bottom at the beginning of the line.

: Depth to the bottom at the end of the line.

TDIST : End to end spread length (Total distance).

DR : Depth of the receiver (Hydrophone depth).

DBR : Depth to bottom at the receiver (Offset depth based on some average basement velocity).

1SHOT
: Shot number.

SIZE : Size of the shot in pounds.

Burn time:

DEPK : Depth to the bottom at the shot point in kilometers (Offset depth).

DIST : Estimated drift distance between shot and sonobuoy computed manually.

KSMA, KSDA, KSHR, KSMN, SSEC : Year, month, day, hour, minute and second of the shot.

KHHR, KH₄N, HSEC : Hour, minute and second of the helicopter ground arrival.

SPVEL : Ship velocity.

NAVIGATION INPUT FORMAT FOR PROGRAM BEAUNELI

| TITLE(I) | | | | | | | |
|----------|------|------|------|-------|--------|-------|--------|
| NYRMO1 | NDA1 | NHR1 | NMN1 | NLAT1 | ALATM1 | NLON1 | ALONM1 |
| . | . | . | . | . | . | . | . |
| . | . | . | . | . | . | . | . |
| NYRMOK | NDAK | NHRK | NMNK | NLATK | ALATMK | NLONK | ALONMK |

TITLE(I) : Line identification.
 K : Number of ship's navigation points for the profile.
 I=1,.....,K : Ship's navigation points number.
 NYRMO(I) }
 NDA(I) } : Year, month, day, hour and minute of navigation points.
 NHR(I) }
 NMN(I) }
 NLAT(I) } : Position in latitude (degrees and minutes) of the ship's navigation points.
 ALATM(I) }
 NLON(I) } : Position in longitude (degrees and minutes) of the ship's navigation points.
 ALONM(I) }

[illegible]

| | | | | | | | | | |
|----------------------|--|---------|--|---------|--|---------------------|--|------------|--|
| LARE, UNIVERSAL TIME | | | | | | | | | |
| ELOCITY = WATERK | | | | | | | | | |
| RECEIVER | | DEPTH = | | UK | | DEPTH AT RECEIVER = | | DBR | |
| SBLUP | | | | | | | | | |
| TRAVT | | TRAM | | S,URFC | | BOTLS | | SLKC, SCOR | |
| TTCON | | TRAM | | SUMECOR | | BOTQUA | | EKCOR | |
| | | | | | | | | SHASUM | |
| | | | | | | | | STIME | |
| | | | | | | | | SPVEL | |
| | | | | | | | | SPVELC | |

OUTPUT FORMAT FOR PROGRAM BEAUHEL1

SBLAP,SBLOP : Sonobuoy position in latitude and longitude.
 KSYM,KSDA : Year,month and day of the shot.
 LLAT,ALATM : Shot position in latitude (degrees and minutes).
 LLON,ALONM : Shot position in longitude (degrees and minutes).
 SUIST : Corrected distance between shot and sonobuoy computed mathematically.
 TTCOR : Corrected travel time including all corrections.
 TTRAW : Travel time including shot and clock corrections but without any bottom or surface corrections.
 SURFCOR : Surface correction.
 BOTCOR : Bottom correction.
 CLKOR : Clock correction between ship and helicopter.
 SHCOR : Total corrections for shot time.
 KSHR,KSYM,STIME : Corrected shot time in hours,minutes and seconds.
 SPVEL : Ship velocity.
 SPVELC : Corrected ship velocity.
 A101,A102,IYMM01,10A1,IHRT,MINT,IYMM02,10A2,IHM2,MIN2,DIF1,DIF2,JSBYM,JSBD,JSBH,JSBM,JSBP,CLK,SLK,MATVELK,DBB,
 DBE,TD1ST,DR,DBR,ISHOT,SIZE,BURN,DEPK,DIST: All the same as in input file.

BEAU76 LINE 22A-23 HELICOPTER

760817 0350 0.018 760817 1023 0.022

760817 0500 522
 0.061 0.00457 1.440 0.019 0.014 70.0 0.0183 0.020
 341 120-135.0 -020 37.6 760817 0730 55.61 0739 03.07 -00474
 342 120-135.0 -020 39.0 760817 0743 49.52 0743 58.07 -00474
 343 120-190.0 -020 42.2 760817 0754 51.11 0754 59.35 -00474
 344 240-192.3 -020 44.6 760817 0802 27.99 0802 36.04 -00474
 345 240-190.3 -020 45.6 760817 0807 46.29 0808 55.34 -00474
 346 240-192.9 -020 47.1 760817 0816 51.50 0817 00.75 -00474
 347 240-188.5 -020 48.5 760817 0825 03.07 0825 12.71 -00474
 348 360-265.7 -020 50.8 760817 0836 19.03 0836 29.79 -00474
 349 480-348.0 -019 54.4 760817 0852 00.14 0852 10.24 -00474
 350 480-199.8 -019 59.3 760817 0907 28.15 0907 39.70 -00474
 351 600-192.9 -020 69.0 760817 0932 22.44 0932 35.40 -00474

BEAU76 NAV22

763817 0500 71 00.18 -152 00.20
 760817 0520 70 59.18 -151 54.48
 760817 0540 70 57.90 -151 47.18
 760817 0600 70 56.68 -151 38.28
 760817 0620 70 56.10 -151 27.78
 760817 0640 70 55.30 -151 17.78
 760817 0700 70 53.90 -151 08.38
 760817 0720 70 53.90 -151 08.38
 760817 0740 70 52.90 -151 00.48
 760817 0800 70 51.40 -150 58.78
 760817 0828 70 47.20 -150 58.00
 760817 0850 70 45.00 -150 42.00
 760817 0908 70 44.00 -150 39.08
 760817 0926 70 42.50 -150 24.50
 760817 0938 70 39.59 -150 12.78

PEAU76 HELI22

PPESHOT TIME CHECK 760817 350 DELTA I= .018

POSTSHOT TIME CHECK 760817 1023 DELTA I= .022

ALL DISTANCES IN KILOMETERS, ALL VELOCITIES IN KM/SEC, ALL TIMES ARE UNIVERSAL TIME

CABLE LENGTH= .061 ACTIVE SECTION LENGTH= .805 WATER VELOCITY= 1.440

START DEPTH= .019 END DEPTH= .019 LINE LENGTH= 78.000 RECEIVER DEPTH= .020

-018 DEPTH AT RECEIVER= .020

SOMCRUOV 5 AT POSITION 22 TIME 760817 5 8 LAT 71.002 LONG -152.083
 WPMODA SHOT LATITUDE LONGITUDE SIZE BURN DEPTH SDIST CADIS TRAVT FTRAM SURF BOTC CLKC SCOR SHOTTIME SPVEL SPWELC
 760817 341 70 53.07 -151 1.71 120.0 135.0 -020 37.64 37.60 7.90 7.88 -03-0.00 -02 40 738 55.21 -00474 -00427
 760817 342 70 52.81 -150 59.64 120.0 135.0 -020 38.99 39.00 7.99 7.97 -03-0.00 -02 40 743 49.12 -00474 -00518
 760817 343 70 52.26 -150 54.73 120.0 190.0 -020 42.17 42.28 8.06 8.04 -03-0.01 -02 58 754 50.53 -00474 -00518
 760817 344 70 51.84 -150 51.06 240.0 192.3 -020 44.49 44.60 9.46 9.46 -03-0.01 -02 59 8 2 27.40 -00474 -00518
 760817 345 70 50.51 -150 50.50 240.0 190.3 -020 45.72 45.68 9.67 9.65 -03-0.00 -02 58 8 8 45.71 -00474 -00710
 760817 346 70 48.66 -150 50.22 240.0 192.9 -020 47.33 47.18 9.88 9.86 -03-0.00 -02 59 816 50.91 -00474 -00710
 760817 347 70 47.06 -150 49.49 240.0 188.5 -020 49.14 48.58 10.26 10.23 -03-0.00 -02 58 825 2.49 -00474 -00353
 760817 348 70 46.33 -150 46.83 360.0 265.7 -020 51.22 50.80 10.03 10.01 -03-0.01 -02 63 836 19.00 -00474 -00353
 760817 349 70 45.27 -150 42.98 480.0 348.0 -019 54.24 54.40 11.22 11.19 -02-0.00 -02 1.87 852 -0.93 -00474 -00353
 760817 350 70 43.76 -150 36.69 480.0 199.8 -019 58.97 59.38 12.21 12.18 -02-0.00 -02 61 9 7 27.54 -00474 -00595
 760817 351 70 41.73 -150 21.39 600.0 192.9 -020 68.91 69.08 13.59 13.57 -03-0.00 -02 59 932 21.85 -00474 -01251

BEAU76 LINE 24A-25 HELICOPTER
 760017 1023 0.022 760010 1400 0.04
 760010 0306 1626
 0.061 0.00457 1.440 0.017 70. 0.0183 0.016
 382 120.136.7 -0.1024.67 760010 0515 22.89 0519 30.14 -0.0402
 383 120.138.5 -0.1030.45 760010 0523 24.13 0523 31.56 -0.0402
 384 120.138.2 -0.1032.00 760010 0527 54.00 0528 01.61 -0.0402
 385 240.163.0 -0.1035.98 760010 0531 53.86 0539 02.04 -0.0402
 386 240.192.1 -0.1039.35 760010 0549 50.02 0550 06.57 -0.0402
 387 240.192.3 -0.1041.00 760010 0558 10.60 0558 27.05 -0.0402
 388 240.182.7 -0.1044.50 760010 0607 00.02 0607 10.37 -0.0402
 389 360.208.4 -0.1049.00 760010 0620 34.93 0620 44.99 -0.0402
 390 360.210.0 -0.1052.35 760010 0633 51.94 0634 02.29 -0.0402
 391 480.211.2 -0.1057.80 760010 0650 39.94 0650 51.29 -0.0402
 392 480.217.8 -0.1062.95 760010 0709 54.03 0710 06.24 -0.0402
 393 660.213.0 -0.1068.55 760010 0726 46.00 0726 59.25 -0.0402

BEAU76 NAV24
 760010 0300 70 40.35 -150 00.20
 760010 0320 70 41.60 -150 10.70
 760010 0340 70 42.60 -150 20.20
 760010 0400 70 44.20 -150 29.00
 760010 0420 70 45.00 -150 39.20
 760010 0440 70 47.50 -150 40.00
 760010 0500 70 47.40 -150 50.00
 760010 0520 70 49.00 -150 52.00
 760010 0540 70 49.20 -151 05.00
 760010 0600 70 50.60 -151 15.00
 760010 0620 70 52.60 -151 24.50
 760010 0640 70 54.00 -151 33.00
 760010 0700 70 54.00 -151 44.00
 760010 0720 70 55.50 -151 55.00
 760010 0740 70 56.70 -152 00.00

BEAU76 HELI24
 PRESOT TIME CHECK 760017 1023 DELTA T = .022
 POSTSHOT TIME CHECK 760010 14 0 DELTA T = .040
 ALL DISTANCES IN KILOMETERS. ALL VELOCITIES IN KM/SEC. ALL TIMES ARE UNIVERSAL TIME
 CABLE LENGTH = .061 ACTIVE SECTION LENGTH = .017 LINE LENGTH = 70.000 RECEIVER DEPTH = 1.440
 START DEPTH = .017 END DEPTH = .017 LAT 3 6 LAT 70.679 LONG -150.056
 SONOBUOY 16 AT POSITION 24 TIME 760010 3 6 LAT 70.679 LONG -150.056
 YRMODEA SHOT LATITUDE LONGITUDE SIZE BUHM DEPTH SDIST CADIS TRAVI YTRAW SURF BOTC CLKC SCOR SHOTTIME SPVEL SPVELC
 760010 302 70 48.77 -150 51.71 120.0 136.7 -0.10 31.04 29.67 7.72 7.70 -02-00.00 -03 .41 519 22.40 -00402 -00267
 760010 303 70 49.01 -150 52.75 120.0 130.5 -0.10 33.01 30.45 7.91 7.88 -02-00.00 -03 .42 523 23.71 -00402 -00700
 760010 304 70 49.06 -150 55.86 120.0 130.2 -0.10 35.54 32.00 8.09 8.06 -02-00.00 -03 .42 527 53.58 -00402 -00700
 760010 305 70 49.16 -151 3.16 240.0 163.0 -0.10 39.60 35.90 8.74 8.71 -02-00.00 -03 .50 530 53.36 -00402 -00700
 760010 306 70 49.67 -151 A.91 240.0 192.1 -0.10 43.27 39.85 9.21 9.18 -02-00.00 -03 .60 549 57.42 -00402 -00513
 760010 307 70 50.26 -151 12.75 240.0 192.3 -0.10 45.83 41.80 9.71 9.68 -02-00.00 -03 .60 558 10.00 -00402 -00513
 760010 308 70 51.01 -151 16.95 240.0 182.7 -0.10 48.72 44.50 10.18 10.15 -02-00.00 -03 .57 6.7 8.25 -00402 -00571
 760010 309 70 52.31 -151 23.13 360.0 208.4 -0.10 53.11 49.00 10.77 10.75 -02-00.00 -03 .65 620 34.20 -00402 -00571
 760010 310 70 53.33 -151 24.91 360.0 210.0 -0.10 57.06 52.35 11.07 11.04 -02-00.00 -04 .66 633 51.20 -00402 -00480
 760010 311 70 54.00 -151 36.93 480.0 211.2 -0.17 62.82 57.00 12.07 12.05 -02 .00 .04 .66 658 39.20 -00402 -00555
 760010 312 70 54.50 -151 47.45 480.0 211.4 -0.16 68.20 62.95 12.95 12.93 -02 .00 .04 .68 7.9 53.35 -00402 -00607
 760010 313 70 55.79 -151 57.09 660.0 213.0 -0.15 74.57 68.55 13.99 13.96 -02 .00 .04 .67 726 45.33 -00402 -00679

VII
RECORD SECTIONS AND
STRUCTURAL CROSS-SECTIONS

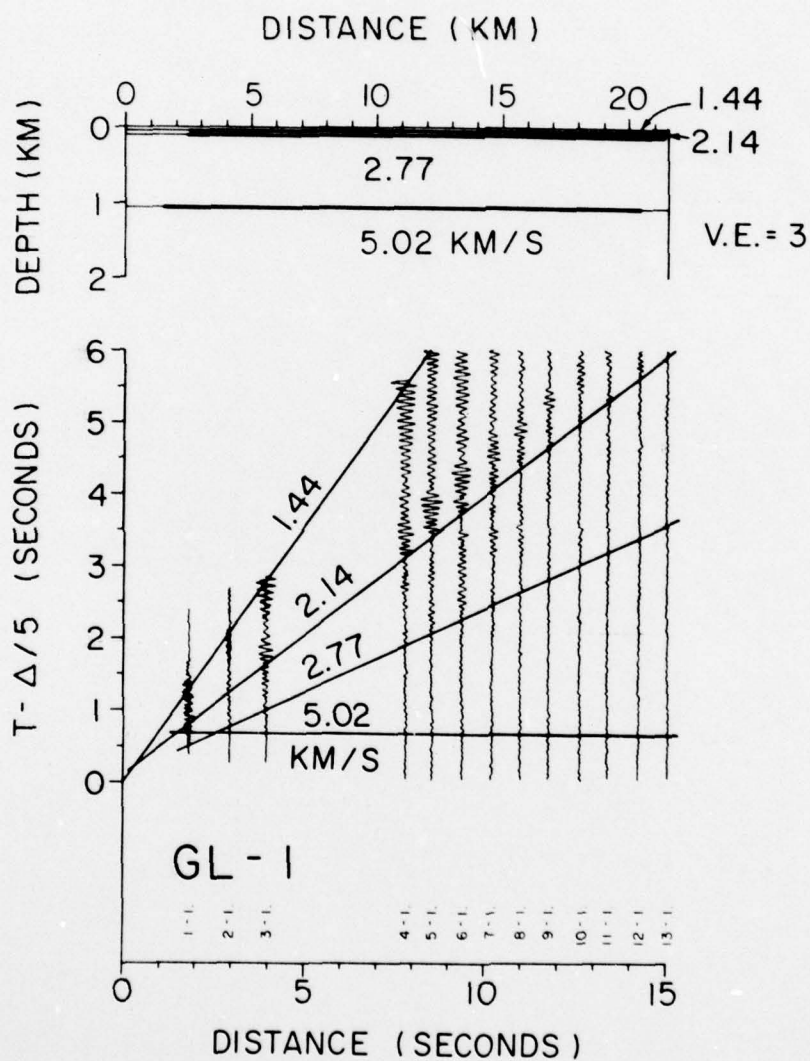


Figure 8. Line GL-1 record section and velocity-depth model interpretation. Below each seismogram is listed the shot number and the charge weight in pounds.

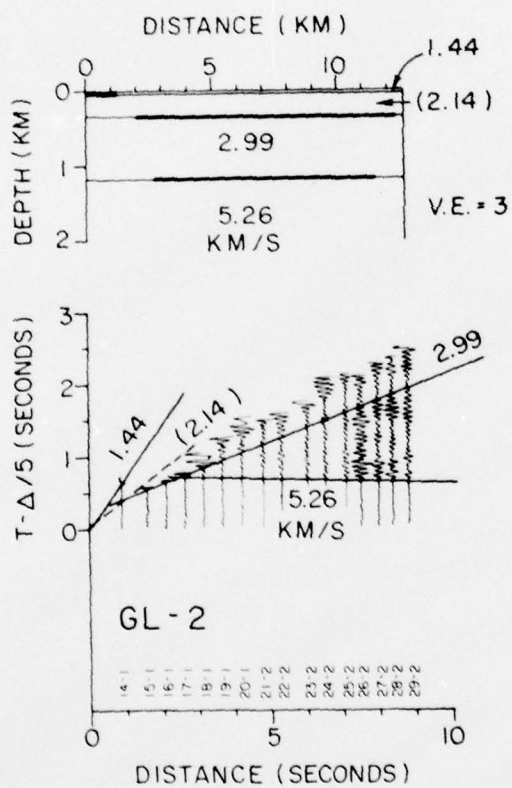


Figure 9. Line GL-2 record section and velocity-depth model interpretation.

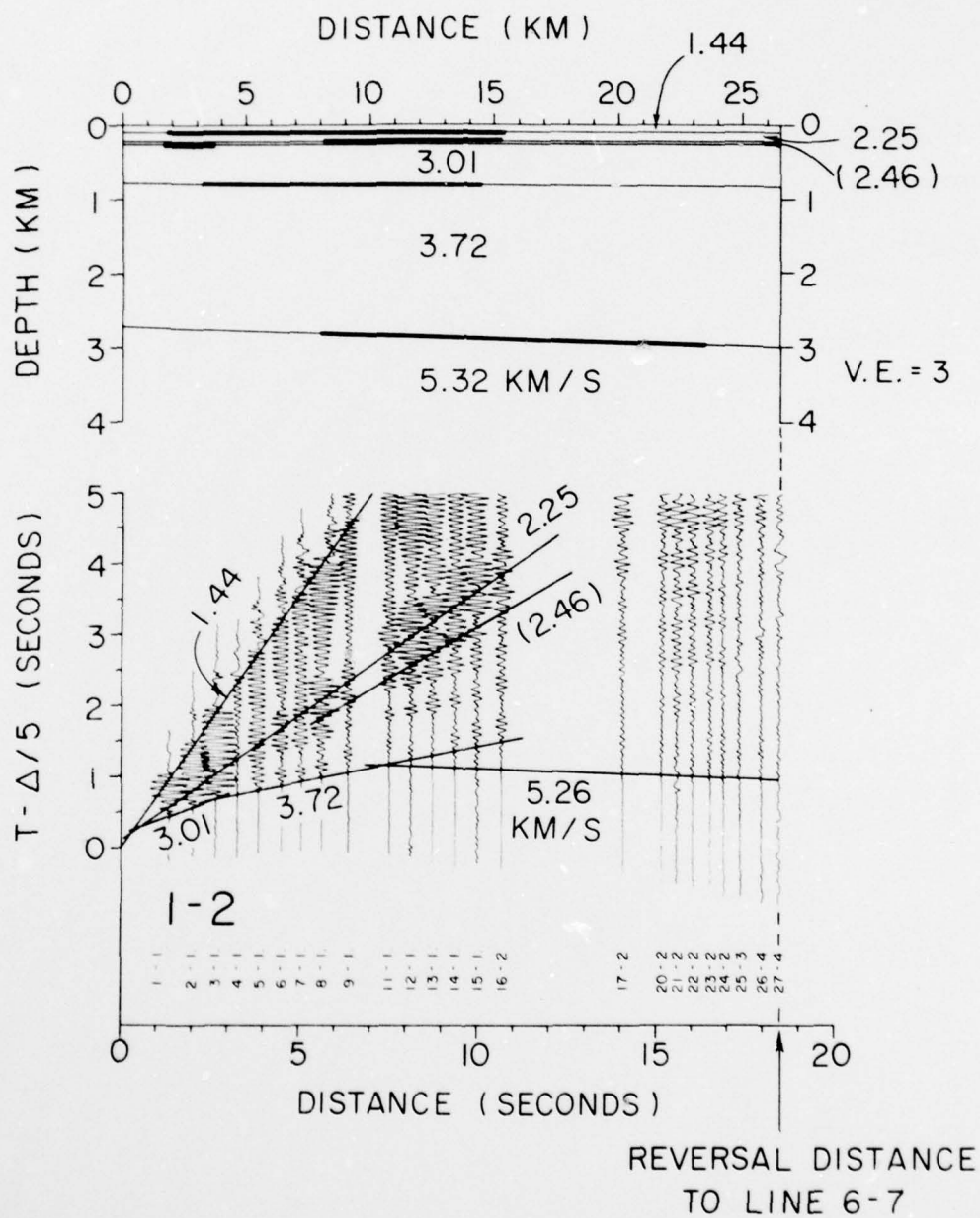


Figure 10. Line 1-2 record section and velocity-depth model interpretation.

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OREGON STATE UNIV CORVALLIS SCHOOL OF OCEANOGRAPHY

F/G 8/11

MARINE SEISMIC REFRACTION DATA BETWEEN WAINWRIGHT INLET AND PRU--ETC(U)

JUN 79 M BEE, S H JOHNSON, E F CHIBURIS

N00014-76-C-0067

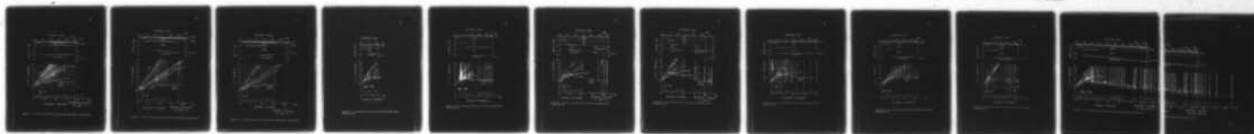
NL

UNCLASSIFIED

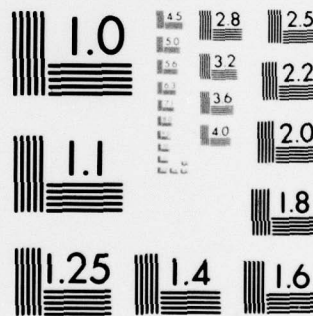
79-9

2 OF 2

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MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

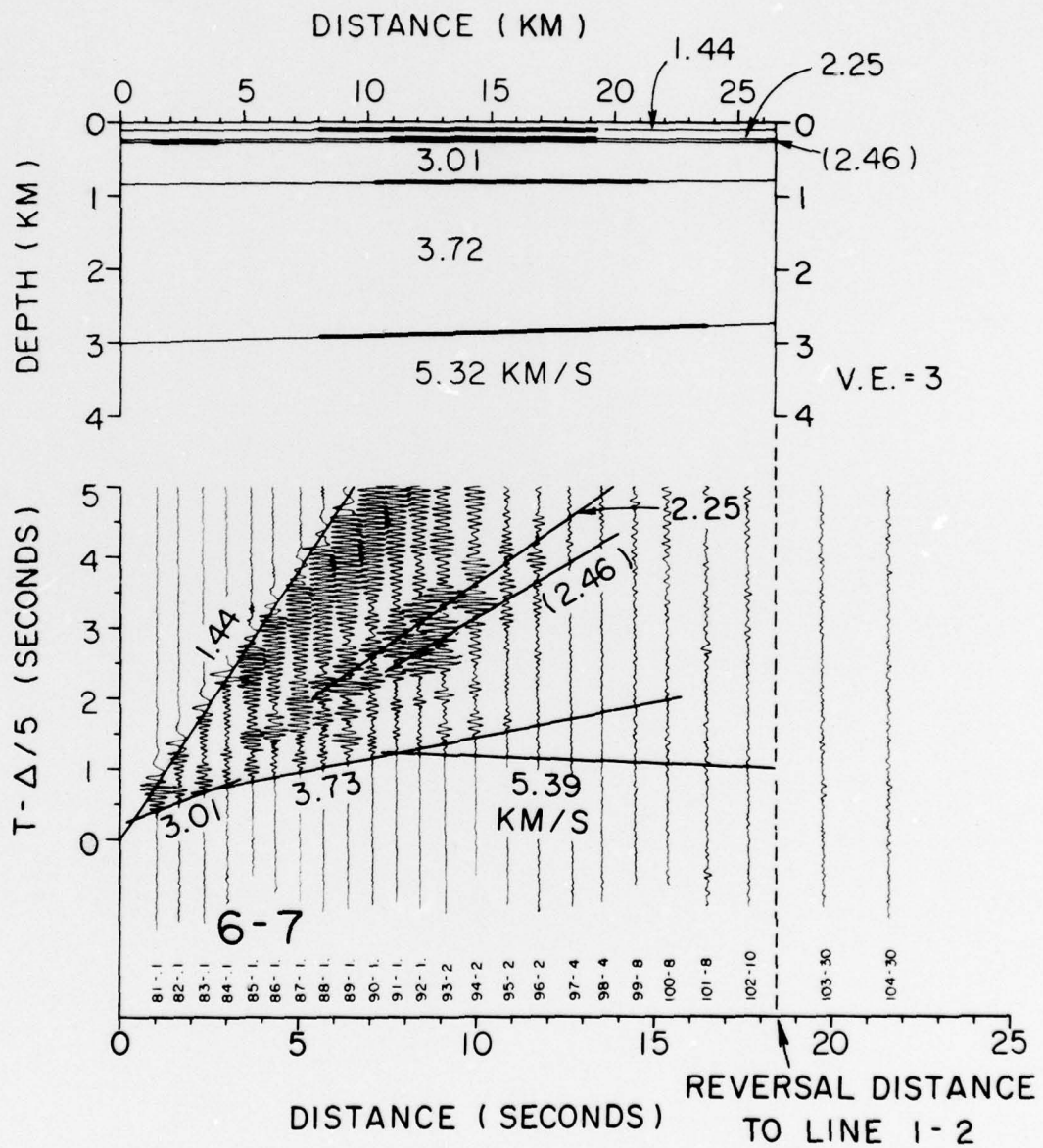


Figure 11. Line 6-7 record section and velocity-depth model interpretation.

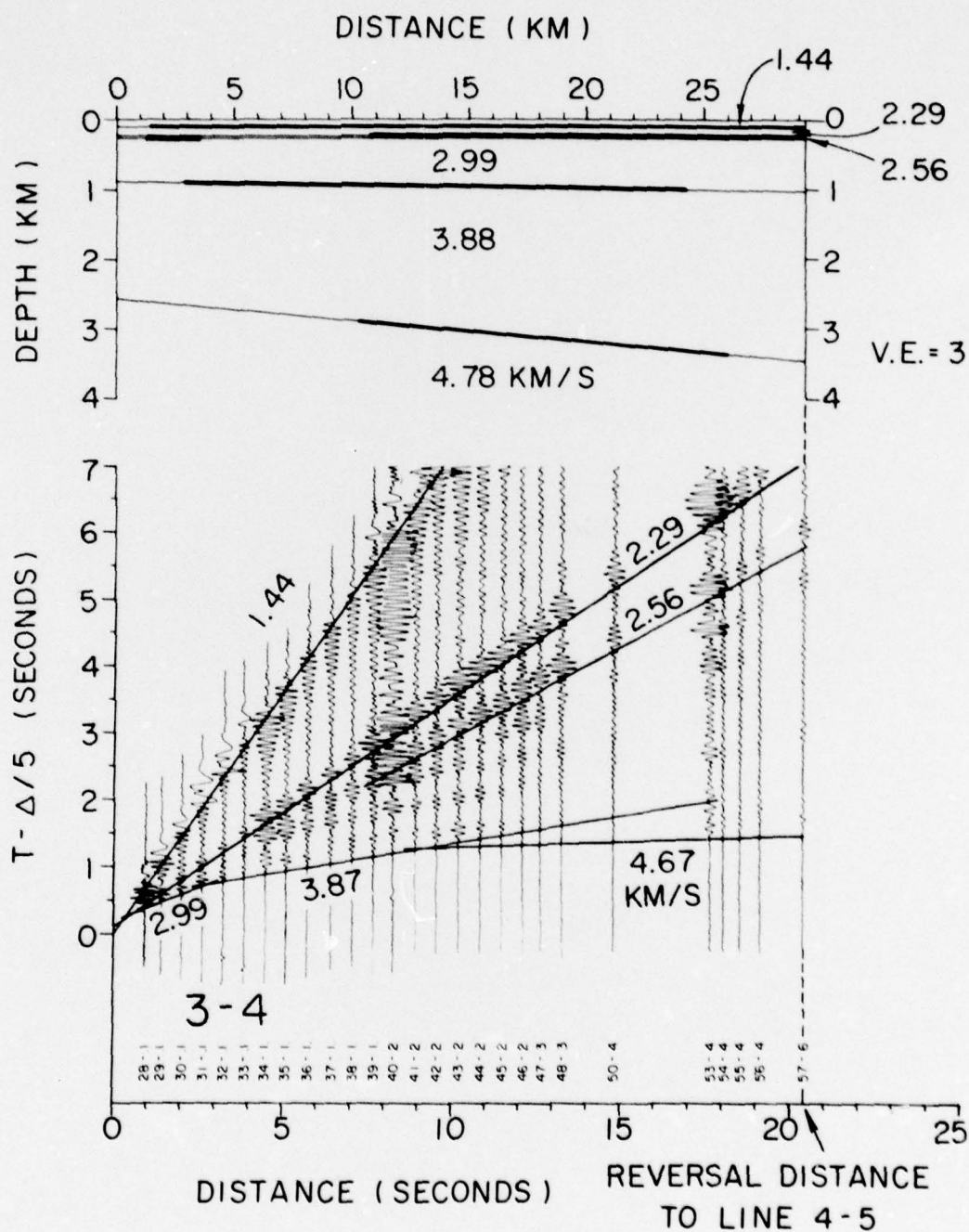


Figure 12. Line 3-4 record section and velocity-depth model interpretation.

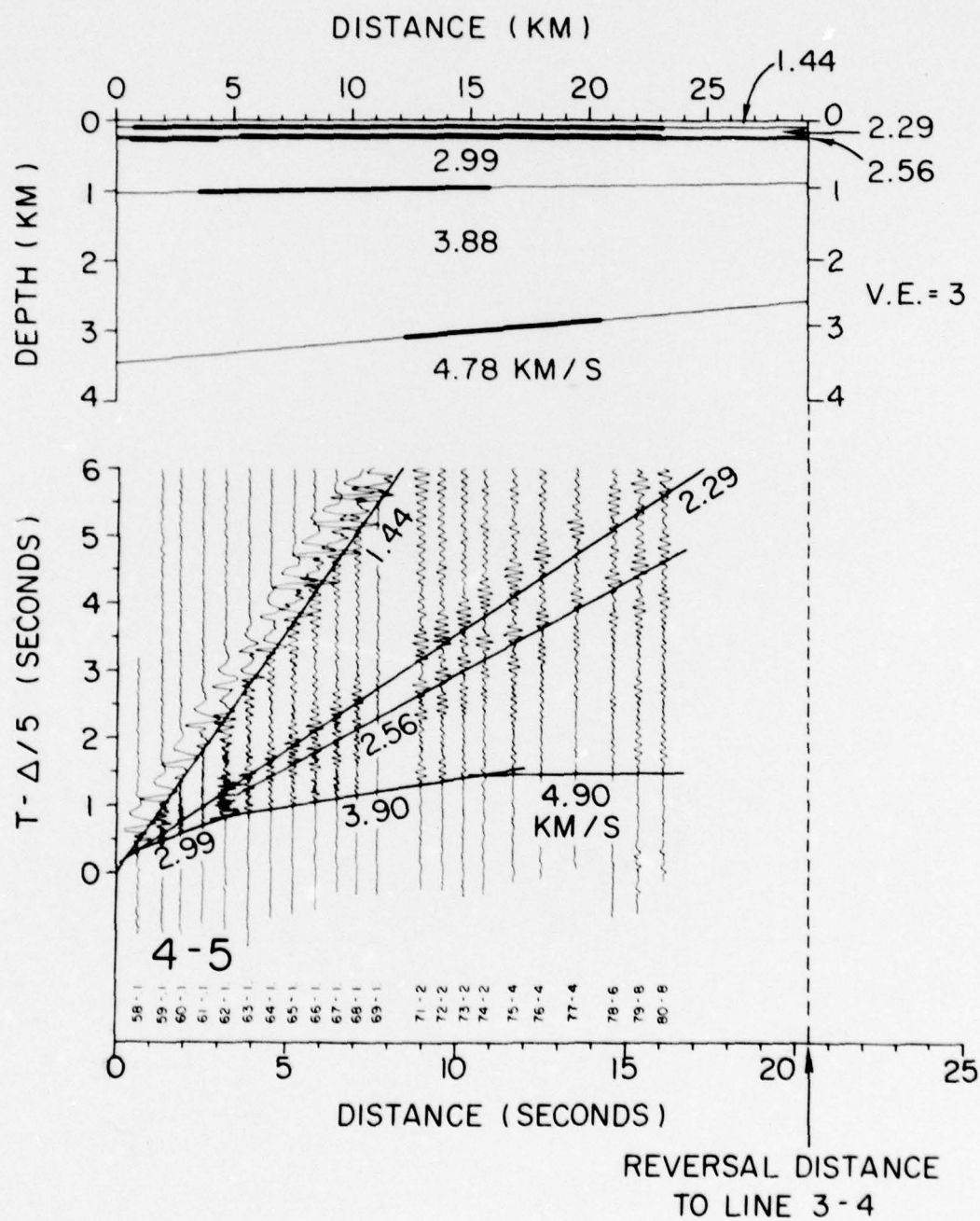


Figure 13. Line 4-5 record section and velocity-depth model interpretation.

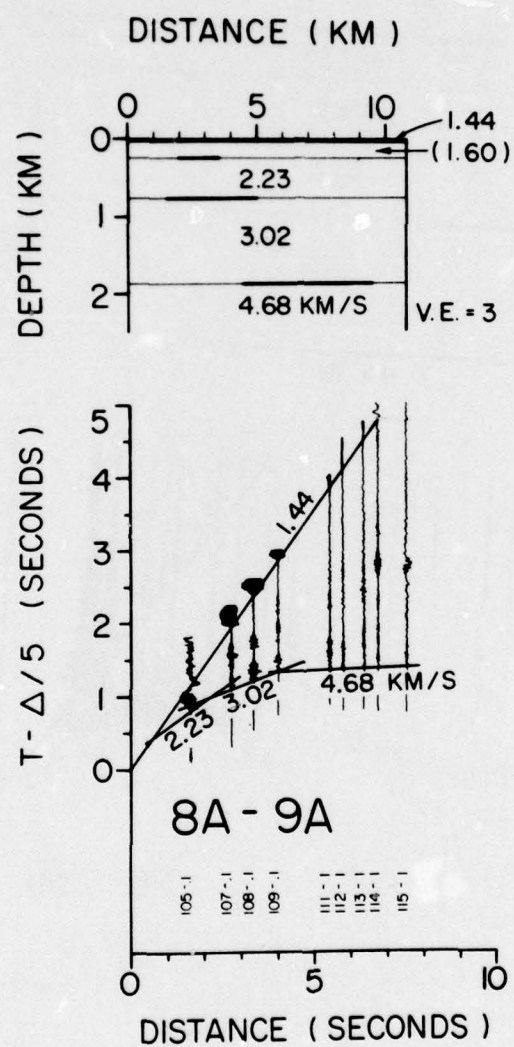


Figure 14. Line 8A-9A record section and velocity-depth model interpretation.

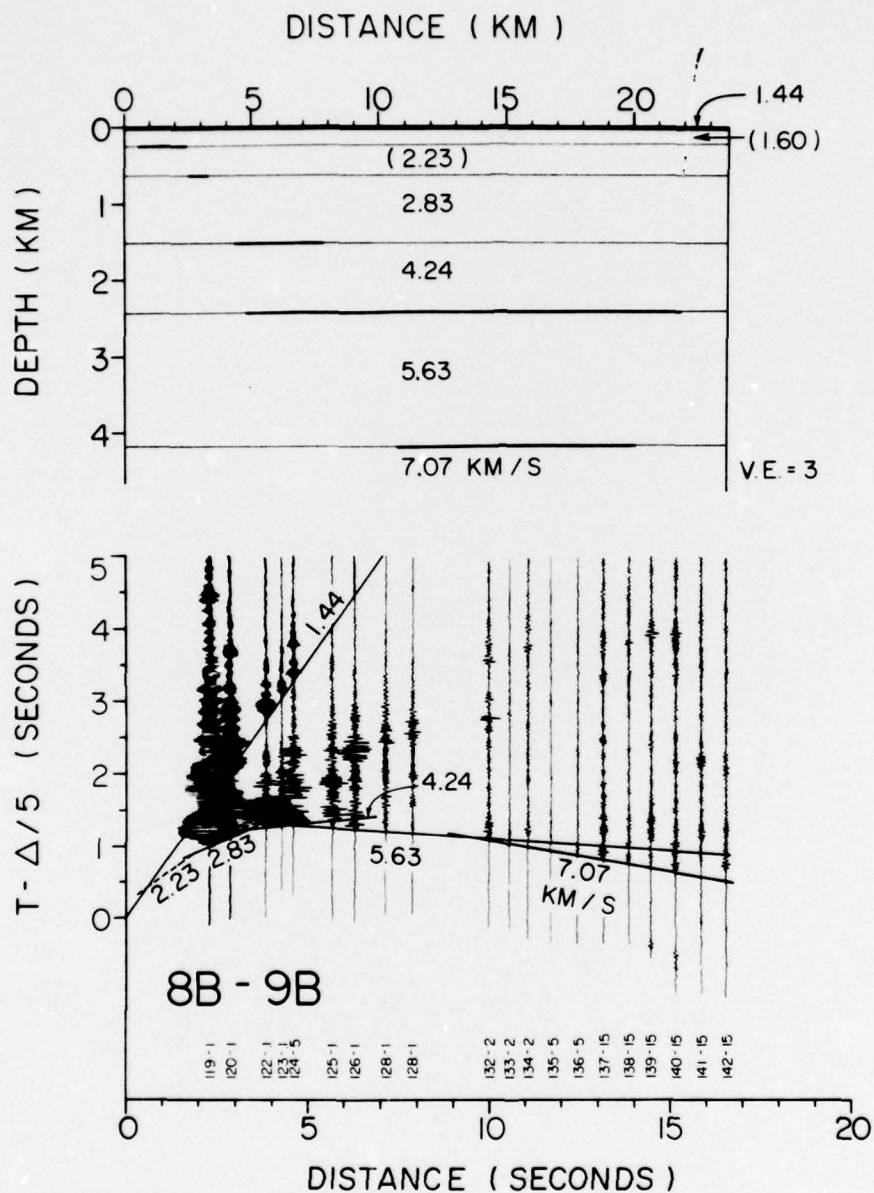


Figure 15. Line 8B-9B record section and velocity-depth model interpretation.

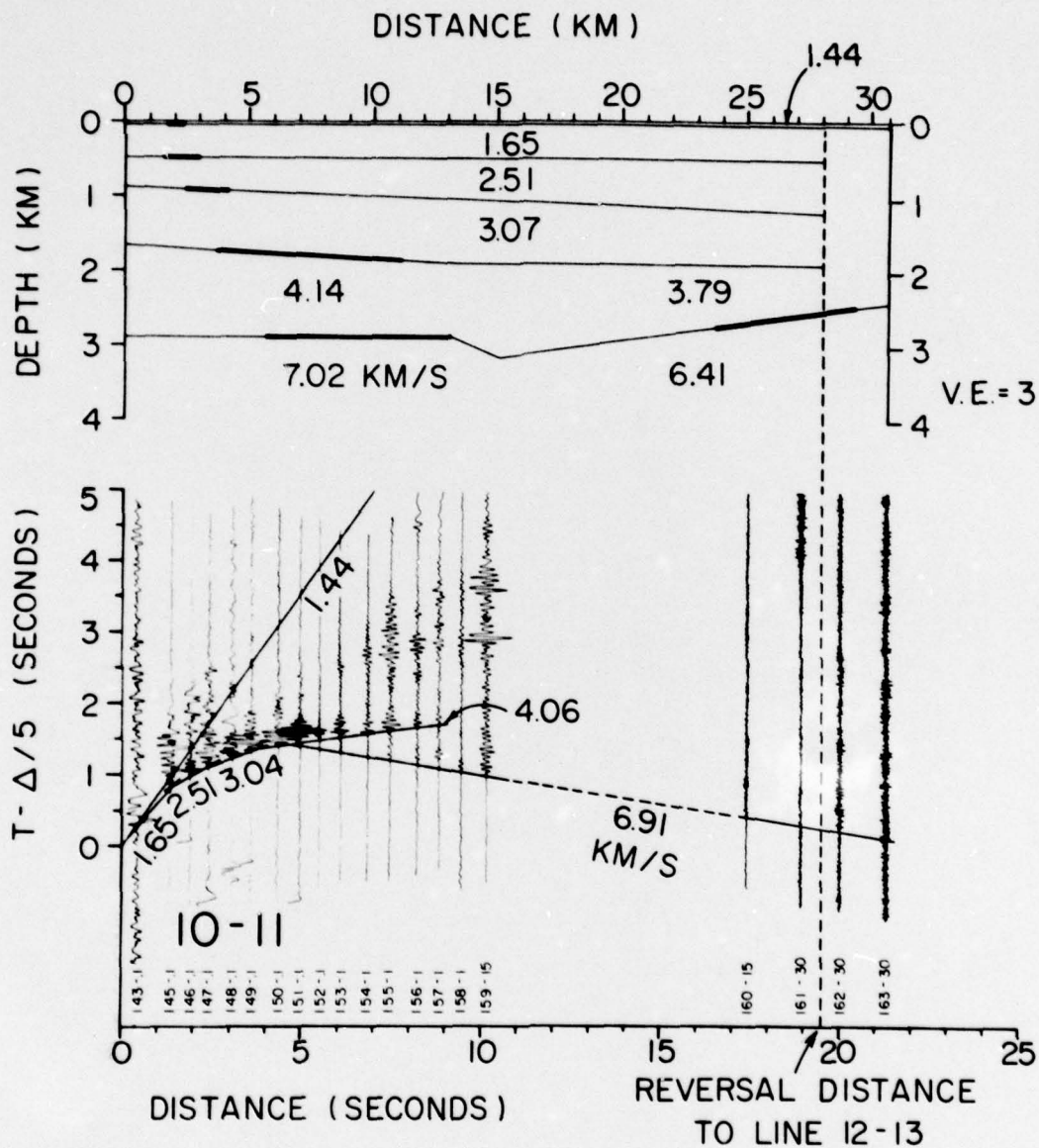


Figure 16. Line 10-11 record section and velocity-depth model interpretation.

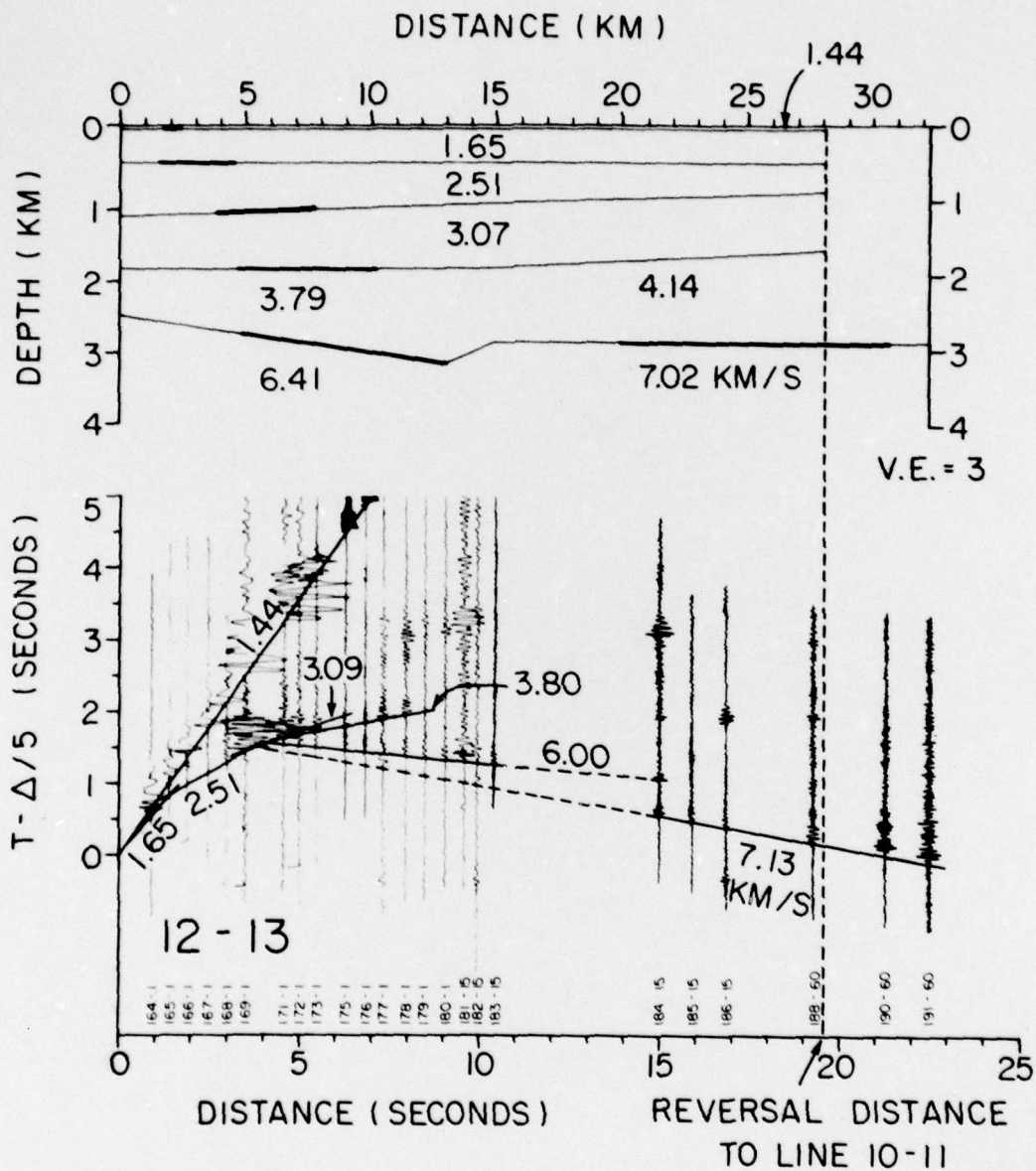


Figure 17. Line 12-13 record section and velocity-depth model interpretation.

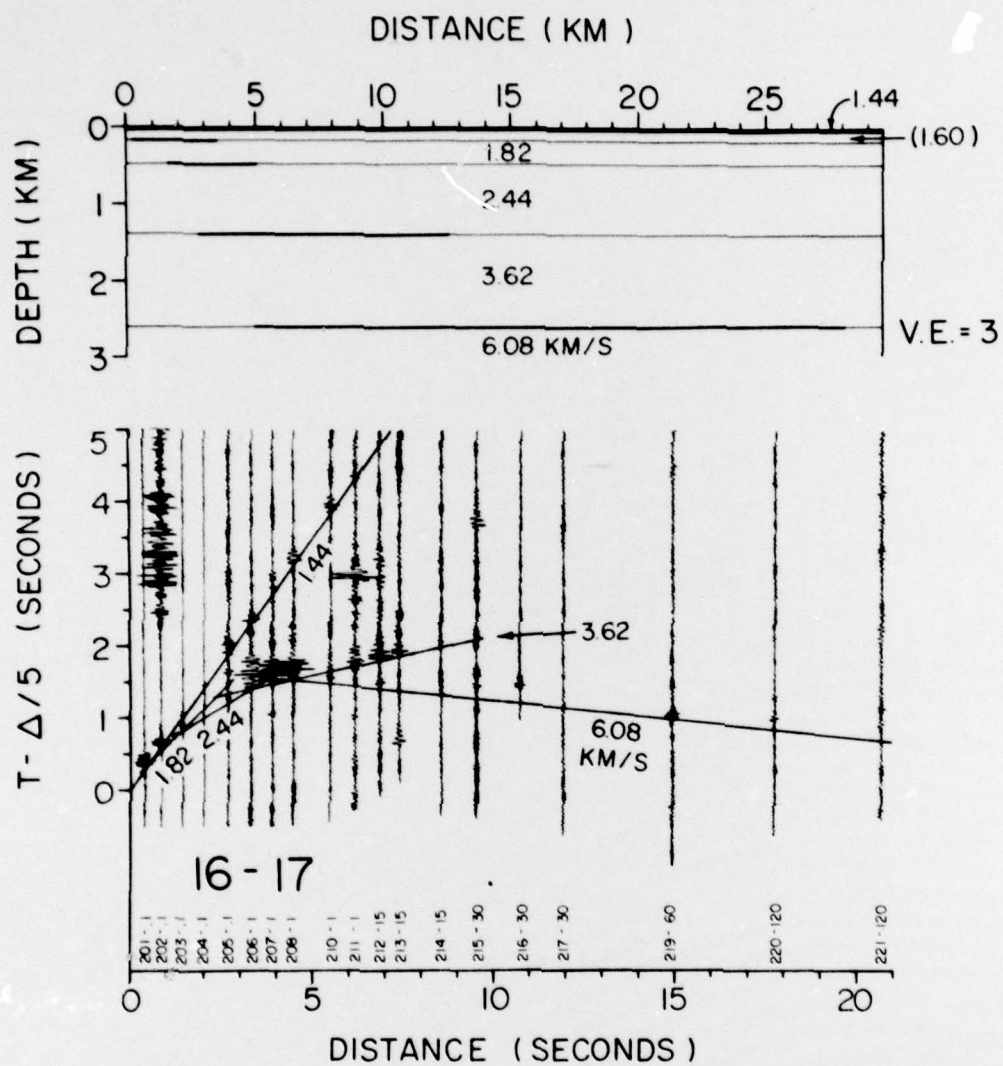


Figure 18. Line 16-17 record section and velocity-depth model interpretation.

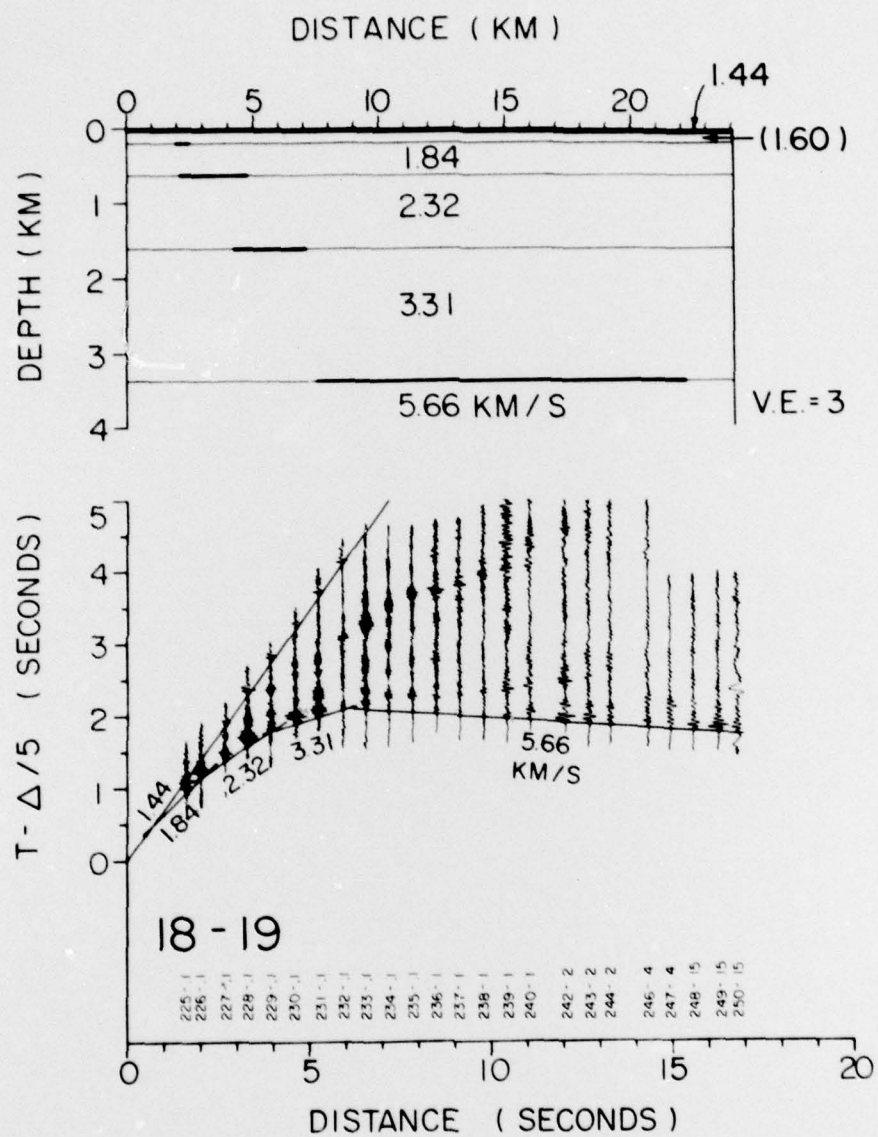


Figure 19. Line 18-19 record section and velocity-depth model interpretation.

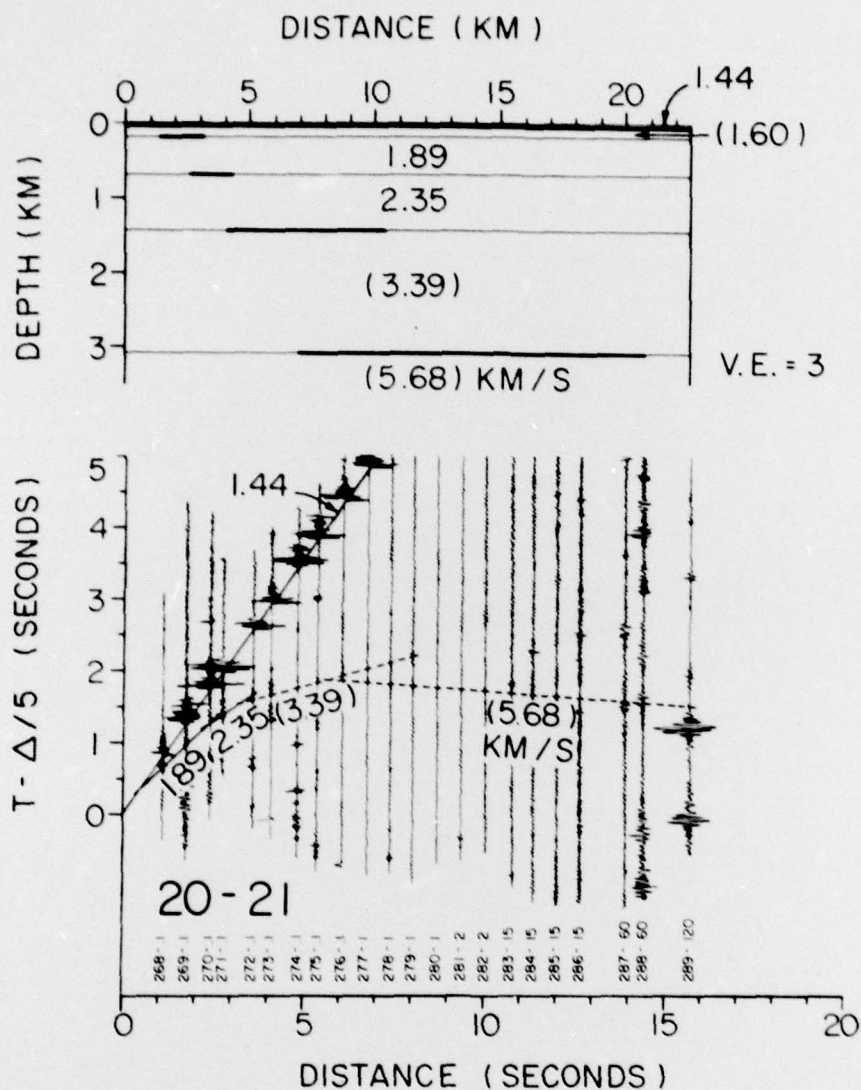


Figure 20. Line 20-21 record section and velocity-depth model interpretation.

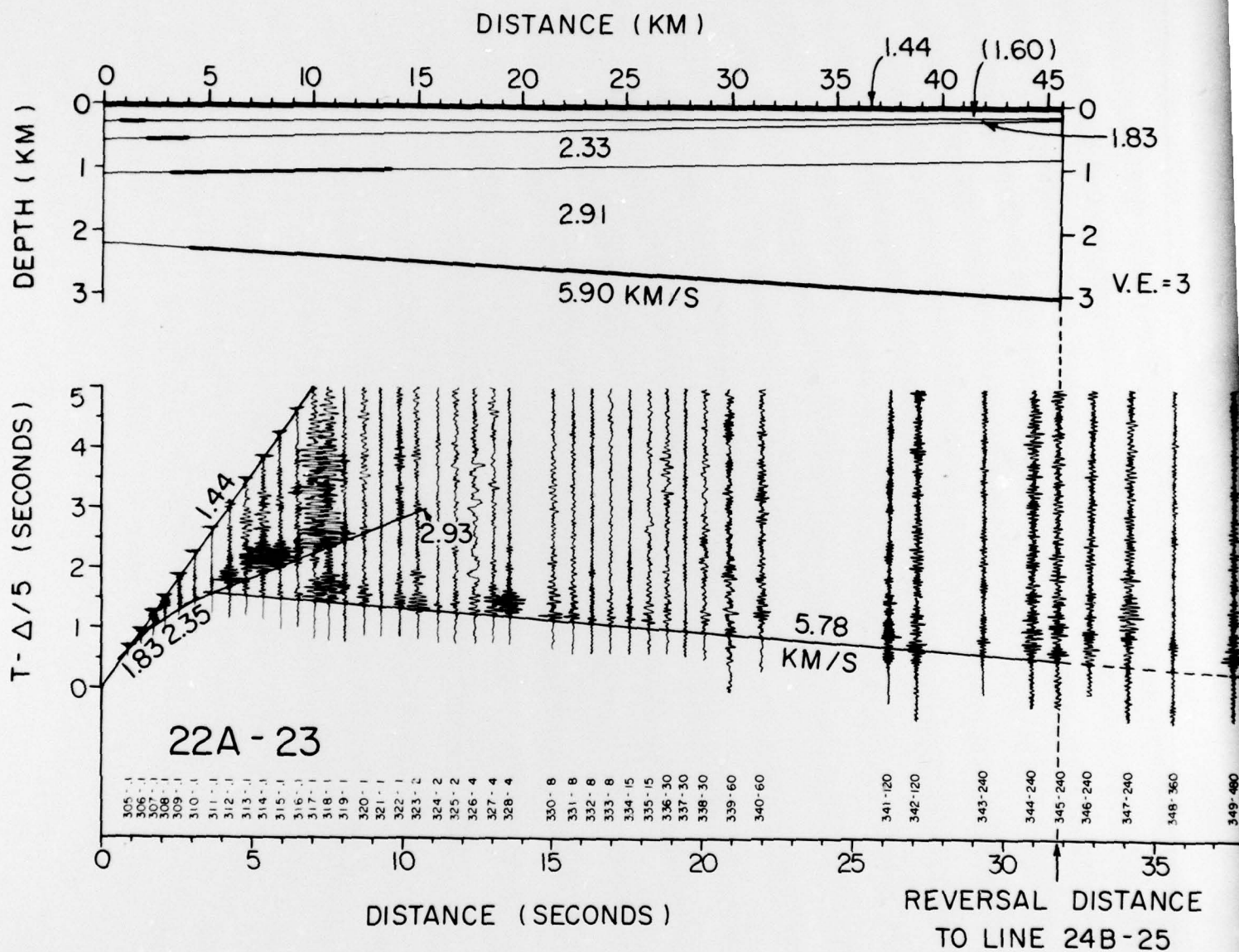
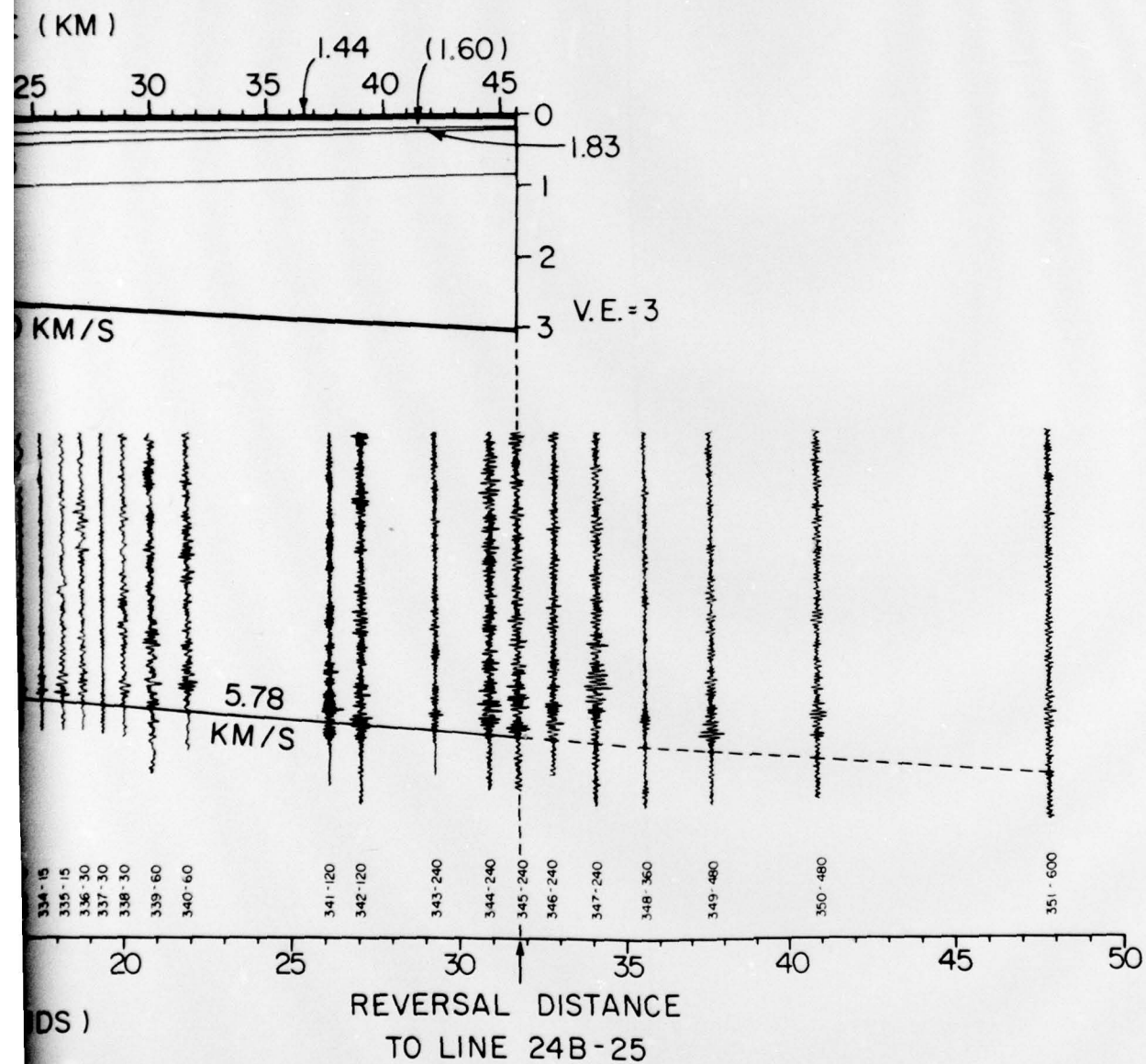


Figure 21. Line 22A-23 record section and velocity-depth model interpretation.



2

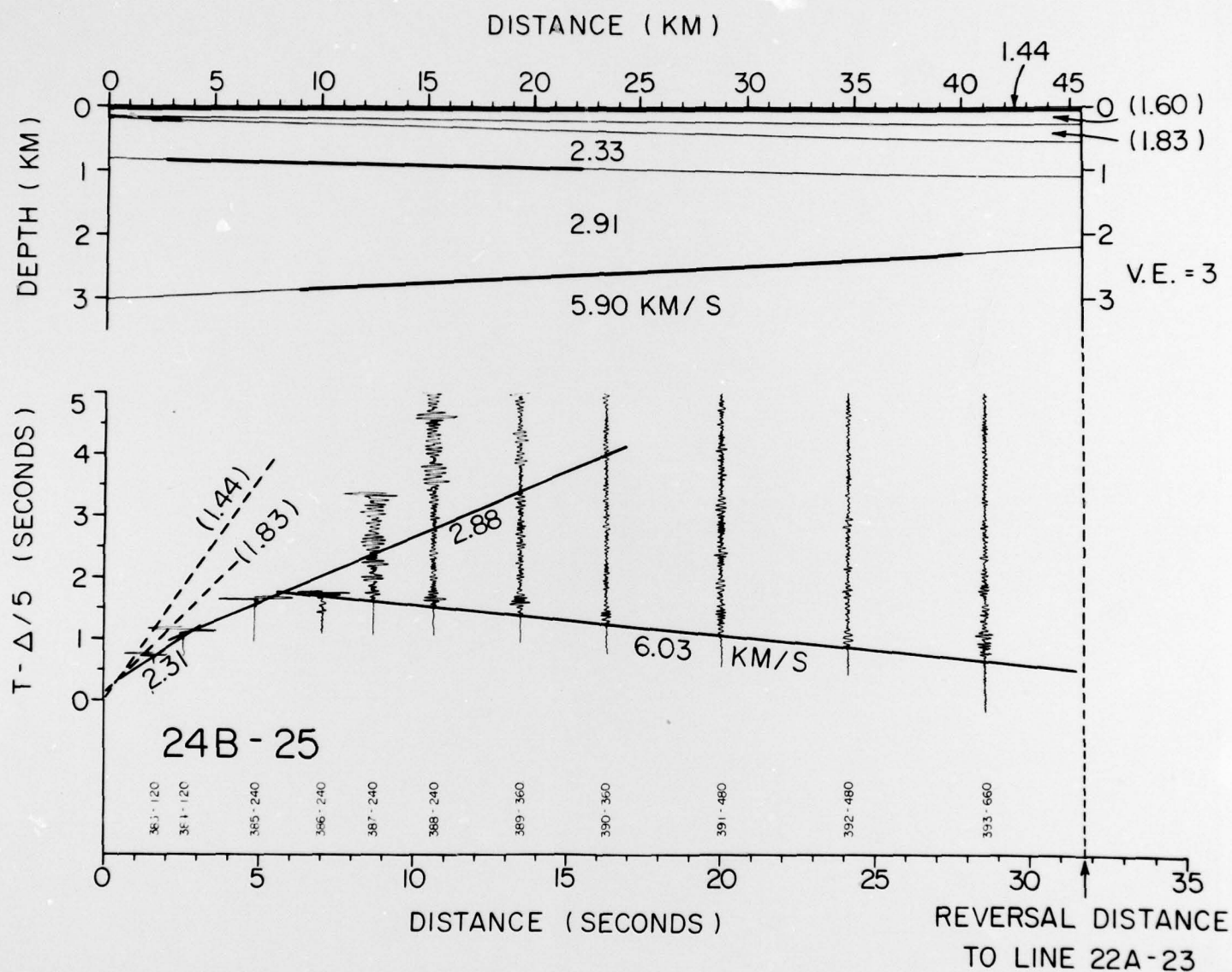


Figure 22. Line 24B-25 record section and velocity-depth model interpretation.

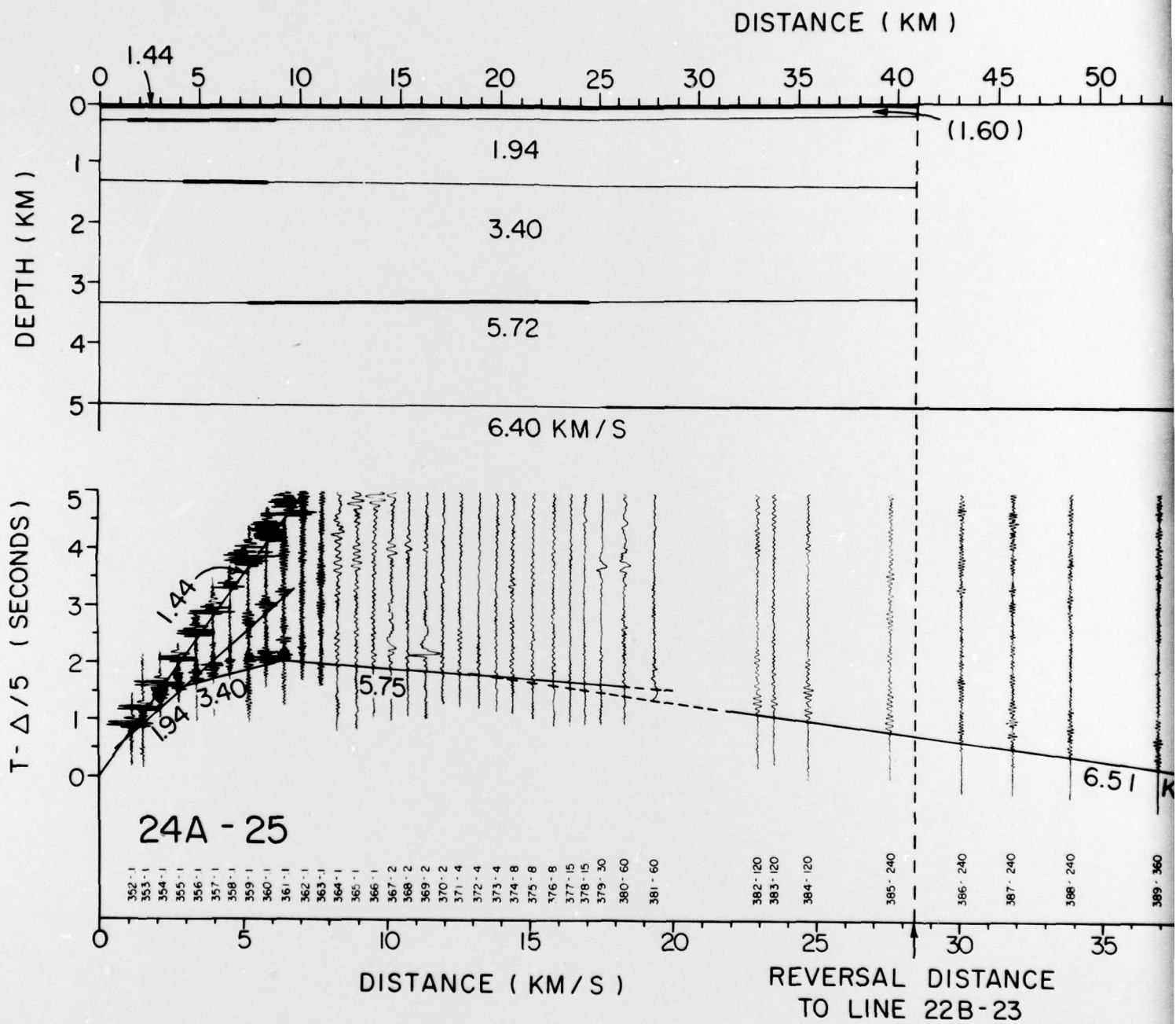
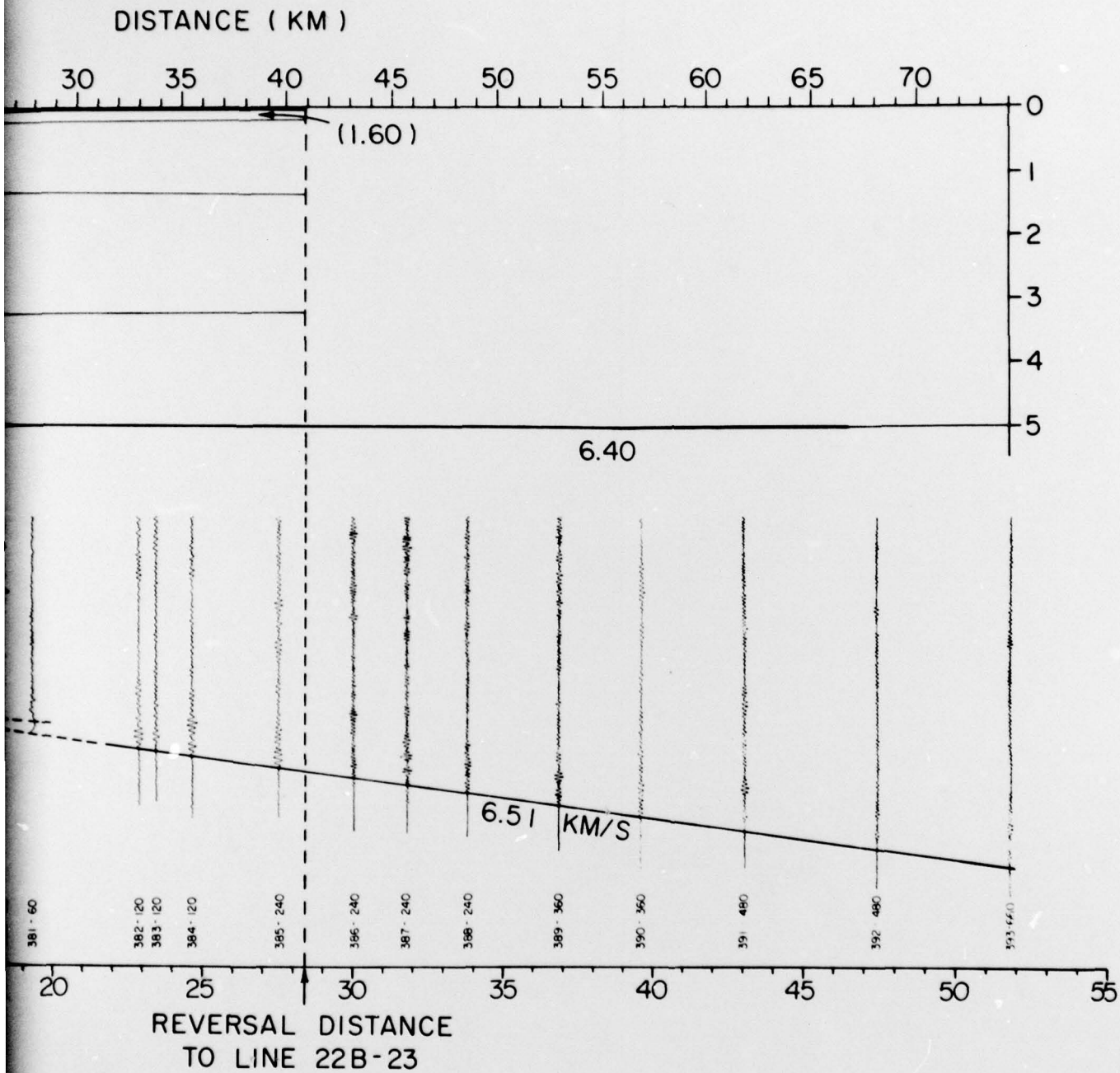


Figure 23. Line 24A-25 record section and velocity-depth model interpretation.



Locality-depth model interpretation.

2

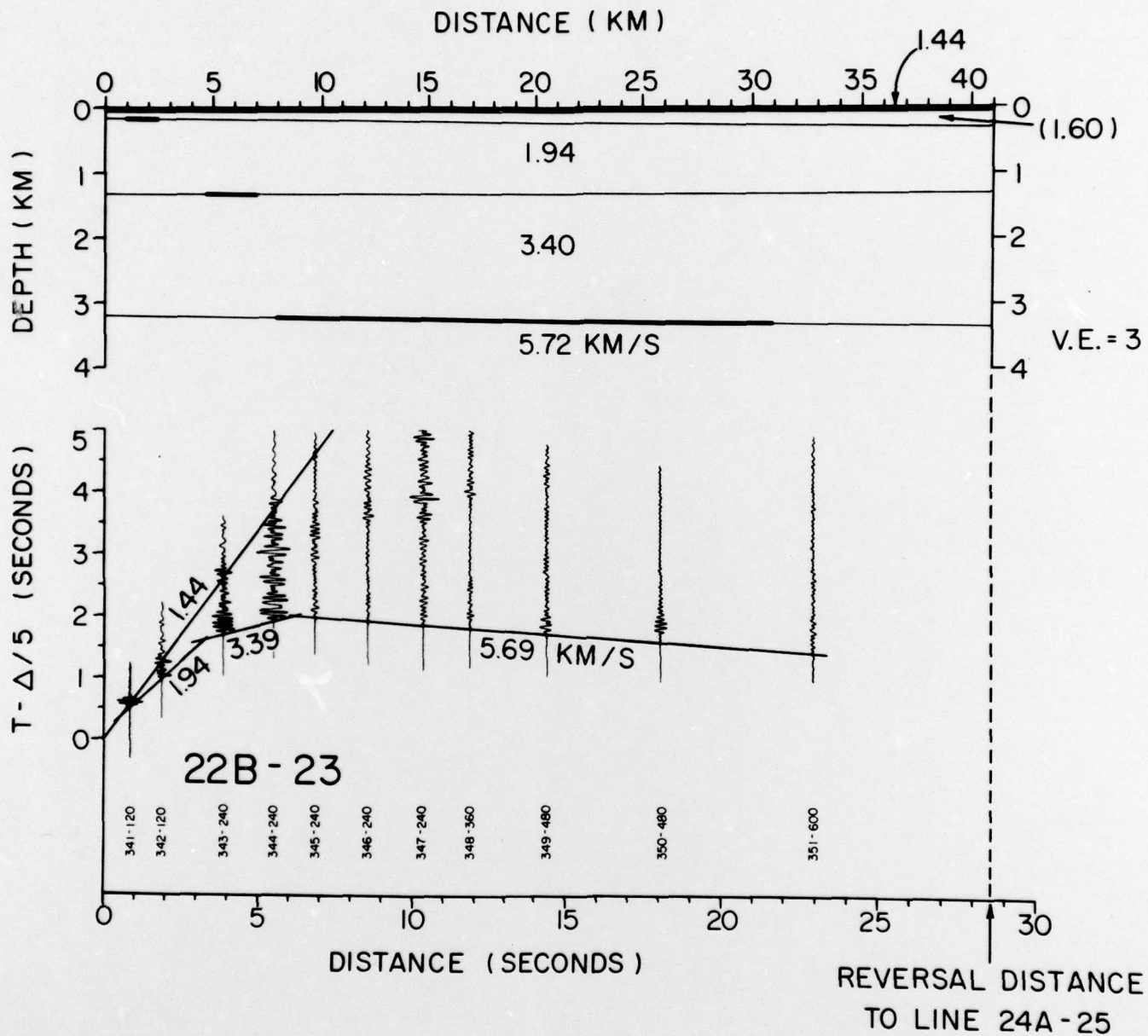


Figure 24. Line 22B-23 record section and velocity-depth model interpretation.

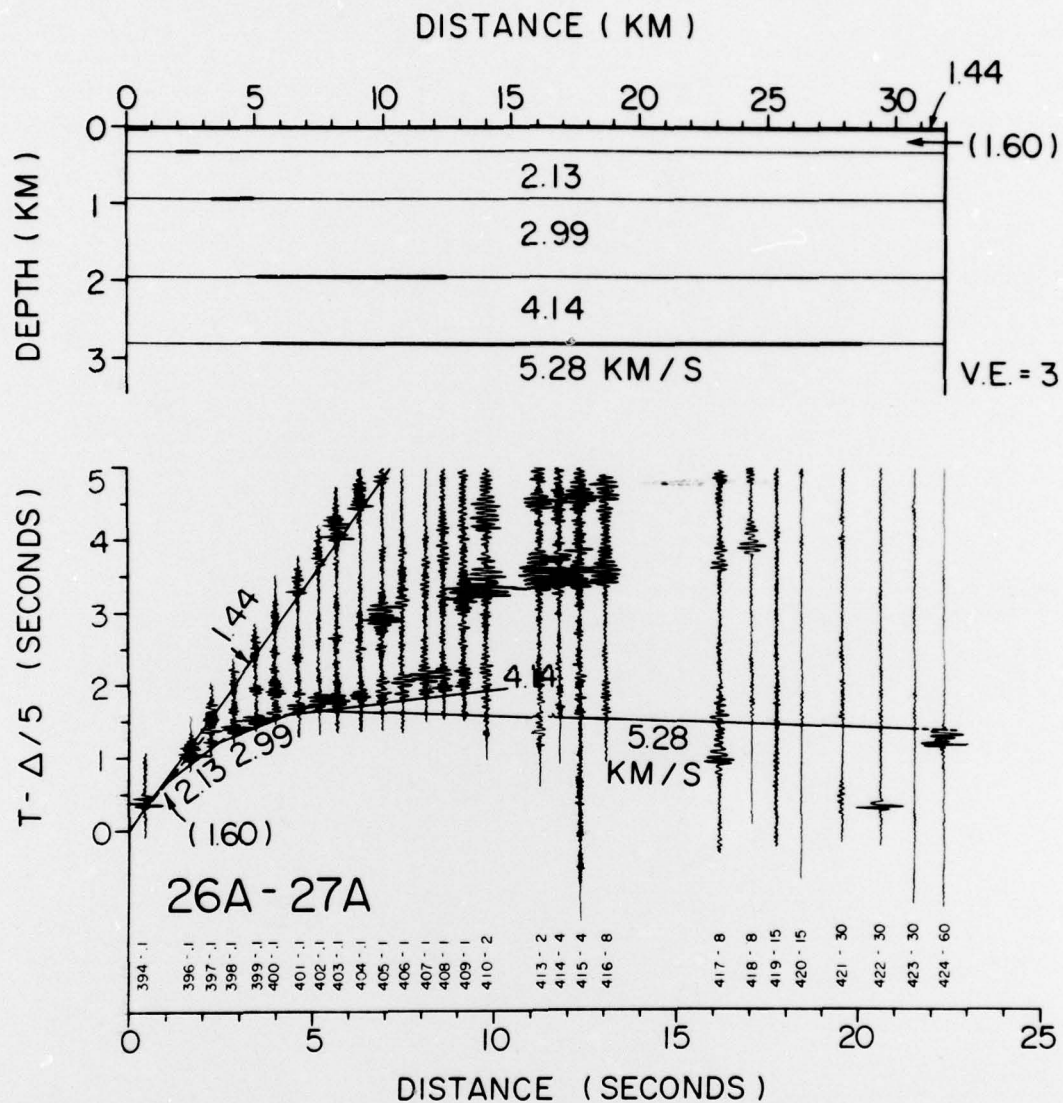


Figure 25. Line 26A-27A record section and velocity-depth model interpretation.

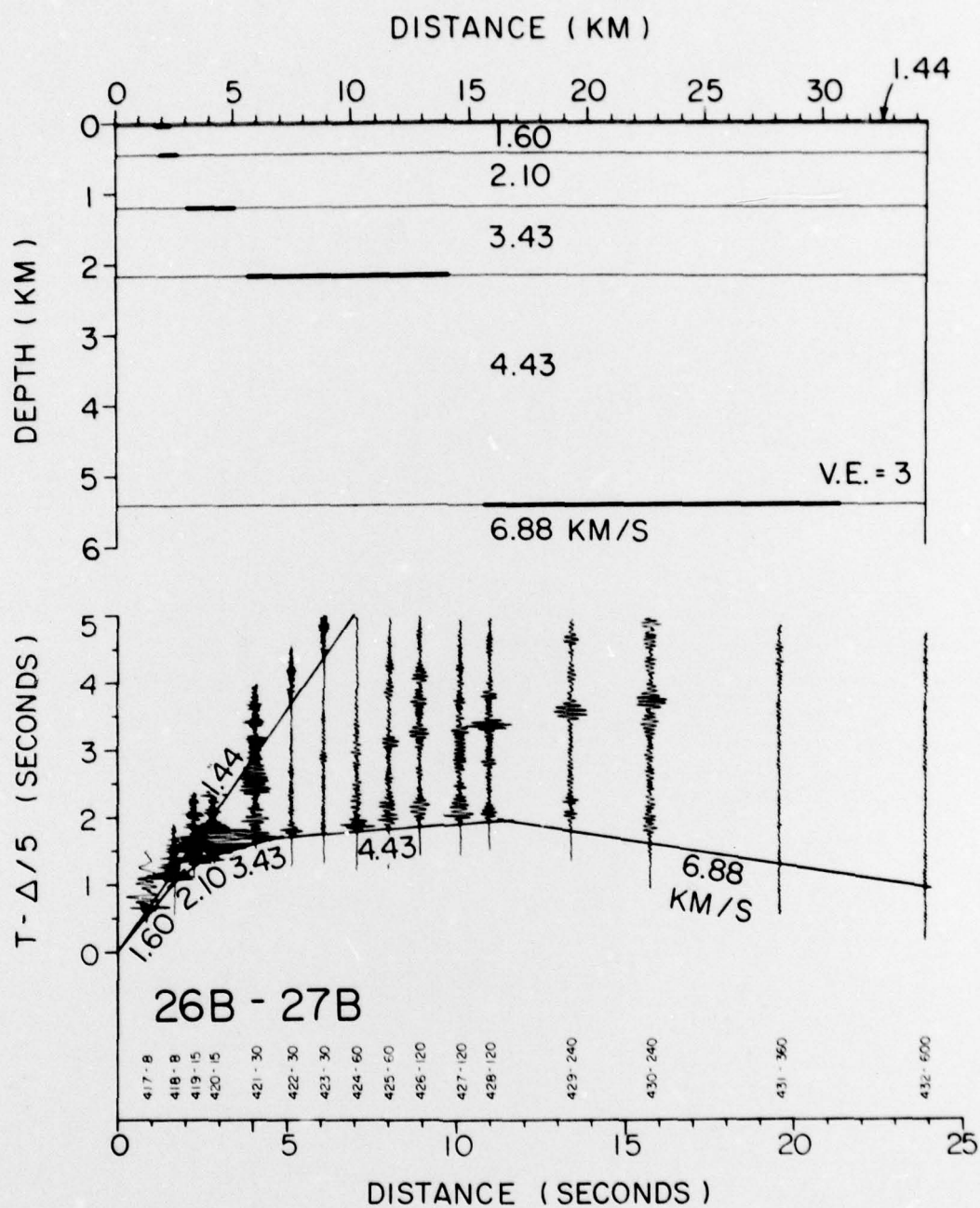
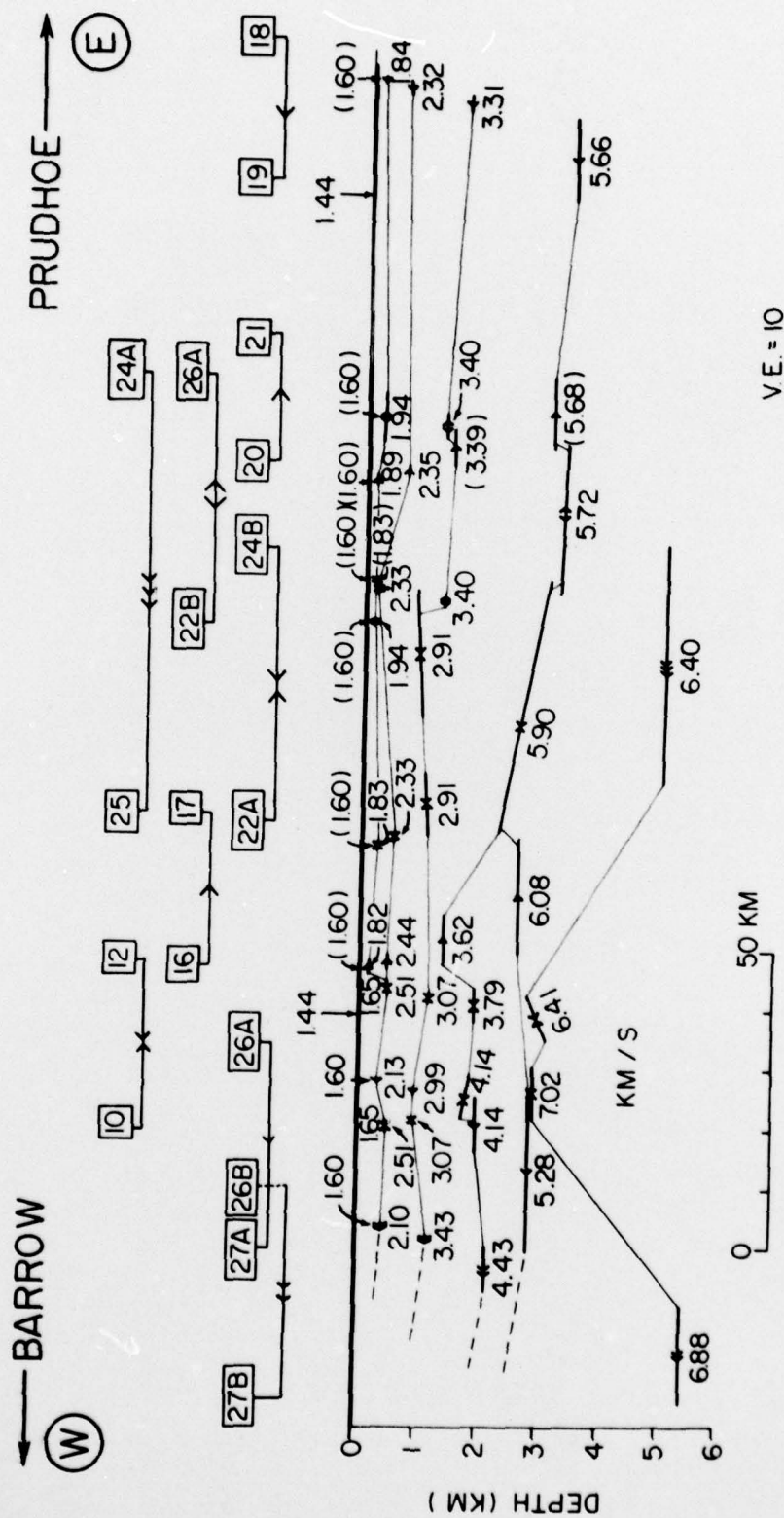


Figure 26. Line 26B-27B record section and velocity-depth model interpretation.



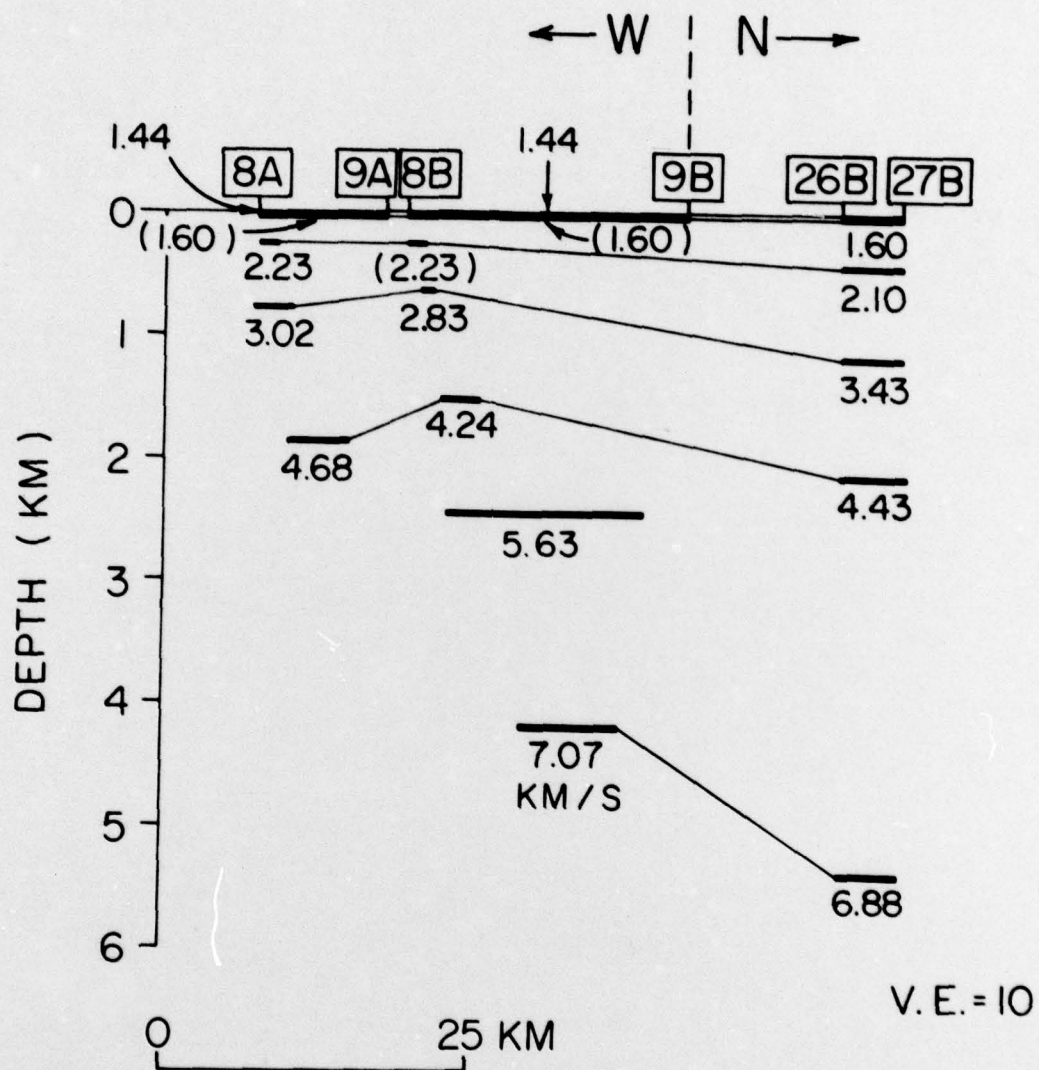


Figure 28. Velocity-depth section north of Smith Bay.

REFERENCES

Adachi, R., 1954. Fundamental relations on the seismic prospecting.

Kumamoto Journal of Science, Series A, 2: 18-23.

Bée, M., 1979. Marine seismic refraction study between Cape Simpson and Prudhoe Bay, Alaska. Master Thesis, Oregon State University, Corvallis, Oregon.